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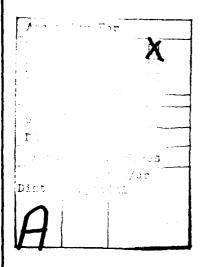
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- Task I encompassed the design, development and procurement of hardware, sensors, and microprocessors for two diagnostic monitoring systems. The first system was installed on the F-14 Hydraulic Flight Simulator on Task II of the program.
- Task II Installed one system on the F-14A Hydraulic Simulator for System component reliability demonstrations. The task also covered simulated component failures and diagnostic system reaction.
- TaskIII Integrated the Diagnostic System into A6E B/N 155628

 Debugged the system and ran a 12 month flight test schedule.

 This report covers Task III.



SUMMARY

This program was based on the feasibility study of a hydraulic monitoring system described in NADC report number TR75168-30 published in July 1976. The interim report, NADC TR76389-30, was published in May 1979 and covered Tasks I and II.

The purpose of the Hydraulic Diagnostic Monitoring System (HYCOS) is to warn of impending failure of hydraulic system components by onboard sensors continuously monitoring failure-indicating parameters.

The monitoring system consists of three basic types of sensors: analog, discrete, and fiber-optic. These sensors feed information to a self-contained, centrally located display panel through interface circuits that are easily accessible to ground maintenance personnel. The panel has circuit and system test capability which detects malfunctions of electronic equipment, sensor circuits, and display indicators.

The Sensor List includes the following types:

- Displacement: (a) Potentiometer rotary and linear (analog)
 - (b) Photo-optic (reflective)
 - (c) Hall Effect (magnetic)
- Temperature: (a) Pressurized gas (discrete)
 - (b) Bimetallic (discrete)
 - (c) I/C transducer (analog)
- Differential Pressure, Filter: Spring biased piston (discrete)
- Pressure: (a) Gas and spring biased switch (discrete)
 - (b) Semiconductor strain gage (analog)
- Liquid Detection: Fiber-optic probe using refractive index coupling (discrete)
- Flow: Orifice with bypass shunt for higher flows (discrete)
- Desiccant Color Detection: Fiber-optic color transmission using reflected light. Optical properties of irregular granules (analog - color spectrum)

Displacement sensors of the variable-resistance type were used to measure reservoir piston, accumulator, rudder, and rudder pedal displacements. Two other concepts evolved in the accumulator application, a reflective photo-optic type and a magnetic Hall Effect type. Since they are experimental in nature and require development, they were not used in the prototype system.

Three types of temperature sensors (one analog and two discrete) were chosen and utilized in the pneumatic, fluid, and surface temperature circuits. Their performance was satisfactory during simulator testing. Filter differential pressure indicators were of the spring biased magnetically latching type. Their performance was satisfactory.

Two types of pressure-sensor devices were utilized. In one pneumatic circuit, a temperature-compensated pressure switch performed as predicted over a broad temperature range. In another pneumatic hydraulic circuit, a semiconductor strain-gage type also performed according to specification.

Liquid detection circuits in high-pressure pneumatic bottles proved to be a challenge in the area of pressure sealing and liquid detection using the optical properties of liquids, solids, and gases. All major problems were overcome after extensive development effort.

The use of shunt orifice flow measuring devices proved satisfactory in three hydraulic subcircuits. In two of the three cases, the indicator was immobilized during normal system operation.

Desiccant color detection utilizing color transmission proved difficult due to the irregular desiccant particles. A high-intensity light source was required to achieve sufficient color transmission. An improved sensor was developed for the A-6E installation.

The diagnostic system monitors the hydraulic system during flight as well as on the ground. Any flight discrete failures are displayed when the aircraft is interrogated on the ground. Discrete sensors are manually resettable.

An onboard preprogrammed microprocessor handles all the analog inputs through A/D converters and determines the condition of components with multiple sensors.

Task I defined and procured hardware sensors for two diagnostic monitoring systems. After individual component acceptance testing, the system was interfaced with a F-14A hydraulic simulator.

Task II consisted of installing the system on the F-14A hydraulic simulator in order to demonstrate system/component reliability under simulated conditions. A baseline was established and various failure modes and diagnostic system reactions determined.

The scope of the Interim Report covered only the development and integration of the F-14 hydraulic monitoring system.

Task III of the hydraulic monitoring system contract consisted of procuring, building, installing, and testing in a bailed A-6E flight test vehicle for a duration of at least 6 months.

To accomplish these objectives:

- Bracketry was designed and fabricated to support the system components. The combined hydraulic fluid distribution system was modified to accept pressure, flow, and temperature sensors
- Electrical and fiber-optic cable runs were designed, fabricated, and installed between the HYCOS display panel and sensors
- The HYCOS system was installed only in the combined hydraulic system and did not affect system operation
- Representative system components and parameters were monitored. These included
 - Hydraulic reservoir
 - Filters
 - Accumulator
 - Pneumatic bottles
 - Hydraulic pump
 - Rudder actuator
 - Relief valve
 - System operational hours
- The microprocessor program was written to apply specifically to the A-6E requirements

- The vehicle received normal ground tests prior to being cleared for its normally scheduled flight program
- During the flight program (installed January 1979, removed November 15, 1980) the system accumulated over 160 flight hours. First flight occurred on October 31, 1979.

A Navy A-6E bailed aircraft was designated as the official test vehicle in January 1979. By May 1979, the modified hydraulic system was initially pressurized to check for system compatibility. During the latter part of the year, the system was modified to improve reliability and maintainability.

Improvements were made to both the display panel and sensors. In the area of light sensing, transmission of colored light proved difficult since, during installation of the fiber-optic cables, excessive bends were made creating unacceptable light losses. However, the concept was verified.

During the test program, the system continuously detected low pneumatic bottle pressures and low reservoir level during calibration and system operation. No other system abnormalities or malfunctions were detected.

The total time for interrogating the system is 1-1/2 minutes. This significantly reduces turnaround time and increases aircraft availability.

PREFACE

This report was prepared by the Grumman Aerospace Corporation under a Naval Air Development Center, Contract Number N62269-78-C-0041, entitled "Hydraulic Diagnostic Monitoring System".

The program was based on a previous feasibility study conducted by Grumman Aerospace Corporation and reported in NADC TR 75168-30.

Task I of this program covered procured hardware, sensors, and microprocessors for two monitoring systems. One system was installed in a F-14 Flight Simulator and the other scheduled for an A-6 aircraft. The work reported in the report covers the November 1977 to December 1978 timeframe.

Task II covered the results of installing the system in an F-14A hydraulic simulator, integrating and debugging the system, and finally simulating various failure modes in order to demonstrate diagnostic system reaction.

Interim Report NADC TR 76389-30 Hydraulic Diagnostic Monitoring System was published 31 May 1979, covered Tasks I and II.

Task III encompassed the basic integration, debugging, and flight test of the A-6 System.

The sponsoring agency is the Naval Air Systems Command, Washington, D.C. Mr. Steve Hurst, AIR 340C, was the Program Manager

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Project Engineer for this contract was Mr. John J. Duzich

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- Aircraft Programs
- Aircraft Project Office
- Controls and Mechanisms
- Electronic Design and Development
- Equipment Lines
- Flight Development Group
- Fluid Power
- Mechanical Design
- Mechanical/Fluid Systems Test
- Quality Control
- Structural Design.

Daily HYCOS System recording, performed by Mr. Frank Martella, Plane Captain, was invaluable in assessing this phase of the program.

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Section 1

HYDRAULIC DIAGNOSTIC MONITORING SYSTEM

1.1 VEHICLE DESIGNATION

On 31 January 1979, Naval Air Systems Command Selected A-6 Bureau Number 155628 as the vehicle to be used as a flight test bed for the hydraulic monitoring system. The vehicle, which was being modified/updated, arrived at the Grumman facility during the preceding year and started through the modification line in February as MOD 229.

1.2 VEHICLE MODIFICATION

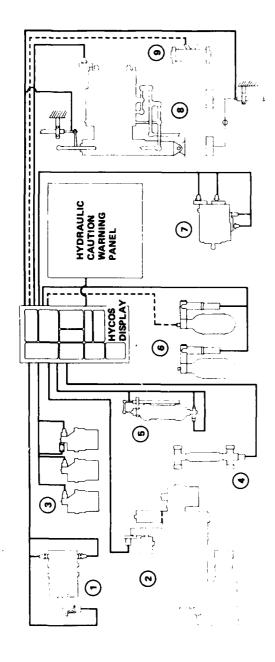
During the time the vehicle was being upgraded to an A-6E configuration, the HYCOS system was installed since all necessary areas were accessible. The HYCOS A-6E block diagram is shown in Figure 1.

Installation was accomplished through the issuance of both Record and Flight Test Engineering Orders (EO) to minimize the impact of the normal buildup. This approach led to an efficient and expeditious system installation. All EOs are listed in Appendix G.

Vehicle modifications included provisions for mounting the HYCOS panel in a ground-accessible area on the port side of the engine duct. Mounting brackets and an access panel door were fabricated and installed. Since the selected surface area is a load-bearing member, Calfax fasteners were used for easy access.

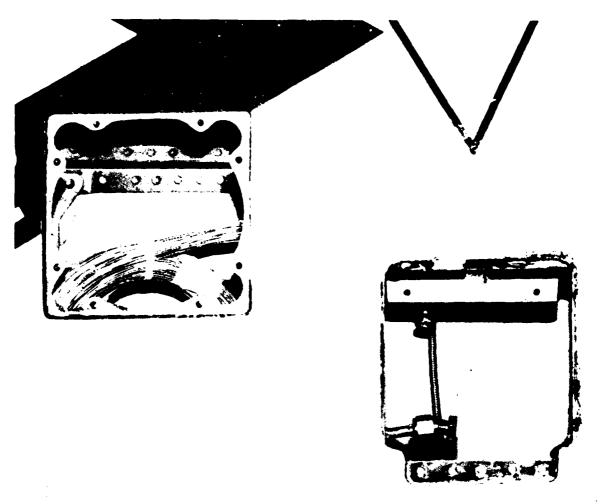
Both wire and fiberoptic line runs were installed in the vehicle at this time in conjunction with the other wiring circuits. New lines were fabricated as required for sensors installed in the pressure system.

All HYCOS sensor line runs terminated at the test panel through the use of three electrical connectors and two fiberoptic connectors. Figure 2 shows the access area with the wire bundles before modification.



1. RESERVOIR LEVEL POTENTIOMETER IC 6. PNEUMATIC BOTTLE PRESS. SWITCH 2. BACK UP PACKAGE TEMP IC 7. PUMP 7. PUMP PRESS. SWITCH PRESS. SWITCH PRESS. SWITCH SWITCH PRESS. SWITCH SWITCH PRESS. SWITCH SWITCH PRESS. SWITCH SWITCH SWITCH PRESS. SWITCH SWITCH SWITCH PRESS. SWITCH SWITCH SWITCH SWITCH PRESS. SWITCH SWITCH SWITCH SWITCH SWITCH PRESS. SWITCH SWITCH SWITCH SWITCH SWITCH SWITCH PRESS. SWITCH PRESS. SWITCH SWITC	ITEM	DESCRIPTION	SENSOR	TYPE	ITEM	DESCRIPTION	SENSOR	TYPE
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AGE TEMP SWITCH PRESS. DELTAP SWITCH 8. FLOW DELTAP SWITCH 8. FLOW DELTAP SWITCH 9. PELOW SAMPLING VALVE) RUDDER ACTUATOR DIFF DISPL TEMP SWITCH RUDDER ACTUATOR DIFF DISPL FESS TRANSDUCER PEDALS DIFF DISPL TEMP TRANSDUCER 9. DESICCANT DISPL TRANSDUCER 9. COLOR			PRESS.		7.	PUMP		
DELTA P SWITCH 8 FLOW TEMP DELTA P SWITCH 8 FLOW QUIESCENT DELTA P SWITCH 8 FLOW QUIESCENT SAMPLING VALVE) RUDDER ACTUATOR DIFF DISPL TEMP SWITCH PRESS TRANSDUCER PEDALS PRESS TRANSDUCER 9 DESICCANT COLOR DISPL TRANSDUCER 9 COLOR COLOR	7	BACK UP PACKAGE	TEMP	SWITCH		OUTLET	PRESS.	SWITCH
DELTAP SWITCH 8 FLOW TEMP DELTAP SWITCH 8 FLOW QUIESCENT DELTAP SWITCH RUDDER ACTUATOR DIFF DISPL TEMP SWITCH PLOW QUIESCENT PRESS TRANSDUCER PEDALS DIFF DISPL TRANSDUCER 9 DESICCANT COLOR	က	FILTERS				CASE	FLOW	SWITCH
DELTA P SWITCH 8. FLOW QUIESCENT		PRESS.	DELTA P	SWITCH			TEMP	SWITCH
DELTAP SWITCH SAMPLING VALVE SAMPLING VALVE TEMP SWITCH PRESS TRANSDUCER P. DESICCANT COLOR COLO		RETURN	DELTAP	SWITCH	æ	FLOW	QUIESCENT	SWITCH
SAMPLING VALVE RUDDER ACTUATOR DIFF DISPL		CASE	DELTAP	SWITCH				
TEMP SWITCH FLOW QUIESCENT PRESS TRANSDUCER 9. DESICCANT COLOR DISPL TRANSDUCER 9. CONDITION			(SAMPLING	VALVE)		RUDDER ACTUATOR	DIFF DISPL	POTENTIOMETER
PRESS TRANSDUCER PEDALS DIFF DISPL TEMP TRANSDUCER 9. DESICCANT COLOR DISPL TRANSDUCER CONDITION	4	RELIEF VALVE	TEMP	SWITCH		FLOW	QUIESCENT	SWITCH
TRANSDUCER 9. DESICCANT COLOR ITRANSDUCER CONDITION	က်	ACCUMULATOR	PRESS	TRANSDUCER			DIFF DISPL	POTENTIOMETER
TRANSDUCER			TEMP	TRANSDUCER	oi	DESICCANT	COLOR	OPTICAL
			DISPL	TRANSDUCER		CONDITION		

Figure 1. A-6E HYCOS block diagram.



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Figure 2. Access panel before modification.

1.3 VEHICLE COMPONENT INSTALLATION

As specified in the statement of work, various components were modified to sense variables as determined during the previous program. The parameters included:

- Level
- Temperature
- Air Content

- Differential Pressure
- Liquid Detection
- Flow
- Desiccant Saturation
- Total System Operating Hours

1.3.1 Hydraulic Reservoir

1.3.1.1 Description

The combined system reservoir was designed to meet the requirements of Specification MIL-R-5520A-1 for a "Class II" separated air and oil reservoir. A "Type B" reservoir pressurized with air to a nominal operating value of 40 psi was used. The detail design configuration is that of a welded and machined outer casing with concave hemispherical ends enclosing a cantilevered, pressure-balanced sleeve. This configuration is not subjected to distortions produced by pressure surges and structural deflection. A free-floating piston separates system oil from pressurizing air. Both return and suction ports are located in the side of the outer shell. Returning oil impinging on the outer surface of the piston sleeve provides natural air separation characteristics. The concave ends minimize weight by reducing the volume of non-usable oil. Figure 3 shows the typical construction.

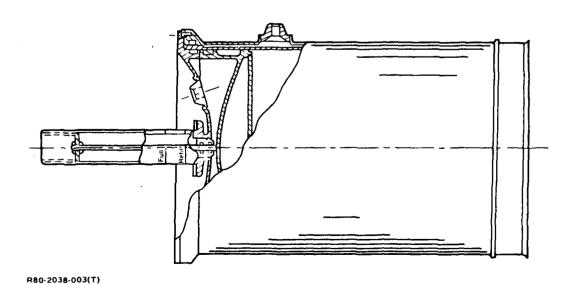


Figure 3. A-6 reservoir typical construction (before modification).

1.3.1.2 Reservoir Sensing Logic

The purpose of the reservoir sensing logic is to:

- Detect the presence of entrained air
- Detect low oil level
- Detect extensive leakage during the previous flight.

Figure 4 shows the A-6E hydraulic reservoir sensing logic. The logic employs variables of fluid temperature and piston displacement. Piston placement during the nonpressurized to pressurized condition gives an indication of entrained air. Fluid thermal expansion is automatically taken into account during microprocessor programming.

1.3.1.3 Displacement Sensor

An external 10-turn potentiometer was driven via a cable attached to the modified piston. Tensioning of the cable was accomplished by a negator spring motor contained in a pressure housing. One pulley on the motor drove an externally mounted potentiometer through a lip type seal. Reservoir pressurization was accomplished through the normal pressure housing port.

This configuration minimized the rework modification required for providing remote reservoir level sensing capability. Figure 5 shows a cross-section of the modification and the adapter ring added to the reservoir piston. Figure 6 shows details and subassembly of the modified reservoir.

The negator motor model number ML-2918, manufactured by the Hunter Spring Division of Ametek, was selected because of its constant-torque characteristics. Pertinent motor assembly details are listed below:

•	Physical Dimensions	$2-1/2 \times 3-3/4 \times 1-3/16$ in.
•	Materials:	

Base Zinc-plated steel	
Drums Delrin or nylon	
Spring 301 stainless steel	
Cable	

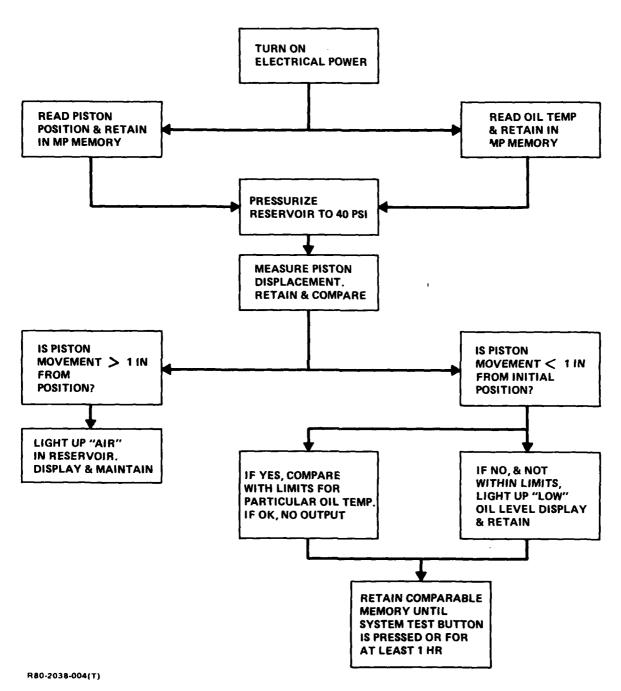


Figure 4. A-6E reservoir sensing logic.

•	Spring Torque 1.56 lb-in.
•	Cable Tension 2 lb
•	Cable Length 72 in.
•	Number of Revolutions
•	Min Endurance Cycles 2500

The motor assembly was mounted in the 1491-901-306 remote sensor housing with the cable terminal modified from a coil to a bead. This cable bead was free to float in the modified piston adapter ring.

A rotary potentiometer was attached to the driving end of the motor assembly as specified in Grumman Specification 209. Some pertinent data includes:

• Type: 10-Turn

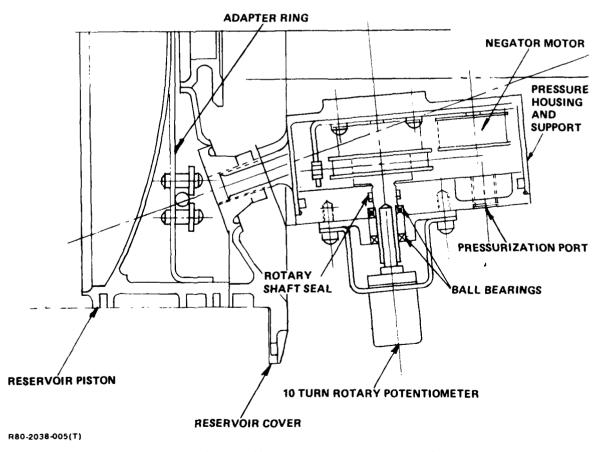
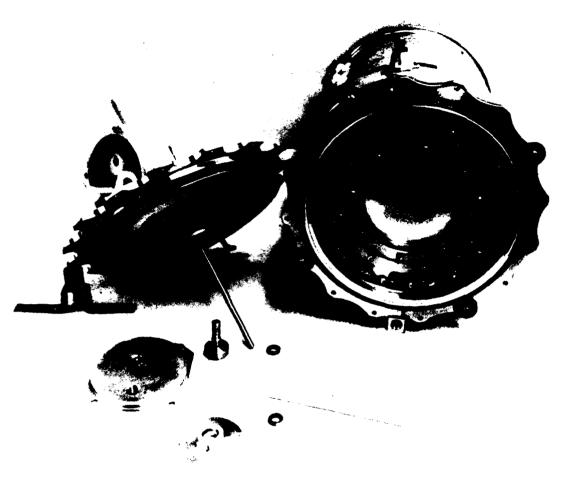


Figure 5. Modified reservoir (level sensing).



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Figure 6. Modified reservoir subassembly and details.

• Element: Wirewound

• Dimensions: 0.875 in. OD

1.00 in. long

• Resistance: 20,000 Ohms

• Power Rating: 2 W

• Temperature Range: -65 to 255°F

• Torque: 0.60 oz-in. maximum

• Weight: 1 oz

• Resolution: 0.014%

Full travel of the hydraulic reservoir piston is 13.31 in. This piston movement relates to approximately three turns of the potentiometer, which is approximately 6000 Ohms. Figure 7 shows a calibration curve prepared in the Plant 14 Laboratory.

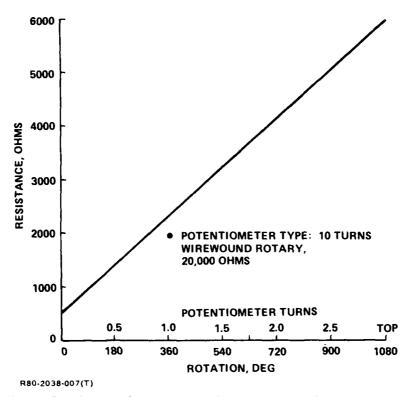


Figure 7. Hydraulic reservoir (laboratory calibration curve).

Considerations of temperature and entrained air variations provide the curves shown in Figures 8 and 9. Since the reservoir pressurization is only 40 psi, significant volumes of entrained air are required to cause measurable piston displacements between the pressurized and nonpressurized state. Hysteresis is limited to 2 psi in either direction.

Another factor considered but not applied in reservoir level sensing is piston movement/depletion time versus leak rate for both the combined and flight system. These curves (Figures 10 and 11) give an indication of reservoir depletion time in minutes versus varying leak rates. The initial datum point is taken at the refill mark of each reservoir. If each respective reservoir is full, the time to depletion is proportionately longer.

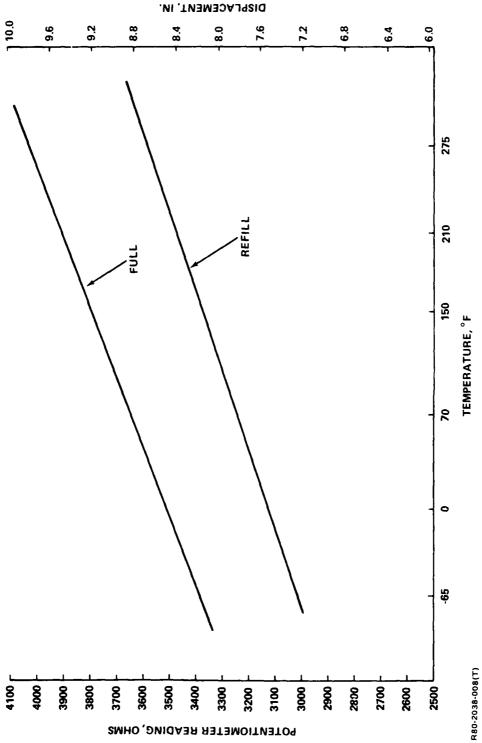


Figure 8. Reservoir calibration curve considering fluid temperature variation.

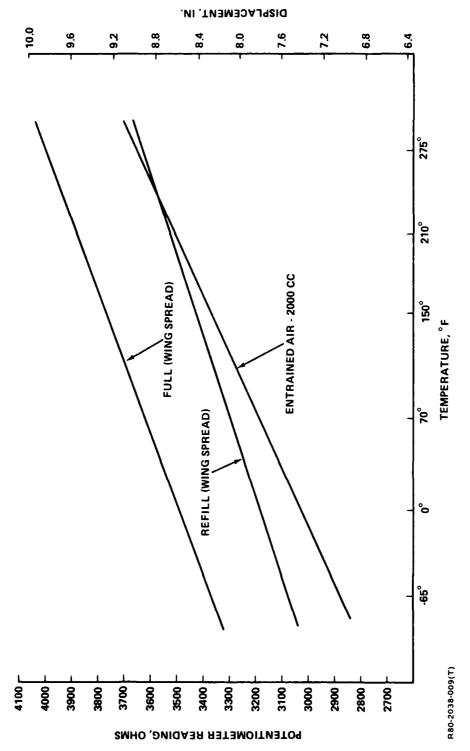


Figure 9. Calibration curve considering entrained air and temperature variation.

1.3.1.4 Temperature Transducer

The temperature sensor utilized a two-terminal I/C temperature transducer manufactured by Analog Devices of Norwood, Massachusetts.

The transducer, part no. AD590.C, produces an output current proportional to absolute temperature. With a supply voltage of 5 VDC, the device acts as a high-impedance, constant-current regulator passing $1\mu\text{A}/^{6}\text{K}$. Table 1 (extracted from Ref. 1) shows pertinent technical data.

TABLE 1. IC TEMPERATURE TRANSDUCER DATA.

• TYPE: ANALOG DEVICES AD 590.C

• **OUTPUT**: 1 μΑ/°Κ

• OPERATING TEMP RANGE: -55°C TO 150°C (-67°F TO 302°F)

• TWO-TERMINAL DEVICE: VOLTAGE IN/CURRENT OUT

• CALIBRATION ACCURACY: ±1°C

● LINEARITY: ±0.5°C OVER FULL RANGE

POWER SUPPLY/RANGE: +4 VDC TO +30 VDC

• SIZE: TO -52 PACKAGE

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Figure 12 (extracted from Ref. 1) shows a voltage-current plot for a typical transducer. Note that the current is essentially flat with an input voltage of 3 to 30 VDC.

The transducer was selected for its small size, performance, and compatability. Figure 13 shows the actual calibration for the unit.

The final subassembly is shown in Figure 14 before potting and assembly. This sensor is used both in the reservoir-level sensing circuit (Figure 15) and in the accumulator circuit discussed in a later section.

1.3.1.5 Optical Desiccant Sensor

Some hydraulic systems (such as the A-6E) are pneumatically pressurized, utilizing regulated engine compressor bleed air.

A desiccant is used to dry the makeup air used to pressurize the reservoir. The cartridges are replaced on periodic intervals predicated on vehicle system usage. In order to remotely detect a saturated condition, a colored desiccant cartridge is placed in series with the existing unit since the latter could not be readily modified.

The selected sensor was made by Delaval Special Products Division and conforms to Grumman Specification Number 205. The sensor measures approximately 5 in. x 3 in. long, has a transparent housing, and is rated for 100 psi operating pressure. The unit

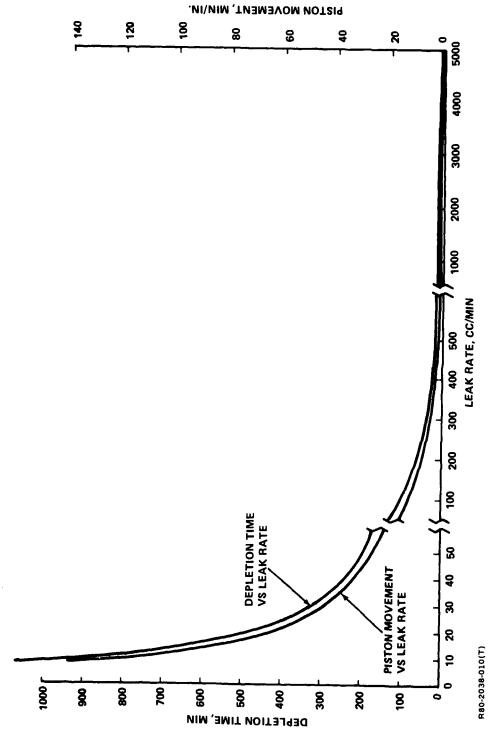
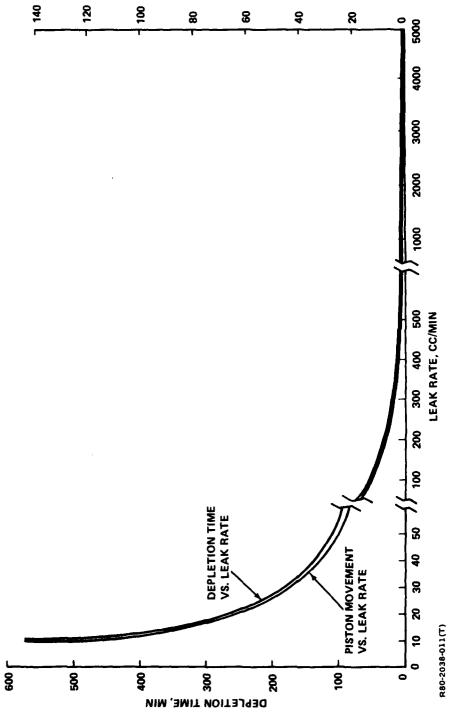


Figure 10. Combined reservoir depletion rate vs time.

PISTON MOVEMENT, MIN/IN.



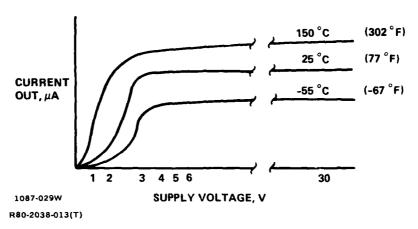


Figure 12. Voltage-current plot for an IC transducer.

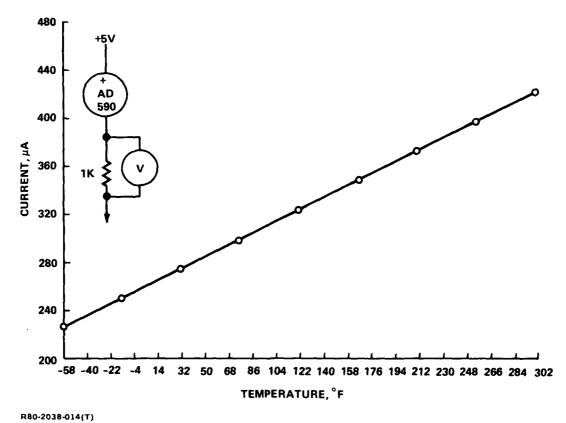
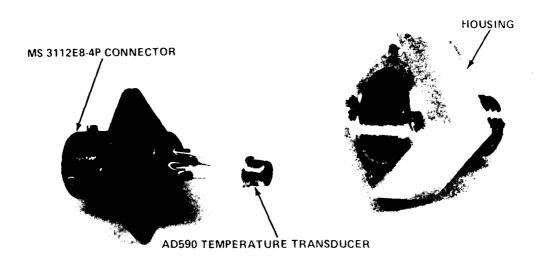


Figure 13. Calibration curve for an IC transducer.



R80-2038-015(T)

Figure 14. Temperature transducer assembly.



Figure 15. Reservoir temperature sensor installation.

contains approximately 2.6 in.³ of dyed silica gel conforming to Military Specification MIL-D-3716, Type IV. The initial color of the desiccant is deep to pale blue, depending on the desiccant condition. The color changes from pale blue to pink as the unit becomes saturated.

Reading desiccant condition remotely is accomplished by using reflected colored light from the irregular desiccant granules through the transparent housing. Figure 16 shows the concept employed to accomplish this objective.

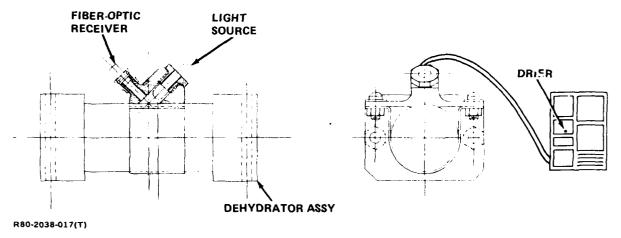


Figure 16. Optical desiccant sensor (early approach).

Initial test results revealed that a major portion of the light was being reflected by the transparent housing since the light transmitter and receiver were on the same axis. The light source transmitter-receiver angle was changed from 13° to 30°. No substantial improvements were noted. Various reflected angles were tested with the transmitter and receiver perpendicular to the desiccant housing axis in order to determine the maximum reflected light. This condition occurred with an included angle of 30 degrees between the transmitter and receiver. A second sensor housing (Figure 17) was originally made to support the grain of wheat light source and the fiber-optic terminal receiver. Subsequent testing revealed that color transmission became apparent but the intensity was not discernable to the viewer at the display panel.

Additional development effort dictated that the light source be brought closer to the transparent housing in order to increase the intensity of reflected light. A light source with a condensing lens was obtained to focus the light rays to one point. This change improved the reflective properties but, due to the irregular shape of the desicant, the reflected light scatters in many directions and makes reflected colored light

difficult. As a final attempt a condensing lens was used on the reflected light source to intensify the reflected color.

The light source for the sensor was originally a grain-of-wheat bulb, but its intensity after passing through the desiccant was not strong enough to be seen at the display panel. The grain-of-wheat bulb was then replaced by a General Electric No. 2701

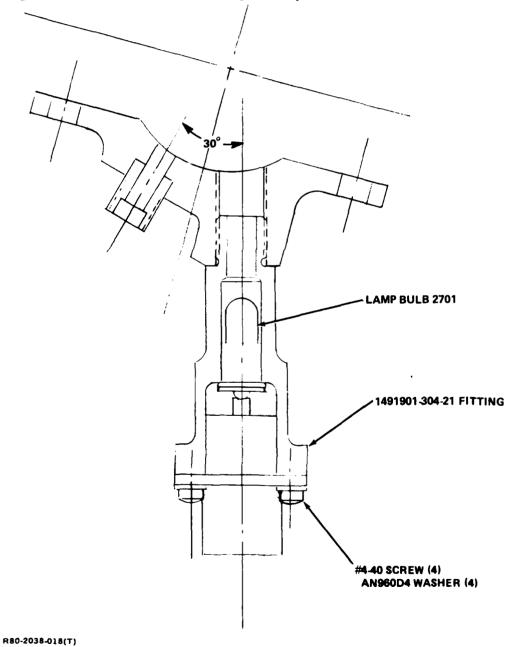


Figure 17. Sensor assembly.

halogen lamp requiring an operating voltage of 3.5 VDC and developing a maximum of 3.5 W, increasing the intensity by a factor of 20. Figure 18 shows plots of voltage, current, and power versus light intensity of the grain-of-wheat bulb; similar plots for the halogen bulb are shown in Figure 19. A comparison of the power versus light intensity of the grain-of-wheat and halogen bulbs is given in Figure 20.

ven with the halogen lamp, the reflected color properties were affected by the irregular angles of the desiccant crystals. Figure 21 shows the interim desiccant sensor installation. A decision was made to eliminate the desiccant and develop a moisture sensor. After several laboratory attempts, a disc was developed.

The desiccant sensor is a mixture of potassium bromide and cobaltous chloride, in a two-to-one ratio by weight, respectively. A description of the two components used in the desiccant is given in Table 2 (extracted from Ref. 2). The mixture is compressed into a half-inch diameter disc under a pressure of 22,000 psi and a vacuum of 25 in. mercury for 2 min. In order to focus the translucent disc color to a narrow point, a condensing lens was used adjacent to the disc support.

The lens is a condensing plano-convex lens Stock No. 10.0015 made by Rolyn Optics Company, Arcadia, California. The lens is made of spectacle crown glass (B-270) having a diameter of $0.295 \pm .02$ in. and a focal length of 0.512 in. $\pm 5\%$, as shown in Figure 22. The power of this lens is the reciprocal of the focal length, which gives a power of approximately 2 in. $^{-1}$ or 76.9 diopters.

The lens and desiccant disc are mounted inside the cartridge by a slide type assembly, shown in Figure 23. The slide is secured in position by the gasket, screen filter, and felt rings in the end covers. The complete assembly is coupled with two through bolts.

Since no suitable halogen bulb lamp holders were available, one had to be designed and fabricated to support the bulb and provide the proper mechanical/electrical interface. The resultant design was the 1491-304-21 optical desiccant fitting shown in Figure 24. A modified MS connector supplied power to the lamp. In order to reduce the voltage from 5 VDC to approximately 3.5 V, a 20-Ohm, 5-W resistor was used in the mating connector.

Specifications for the light source are as follows:

- GE Lamp Number 2701
- Voltage 3.5 V

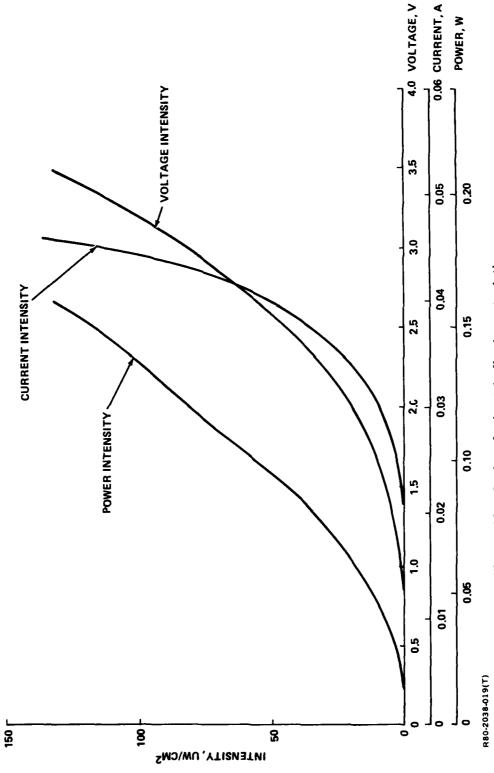


Figure 18. Grain-of-wheat bulb characteristic.

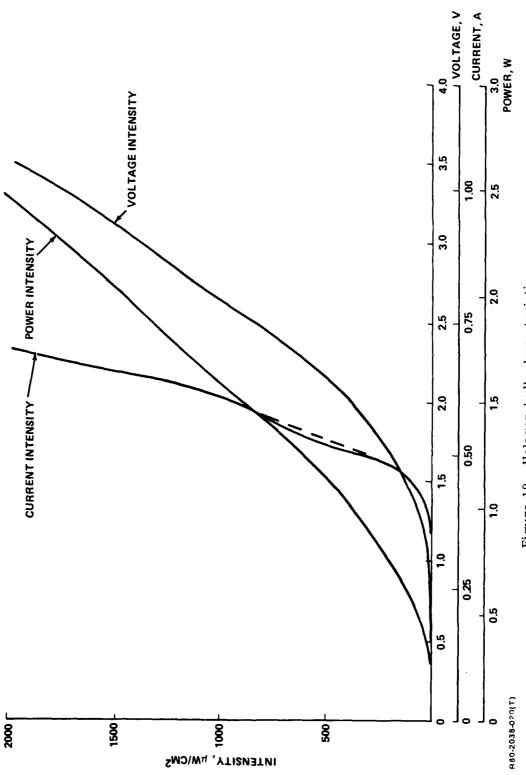


Figure 19. Halogen bulb characteristic.

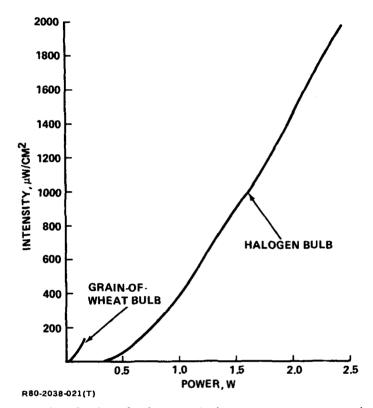


Figure 20. Grain-of-wheat bulb/halogen bulb comparison.

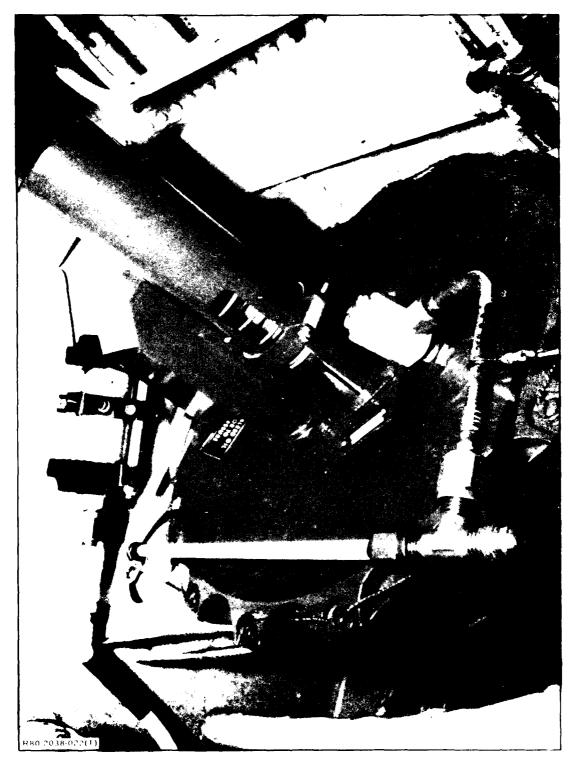


Figure 21. Interim desiceant sensor installation.

TABLE 2. DESICCANT COMPONENTS.

POTASSIUM BROMIDE, KBr	COBALTOUS CHLORIDE (COBALT CHLORIDE (A) CoCl ₂ (B) CoCl ₂ 6H)
PROPERTIES: WHITE, CRYSTALLINE GRANULES OR POWDER; PUNGENT, STRONG, BITTER SALINE TASTE; SOMEWHAT HYGOSCOPIC. SOLUBLE IN WATER AND GLYCERIN; SLIGHTLY SOLUBLE IN ALCOHOL AND ETHER; SP GR 2.749; M.P. 730°C; H.P. 1435°C.	PROPERTIES: (A) BLUE (B) RUBY-RED CRYSTAL. SOLUBLE IN WATER AND ALCOHOL; ALSO SOLUBLE IN ACETONE. SP GR (A) 3.348 (B) 1.924; M.P. (A) SUBLIMES (B) 86.75°C.
DERIVATION: SOLUTIONS OF IRON BROMIDE AND POTASSIUM CARBONATE ARE MIXED AND HEATED THE SOLUTION FILTERED AND CONCENTRATED AND THE BROMIDE CRYSTALLIZED OUT.	DERIVATION: BY THE ACTION OF HYDRO-CHLORIC ACID ON COBALT, ITS OXIDE, HYDROXIDE OR NATE. CONCENTRATION GIVES (B) AND DEHYDRATION (A).
GRADES: TECHNICAL, C. P. N.F.; REAGENT; SINGLE CRYSTALS. HAZARD: MODERATELY TOXIC BY INGESTION AND INHALATION.	USES: ABSORBENT FOR AMMONIA; GAS-MASKS; ELECTROPLATING, SYMPATHETIC INKS, HYGROMETER IN SOILS AND ANIMAL FEEDS; VITAMIN B ₁₂ ; FOR MAGNESIUM REFINING; SOLID LUBRICANT; MORDANT; CATALYST; BAROMETERS.
USES: MEDICINE; PHOTOGRAPHY (GELATIN BROMIDE PAPERS AND PLATES); PROCESS ENGRAVING AND LITHOGRAPHY; SPECIAL SOAPS, LABORATORY REAGENT.	

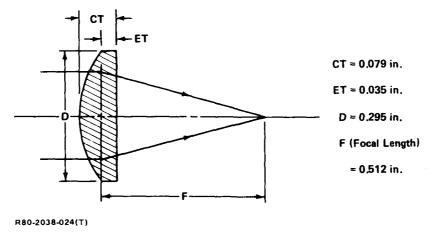


Figure 22. Plano-convex lens.

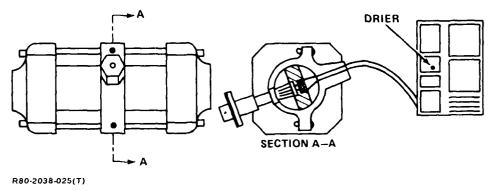


Figure 23. Moisture detector fiber-optic circuit.

•	Power	•	•	•	٠	•	•	•	•	•	•	•	•	•	•	•	2.5 W
•	Life	•	•	•	•	•						•	•	•			20 hr
•	Bulb Type	•	•	•	•	•	•	•	•			•	•	•	•	•	TL 1/2
•	Dimensions																0.625 x 0.285 in.

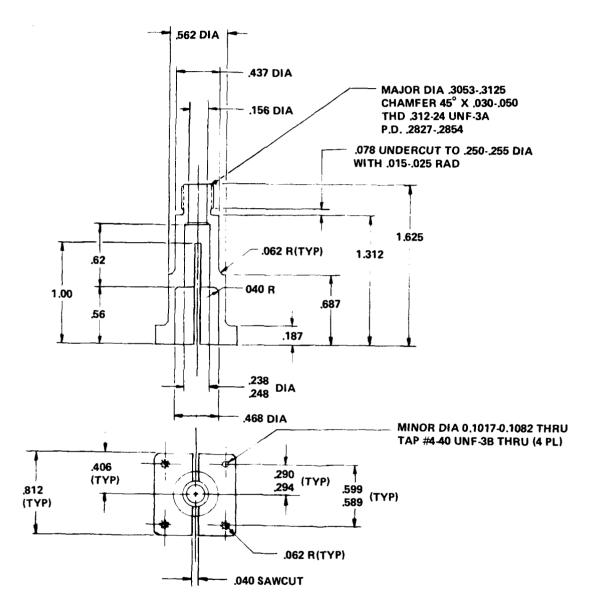
Desiccant Fiber-Optic Link. In an effort to improve visibility at the display, power optical measurements were taken using a recently purchased Photodyne Model 22XL optical multimeter. The results indicated that the cable running from the optical sensor to the display unit had an unsatisfactory 32 db/m optical loss instead of 10 db/m, which would normally be expected with a properly installed line run. The fact that the cable run was installed during vehicle buildup precluded improvements in this area.

1.3.2 Pneumatic Bottles

1.3.2.1 Description

Pneumatic bottles are energy storage devices which are used as an emergency backup to a principal system. Servicing these bottles requires that the maintenance technician compensate for topping pressure as a function of ambient temperature. A typical nitrogen bottle service card is shown in Figure 25 (Ref. 3).

In this flight test program, two of the eight stored energy sources were modified to accept HYCOS sensors. One landing gear door dump bottle (Figure 27) was modified to accept a temperature-compensated pressure switch and a fiber-optic liquid detection circuit. The second emergency canopy dump bottle (Figure 26) was modified to accept another temperature-compensated pressure switch. Special fittings were manufactured to provide sensor bosses.



-21 FITTING

MATERIAL: AI ALLOY 7075-T73

FINISH: BLACK ANODIZE PER MIL-A-8625 TYPE II

R80-2038-026(T)

Figure 24. No. 1491901-304-21 optical desiccant fitting.

A-1	13	Mñ.	4[8 e:	01-85ADA 1 Decemb			CrANGE NO.	PHASE A	ici FaR On
];; ==EA	#04.00 0000		OR	TIME 01:30	RIG AMH NO. 1	195. 6053 NO. 1	LANDING GEAR EME	RGENCY OPERATIONAL CHECK	CONSTRUCT NA
				WARNI	Power Power Trail Wrend Fluid NG: Insure	er, External Source, Elec Source, Hydr er, Nitrogen h, Torque (0- CC Hydraulic wheel well a	tric aulic 150 in-1b) NSUMABLES/REPLACEM reas are clear of	AMH-4 HT REQUIRED 128GT10154 515R100	(90.0 Min) (90.0 Min)
2,4/5						-		em IAW NA 01-85ADA-2-2.2, rvicing, swivel nut torque	
1,4/9				2. S	ervice land	ing gear emer	gency extension bo	ttles IAW NA 01-85ADA-2-1,	SECT 6.
								(End of Card Card A-13.1 Blank)
R80-20	38-027(T)		· · · · · · · · · · · · · · · · · · ·					

Figure 25. Typical service card.

1.3.2.2 Temperature-Compensated Pressure Switch

At the onset of the program, it became evident that temperature-compensated pressure switches were not off-the-shelf hardware. NeoDyn Incorporated of Chatsworth, California, was contracted to develop and build temperature-compensated pressure switches for the hydraulic monitoring system program. An initial Grumman sensor specification (Number 204) was prepared.

Switch Description. The switch is an all-welded, hermetically sealed unit which physically conforms to Figure 28. The switch senses applied pressure and compares it to an internal sealed self-contained reference pressure within the probe, which is at the same temperature as the sensed media. A proprietary, welded stainless-steel sensing diaphragm is exposed to the probe reference pressure on one side and to the sensed pressure on the other side. Pressure settings, which vary as a function of sensed and reference pressure, are accomplished through a force balance interaction between a sensing diaphragm and a Belleville spring reference load. Since the reference pressure varies directly with sensed temperature, pressure settings are a function of temperature. Variation of reference pressure with temperature is shown graphically in Figure 29.

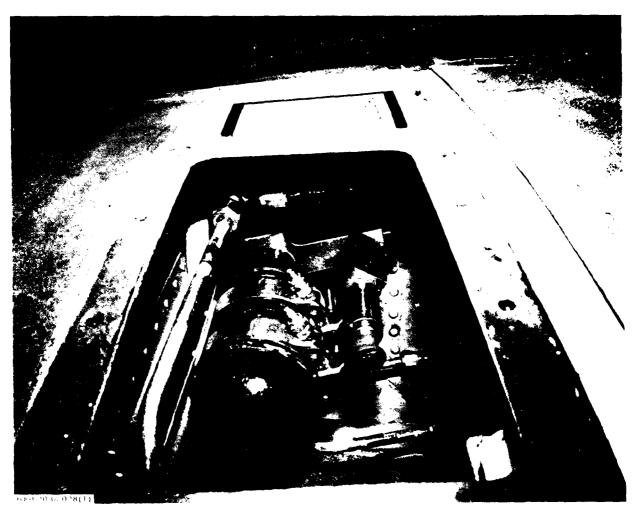


Figure 26. Emergency canopy dump bottle installation.

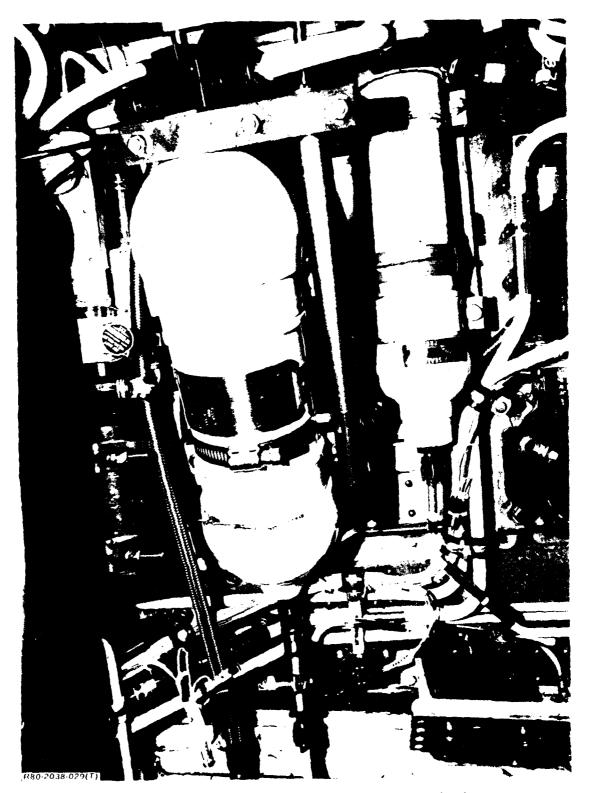


Figure 27. Landing gear door dump bottle installation.

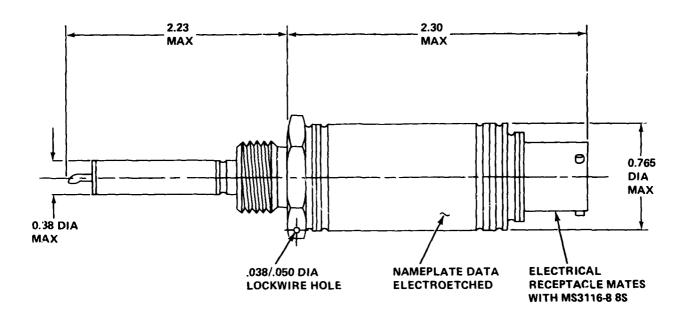




Figure 28. Temperature-compensated pressure switch.

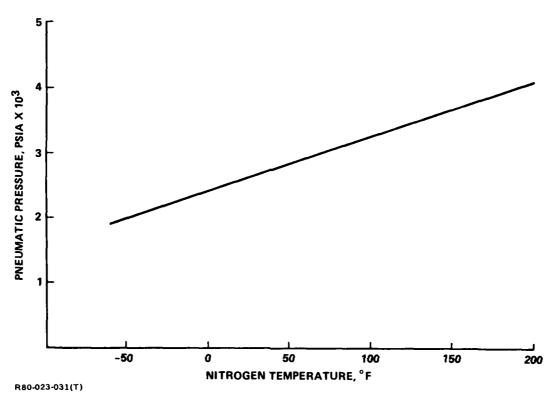


Figure 29. Plot of pressure vs temperature for nitrogen.

A precision snap-action electrical switch exposed to sensed pressure is positioned within the mechanism stroke limits to provide electrical circuit control at predetermined differences between sensed and reference pressure. The complete assembly is housed within an all-welded, high-pressure hermetically sealing housing. Figure 30 shows the diagrammatic circuit.

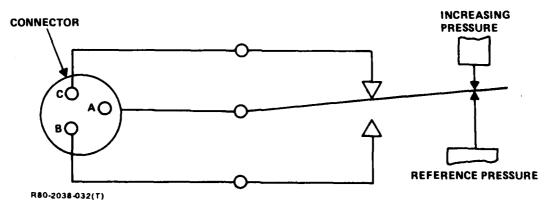


Figure 30. Temperature-compensated pressure switch: diagrammatic circuit.

Laboratory testing of a penumatic charge at variable temperatures verified the pressure switch temperature concept. Data for this switch (Grumman specification 204-1) is shown in Figure 31.

The reference temperature compensating gas is dry nitrogen that is hermetically sealed within the unit.

Switch Testing. Switch testing was conducted and found to fall within acceptable limits as defined by source control specification 204-2. The test results are listed in Table 3 and plotted in Figure 32.

1.3.2.3 Fiber-Optic Liquid Detection Circuit

The fiber-optic fluid detection circuit employs the properties of refractive index. If a diagonal gap exists between two fibers, light transmission will not jump the gap and will be absorbed by the core. In the presence of suitable fluid, the light will pass through the fluid and appear at the display panel. Water will be indicated by a white light and hydraulic oil will appear as a red light.

The liquid detector concept uses the optical properties of the light-conducting media. It is necessary to determine not only the properties of the light-conducting cables but also those of the fluids.

One of the important parameters of any fluid or light-conducting medium is its refractive index, defined as the ratio of the velocity of light in air to that in a given

- ACTUATION POINTS (SEE GRAPH)
- INCREASING PRESSURE: BY "A" MAX
- DECREASING PRESSURE: WITHIN BAND "B-C"

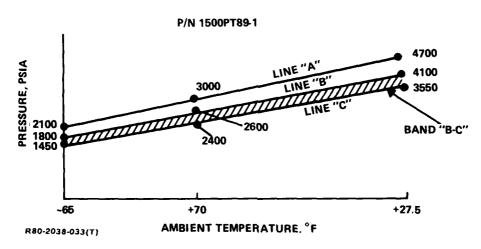
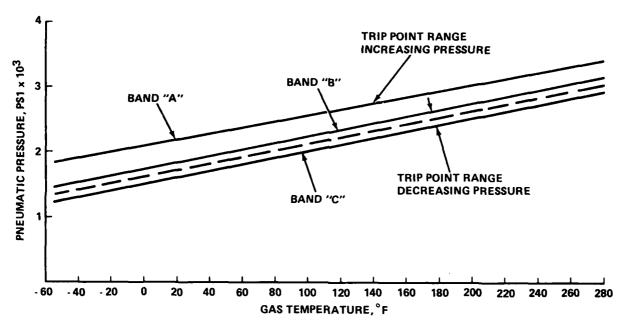


Figure 31. Switch actuation points vs temperature (Specification 204-1)

TABLE 3. TEMPERATURE-COMPENSATED PRESSURE SWITCHES (GRUMMAN SPECIFICATION 204-2).

P/N 1500 PT89-2, S/N 001								
ANDIENT	+69°F	1950 PSIG						
● AMBIENT	69°F	2000 PSIG						
	273°F	3000 PSIG						
• нот	275°F	3000 PSIG						
	-48°F	1525 PSIG						
● COLD	−55°F	1325 PSIG						
;	P/N 1500 I	PT89-2, S/N 002						
AAADIFAIT	69°F	INCREASING PRESS. TRIP	2025 PSIG					
● AMBIENT	TO 73.5° F	DECREASING PRESS. TRIP	1975 PSIG					
• corp	−64.5°F TO	INCREASING PRESS. TRIP	1450 PSIG					
• COLD	−68°F	DECREASING PRESS. TRIP	1175 PSiG					
	+274.5°F	INCREASING PRESS. TRIP	3020 PSIG					
● HOT R80-2038-035(T)	TO +272°F 	DECREASING PRESS TRIP	2960 PSIG					



A. P/N 1500 PT 89-2, S/N 001

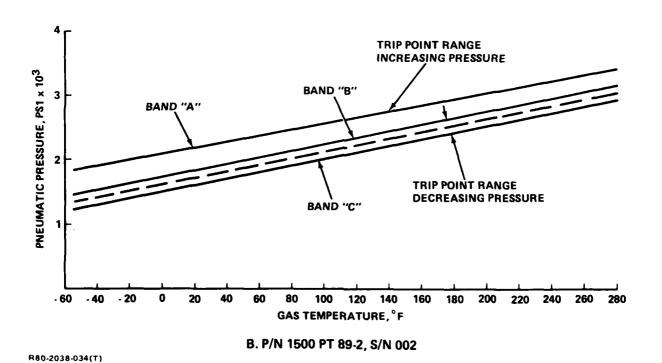


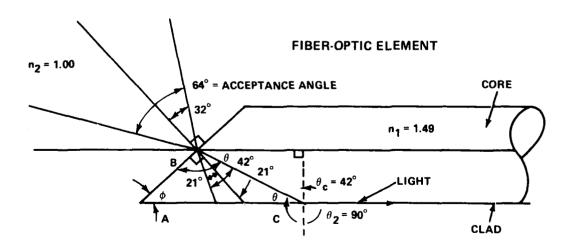
Figure 32. Switch actuation points vs temperature (Grumman Specification 204-2).

solid or fluid taking into account the angle at which the light beam travels. Willebrond Snell's Law of Sines states that the index of refraction is a constant, equal to the sine of the angle of incidence divided by the sine of the angle of refraction. Table 4 lists the refractive indices of various materials.

TABLE 4. REFRACTIVE INDICES OF VARIOUS ELEMENTS.

• WATER: 1.330	● MIL-H-83282 — 1.456
• AIR: 1.003	● MIL-H-6083 — 1.468
• MIL-H-5606: 1.463	
• CROFON (DUPONT)	• CABLE, FIBER-OPTIC TRANSMISSION
- CORE: 1.490	- CORE: 1.62
- CLAD: 1.392	- CLAD: 1.52
• LUCITE/PLEXIGLASS: 1.51	
R80-2038-036(T)	

During the course of development, it became apparent that a single large-diameter fiber would be placed within the pneumatic bottle to detect the presence of a liquid, using the properties of the liquid for light coupling. The fiber angle in which a light ray would be lost when traveling through the conduit, unless the presence of water and/or hydraulic oil were available to permit optical coupling, was then derived mathematically. An analysis of the derivation follows:



$$\frac{\sin \theta_{c}}{\sin \theta_{2}} = \frac{n_{2}}{n_{1}}$$

$$\sin \theta_2 = \frac{n_1}{n_2} \sin \theta_c$$

$$\sin 90^{\circ} = \frac{n_1}{n_2} \sin \theta_c$$

$$\frac{\sin 90^{\circ}}{\sin \theta} = \frac{n_1}{n_2}$$

$$\frac{1}{\sin \theta_{c}} = \frac{1.49}{1.00}$$

$$\sin \theta_{c} = \frac{1.00}{1.49} (1)$$

$$\theta_{\rm c} = \sin^{-1} \frac{1.00}{1.49} = 42^{\circ}$$

$$\theta = 90^{\circ} - \theta_{c}$$
 $\angle A = \phi$ $\angle B = 90^{\circ} + 21^{\circ}$

$$\theta = 90^{\circ} - 42^{\circ}$$
 $\angle C = 0$

$$\Delta ABC = \theta + (90^{\circ} + 21^{\circ}) + \phi$$

$$180 = \theta + (90^{\circ} + 21^{\circ}) + \phi$$

$$180 = 48 + 90 + 21 + \phi$$

Any beveled cut less than 21° will result in having light absorbed by the core.

Definitions

 $\theta_{\rm c}$ = critical angle

light guide.

 ϕ = angle required (beveled cut angle)

Since θ_{c} (63°) exceeds the critical angle

(42°), light will be transmitted through the

n = refractive index

 θ = angle used in solving ϕ

Assume $n_2 = 1.33$ (index of refraction for water)

$$\sin \theta_{\rm C} = \frac{1.33}{1.49}$$

$$\theta_{\rm C} = \sin^{-1} \frac{1.33}{1.49} = 63^{\circ}$$

$$180^{\circ} = \theta + (90^{\circ} + 21^{\circ}) + \phi$$

$$180^{\circ} = 27^{\circ} + 90^{\circ} + 21^{\circ} + \phi$$

 ϕ = 42°; beveled angle is increased, resulting in light being transmitted.

$$\sin \theta_{C} = \frac{1.4635}{1.49}$$

$$\theta_{c} = \sin^{-1} \frac{1.46}{1.49} = 79.2^{\circ}$$

Since θ_c (79.2°) exceeds the critical angle (42°), light will be transmitted through light guide with a <u>MIL-H-5606</u> coupling.

It has been shown in the laboratory that this approach works in the presence of either fluid. However, instead of using one multistrand fiber-optic cable it became necessary to employ two single-fiber cables with an external light source, with the flexible sensing probe at the bottom of the bottle. Figure 33 shows the concept of an early liquid sensor (Ref. dwg 1491901-307). This approach had screw-on terminals attached to the fiber-optic cables at both the sensing proble and a lucite conductor. The lucite conductor provided an optical means of passing light out of the pneumatic bottle while still retaining the pressure seal. This method proved unacceptable as losses through the fittings and connectors were so drastic that no detectable amount of light could be found at the output fiber. Modifications were made and all unnecessary connectors removed. The result was a design which had one continuous fiber carrying inputted light, a gap allowing fluid detection, and another continuous fiber carrying outputted light. This design (Figure 34) combined the sensor with the fiber-optic cables and greatly reduced transmission losses.

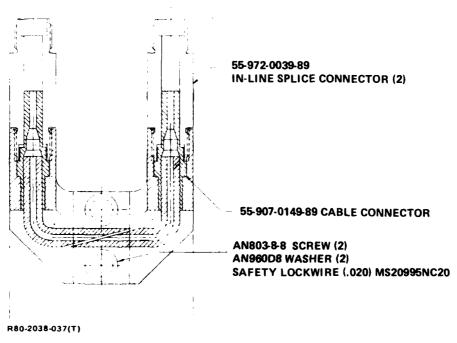
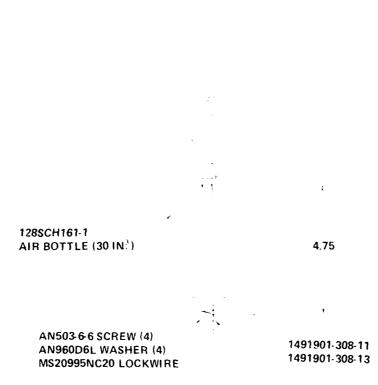


Figure 33. Liquid sensor assembly (early version).



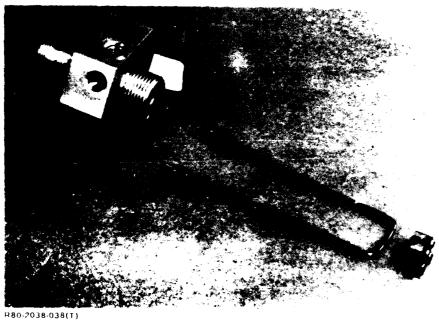


Figure 34. Liquid sensor assembly (improved version).

Two types of fiber-optic cables were purchased from Valtec Corporation, West Boylston, Massachusetts. The transmission cables were of the bifurcated and the single cable types. The bifurcated cabled type is used on the pneumatic bottle detection loop, whereas the single cable is used on the desiccant color-detection circuit.

Some of the parameters include:

• Number of fibers: 222-234

• Fiber diameter: 0.0031

Bundle diameter: 0.045

Acceptance cone angle: 68°

Cone index of refraction: 1.62.

Additional cable information is provided in Appendix B, Specification No. 206. All cables use fiber-optic connectors in accordance with MIL-L-85044/1, developed by the Naval Ocean Systems Laboratory in San Diego, California. MIL-L-85044/1 covers pressurized bulkhead connectors, Type 1, for relatively low-pressure systems. These stainless steel connectors were manufactured and supplied by the Sealectro Corporation in Mamaroneck, New York.

The cable terminal ends were installed in accordance with the procedure specified on Page 6 of MIL-C-85044 using an epoxy bonding agent to fasten the assembly together.

Properties of Crofon Light Guides. Crofon is a Dupont registered trade name for plastic fiber light guides. The data in Table 5 were taken from a Dupont publication on Crofon Fiber Optics (Ref. 4) and a Machine Design article (Ref. 5). Table 5 shows some properties of the Crofon Fibers and their polyethylene jackets. Figure 35 shows a light ray entering the light guide.

Transmission of light through Crofon varies as a function of length. It is also dependent on input light intensity, output light interfaces, and any gap through the optic circuit. Figure 36 shows the transmission efficiency of white light through fully polished light guides.

Single bends are employed in the liquid detection circuit at the sensor end. It is desirable to ascertain the minimum bend radius for the single 1056 light guide. Too severe a bend will cause a significant light loss due to degradation of the cladding fiber itself. Figure 37 shows typical light transmission for several grads of Crofon light

TABLE 5. PROPERTIES OF CROFON FIBERS WITH POLYETHYLENE JACKETS.

A. IDENTIFICATION: CROFON 1056

• NUMBER OF FIBERS:

1

• CRITICAL ANGLE: 69°

• OD:

DOLAMETED

0.111 $\pm .005$ IN.

• INDEX OF REFRACTION:

• FIBER DIAMETER:

0.056 IN.

- CORE N_D ≈ 1.490

JACKET MATERIAL:

POLYETHYLENE

- CLAD N_D ≈ 1.392

• FIRER

001 V445T11V4 145T114 00V

OPERATING TEMPERATURE

POLYMETHYL METHACRYLATE

LIMITS:

• ACCEPTANCE ANGLE: 64°

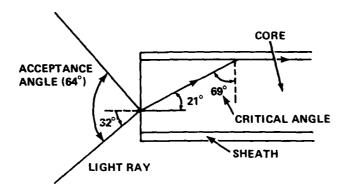
-40 °F TO 175 °F

B. TYPICAL PROPERTIES OF POLYETHYLENE

ASTM TEST	PROPERTY	LOW DENSITY	MEDIUM DENSITY	HIGH DENSITY	ULTRAHIG MOLECULA WEIGHT
	PHYSICAL				
D792 -	SPECIFIC GRAVITY SPECIFIC VOLUME (IN. 3/LB)	0.910-0.925 30.4-29.9	0.926-0.940 29.9-29.4	0.941-0.965 29.4-28.7	0.928-0.941 29.4
D570	WATER ABSORPTION, 24 HR, 1/8-IN. THK (%)	√0.01	< 0.01	<0.01	<0.01
	MECHANICAL	<u>.</u>			
D638 D638	TENSILE STRENGTH (PSI)	600-2,300 90-800	1,200-3,500 50-600	3,100-5,500 20-1,000	4,000-6,000 200-500
D638 D785	TENSILE MODULUS (10 ⁵ PSI) HARDNESS, ROCKWELL R	0.14-0.38 10	0.25-0.55 15	0.6 - 1.8 65	0.20-1.10 55
D790 D256	FLEXURAL MODULUS (10 ⁵ PSI)	0.08-0.60	0.60-1.15	1.0-2.0	1.0-1.7
	(FT-LB/IN. OF NOTCH)	NO BREAK	0.5-16	0.5-20	NO BREAK
	THERMAL				
C177 D696	THERMAL CONDUCTIVITY (10-4 CAL-CM/SEC-CM ² -°C) COEF OF THERMAL EXPANSION	8.0	8.0-10.0	11.0~12.4	11.0
D648	(10 ⁻⁵ IN./IN C) DEFLECTION TEMPERATURE (F)	10-22	14-16	11-13	14
	AT 264 PSI AT 66 PSI	90-105 100-121	105-120 120-165	110-130 140-190	118 170
-	CONTINUOUS, NO-LOAD SERVICE TEMP (^O F)	180-212	220-250	250	-
	ELECTRICAL				
D149 D150	DIELECTRIC STRENGTH (V/MIL) SHORT TIME, 1/8-IN. THK DIELECTRIC CONSTANT	460-700	460-650	450~500	900*
	AT 60 Hz AT 103 Hz	2.25-2.35 2.25-2.35	2.25-2.35 2.25-2.35	2.25-2.35 2.30-2.35	 2.30-2.35
D150	DISSIPATION FACTOR	0.0002	0.0002	0.0003	0.0002
D257	VOLUME RESISTIVITY (OHM-CM) AT 73°F, 50% RH	1015	1015	1015	1015
D495	ARC RESISTANCE (SEC) OPTICAL	135-166	200-235	_	
D542	REFRACTIVE INDEX	1.51	1,52	1.54	
D1003	TRANSMITTANCE (%)	4-50	4-50	10-50	_
*kV/CM					
087-052	w				

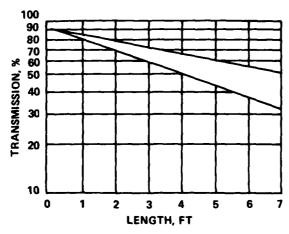
guides. It becomes evident that bend radius should be as large as possible to minimize transmission loss.

<u>Fiber-Optic Connectors</u>. Numerous types of fiber-optic connectors were considered for use in HYCOS. The major concern was the availability of a high-pressure bulkhead fitting capable of sealing 3000 psi pneumatic pressure. As of February 1978, no bulkhead connectors on the market were capable of withstanding this high pneumatic pressure differential without leakage.



CORE INDEX OF REFRACTION n_D = 1.490 SHEATH INDEX OF REFRACTION n_D = 1.392 R80-2038-040(T)

Figure 35. Crofon light guide properties.



NOTE: TRANSMISSION VALUES ARE FOR LIGHT GUIDES WITH CAREFULLY POLISHED ENDS.

R80-2038-041(T)

Figure 36. Transmissivity of Crofon light guides.

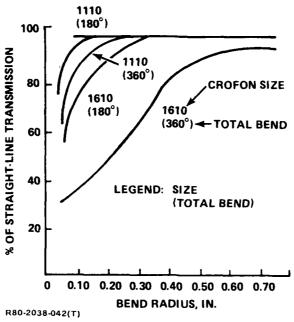


Figure 37. Effect of bend radius on light transmissivity.

Grumman was informed that the proposed MIL-C-85044/1 Connector, Fit ar-Optic, Pressurized Bulkhead, Type I, Class I was being manufactured by Sealectro Councillation, Mamaroneck, New York. Sealectro indicated that the connectors were in stock.

Sealectro part numbers and unit weights are:

• Cable Connector:	55-907-0149-89	0.1056 Oz
• In-Line Splice:	55-972-0039-89	0.1746 Oz
 Bulkhead Mounting Connector: 	55-975-0049-89	0.3527 Oz

All parts are made of corrosion-resistant stainless steel. Figure 38 shows a typical fiber-optic terminal used in HYCOS. The connector has a fiber terminal diameter of 0.0465 in. (area = 0.001698 in.²). For HYCOS, special connector interfaces were designed to withstand the intended environment. Figure 39 shows a Display Panel fiber-optic terminal.

<u>Pressure Seal</u>. In order to transport light through a pressure seal, it became necessary to design a seal that would satisfy system integrity and provide maximum light transmissivity. Concept Number One, shown in figure 40A, employed a transfer tube containing machined and polished clean acrylic rod for light transmission. Although



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Figure 38. Assembled fiber-optic connector.

initial pressure testing at 3000 psi revealed good results, the optical transmission properties were very poor. Almost all of the light generated at the outside source was lost due to the optical properties of the acrylic rod. A revised approach, shown in Figure 40B, eliminated the acrylic rod and utilized the fiber-optic cable up to the external connector interface. Initial testing revealed that the plastic tended to creep and extrude under prolonged exposure to pressure. Additional development effort overcame this problem and considerably improved the overall transmission efficiency. Limited operational cycling and proof testing verified this approach. No problems were encountered during the flight test program.

1.3.3 Hydraulic Pump/System

1.3.3.1 Flow Sensor Description

The flow sensor is a device placed in series with a hydraulic system or component which gives an external indication when a specific flow value has been exceeded under controlled conditions.

1.3.3.2 System Quiescent Flow Sensor

System quiescent flow values for the A-6E system were established at 0.5 to 1.5 gpm. This will vary depending on which system components are on the line during a no-input system demand condition. For the A-6E combined system, quiescent flow limits of 4.5±1 gpm were established as excessive internal flow.

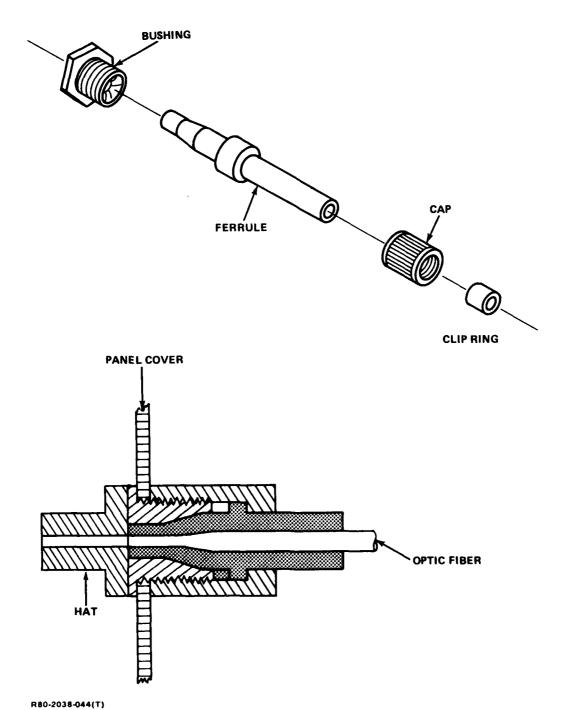
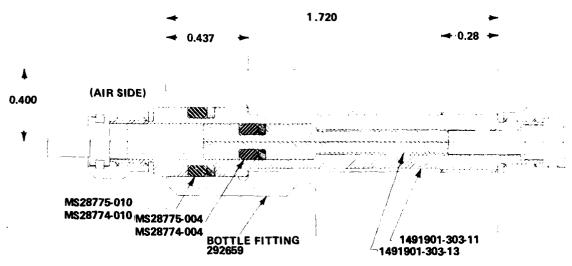
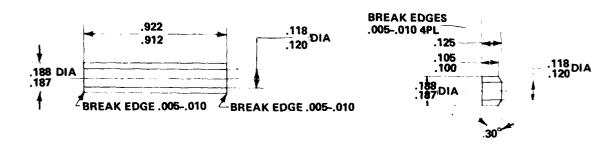
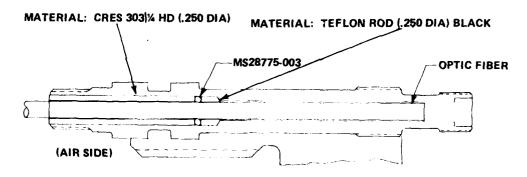


Figure 39. Display panel fiber-optic terminal.



A. PNEUMATIC HIGH-PRESSURE SEAL CONFIGURATION





B. IMPROVED HIGH-PRESSURE SEAL

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Figure 40. Pressure seal.

The system flow sensor incorporates an electrically actuated locking device which prevents indicator actuation during normal system flow demands. Under quiescent flow conditions, the flow is measured through a movable orifice. Flows beyond the required measured values are shunted across the movable orifice. Figure 41 shows a typical quiescent flowmeter used in the flight test program. Once the indicator trips due to excessive flow conditions, it must be manually reset.

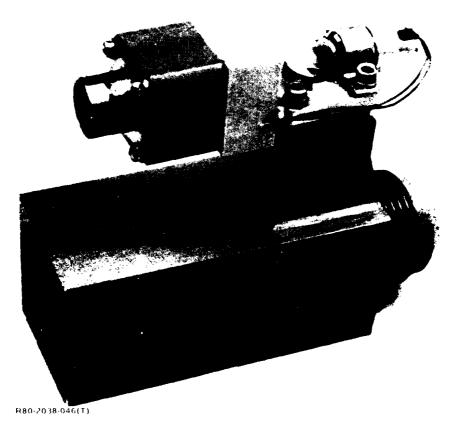


Figure 41. Quiescent flow sensor.

The flow sensor meters actual quiescent flow through a flow resistor that produces a desired differential pressure. The differential pressure, equated to a specific maximum permissible quiescent flow leakage, generates a signal. During normally higher system flow demand, the calibrated restrictor bypasses through additional flow passages at acceptable additional pressure differentials across the entire sensor.

Plant 14 Hydraulic Laboratory generated calibration data that produced the curve shown in Figure 42. The curve shows a trip point of 4.18 gpm which is within the design limits. It should be noted that the curve flattens out above 8 gpm.

The actual installation on the flight test vehicle is shown in Figure 43.

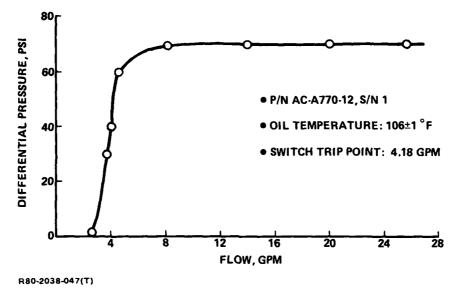


Figure 42. Calibration: flow sensor, bypass type, quiescent flow.

1.3.3.3 Pump Case Drain Flow Sensor

The pump case drain flow sensor is similar to the system quiescent flow sensor in design but does not incorporate a lockout device since pump case flow does not significantly vary over the hydraulic pump flow range. A failsafe bypass device is incorporated, however, to preclude high back pressure due to inadvertent momentary block liftoff. Excessive pump case flow was established at 1.25 to 1.75 gpm. Figure 44 shows a typical pump case flow sensor. A case drain flow calibration curve is presented in Fig. 45. Actual switch trip occurred at 1.47 gpm, Figure 46 shows a partially obscured installation in the A-6E test vehicle.

1.3.3.4 Rudder Actuator Quiescent Flow Sensor

Excessive rudder actuator internal leakage is detected by an in-line flow sensor located in the pressure line. The unit is similar in construction to the system quiescent flow sensor, but is sized for a lower flow. Since normal rudder actuator quiescent leakage rates are very low, a value of 0.625 to 0.875 gpm was selected for the A-6E rudder actuator. Figure 47 shows the rudder actuator quiescent flow sensor.

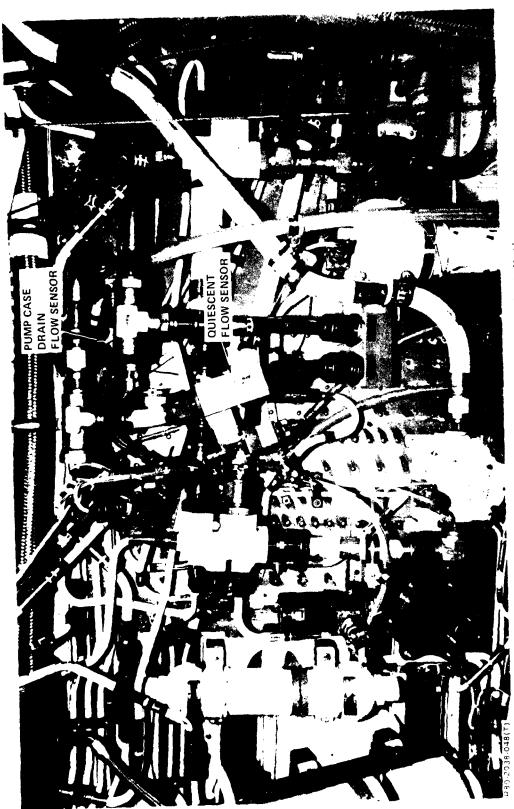


Figure 43. System quiescent flow sensor installation.

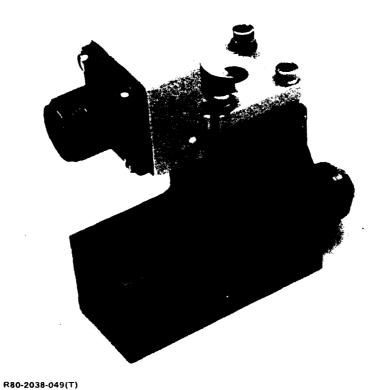


Figure 44. Pump case drain flow sensor.

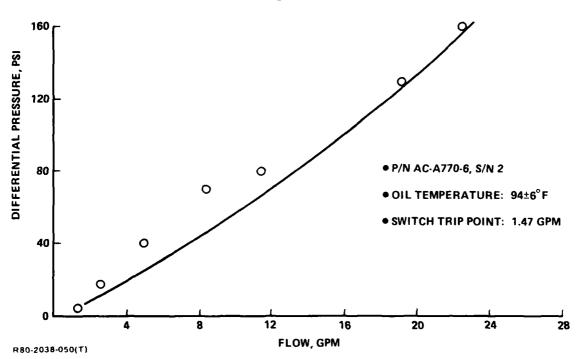


Figure 45. Calibration: pump case drain flow sensor, bypass type.

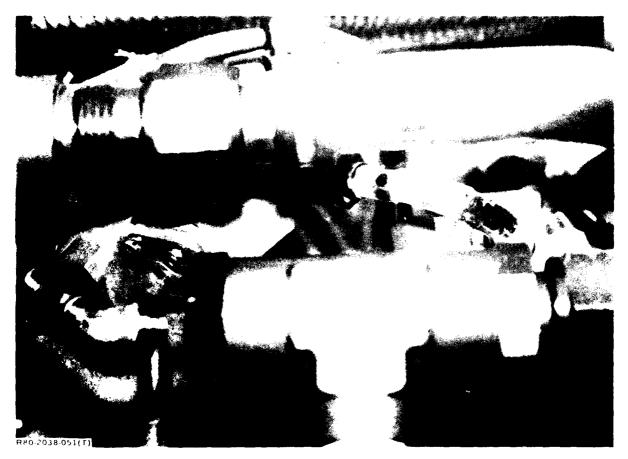


Figure 46. Pump case drain flow sensor installation.



R80-2038-052(T) Figure 47. Rudder actuator flow sensor.

Flow versus pressure drop data produced the curve shown in Figure 48. The installation is shown in Figure 49. Note that the sensor was installed in the pressure line.

1.3.3.5 System Pressure Switch

The system pressure switch serves two functions: it indicates low system pressure during system operation and provides panel circuitry to the flow sensors and elements.

The elapsed time meter on the panel is actuated by the pressure switch; the flow sensor circuits are dependent on the pressure circuit being on.

For this purpose, a switch (Figure 50) manufactured by Sigmanetics of Mountain Lakes, New Jersey, was incorporated. The switch weighs less than 0.085 lb and actuates on decreasing pressure of 2300 ± 100 psi. The switch installation is shown in Figure 51.

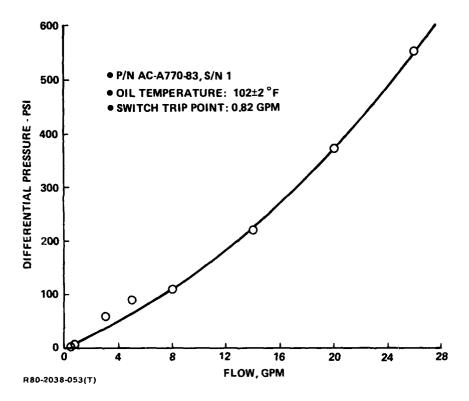


Figure 48. Calibration: rudder actuator quiescent flow sensor, bypass type.

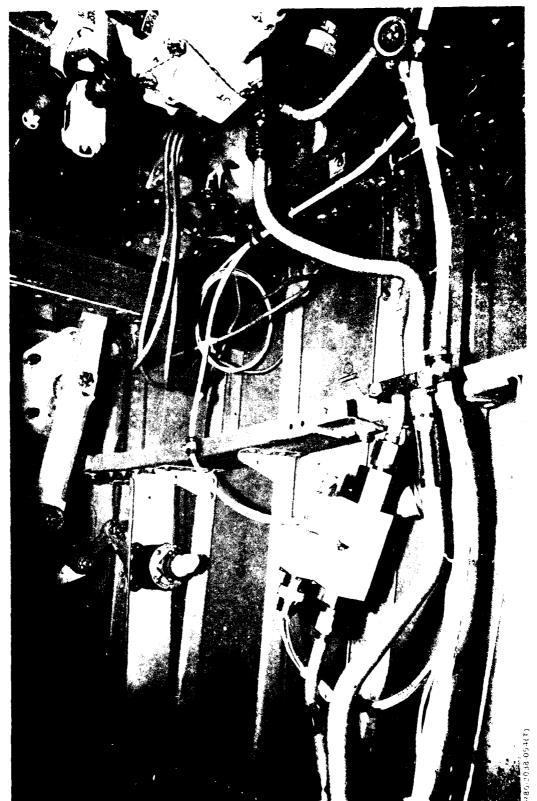


Figure 49. Rudder actuator quiescent flow sensor installation.

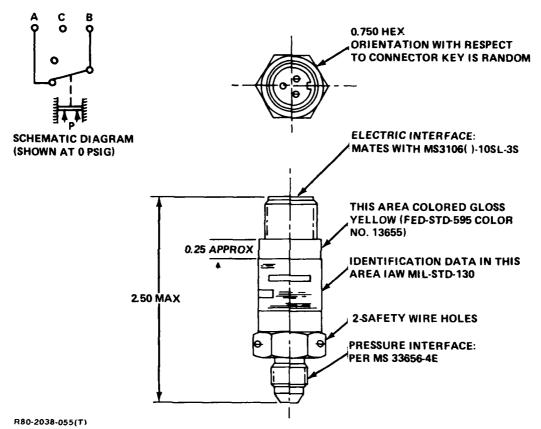


Figure 50. System pressure switch.

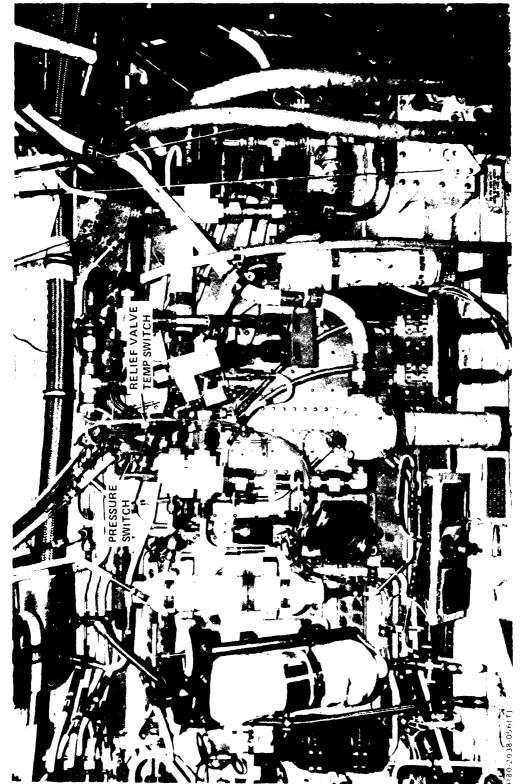


Figure 51. Relief valve temperature and system pressure switch installation.

1.3.3.6 Case Drain Flow Temperature Switch

Excessive case drain flow indicates hydraulic pump degradation, resulting in system fluid temperature rise. By installing a fluid temperature switch in series with the flow sensor, an excessive temperature limit can be detected.

Type II hydraulic systems operate at a 275° F maximum. A value of $300 \pm 20^{\circ}$ F was selected as the trip limit on a Texas Instrument Klixon manual reset temperature switch.

The switch was mounted to the case drain line near the pump by using a clamp-on adaptor. This switch must be manually reset after being tripped.

1.3.3.7 Relief Valve Leakage

Relief valve leakage was measured with a probe-type manual reset temperature switch as used to measure pump case drain flow. Trip setting for this switch was 300 ± 20°F.

Type II hydraulic systems operate at 275°F maximum. A value of 300°F was selected as the trip limit on a Neo-Dyne model 1103TR119 manual reset temperature switch.

The switch probe is immersed in the fluid flow and contains n-propyl alcohol as the sensing medium. Temperature sensing is accomplished by exposing a welded corrosion-resistant steel diaphram to changes in pressure created by expanding fluid in the probe. Figure 52 shows pressure versus temperature slot for this fluid at constant volume. Temperature settings are determined by a force-balance interaction between the sensing diaphragm and a snap-action Belleville spring system. An electrical switch assembly positioned within the mechanism's stroke limit provides electrical circuit control at predetermined temperatures. The manual reset button functions as both a visual indication and a mechanism reset after switch actuation. The temperature switch is illustrated in Figure 53. Installation is shown in Figure 51.

1.3.4 Hydraulic Accumulators

1.3.4.1 Description

Hydraulic accumulators are energy storage devices used in many aircraft hydraulic systems. They usually employ stored gas as the variable energy source. Their applications include hydraulic pump ripple attenuation, momentary system power overdemand conditions, and performance of emergency actuation functions such as deploying a ram air turbine via a hydromechanical actuator.

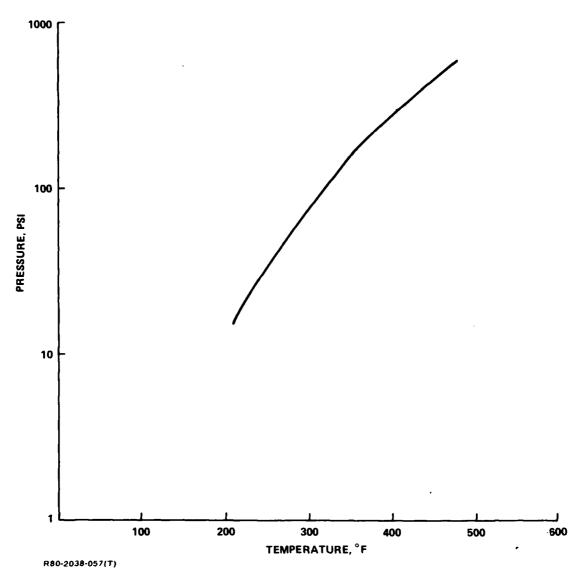


Figure 52. Pressure versus temperature of n-propyl alcohol at constant volume.

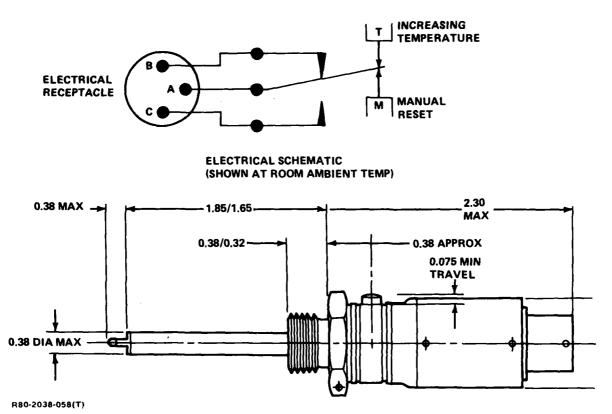


Figure 53. Manual reset temperature switch.

The work output is dependent on initial precharge pressure, precharge temperature, and delta volume change caused by piston movement under constant temperature conditions:

$$P_1V_1 = P_2V_2$$

and

$$W = \int_{V_1}^{V_2} P \, dv$$

If we consider an isentropic (no heat flow condition), then

$$W = K \int_{V_1}^{V_2} \left[\frac{dv}{V^{1.4}} \right]$$

Since the variables are precharge pressure, precharge temperature, and piston displacement, the piston displacement for a final hydraulic system pressure of 3000 psi is a function of initial precharge conditions (Ref. 6, NADC TR 75168-30-Pg 33).

This monitoring effort was initiated to develop a method of determining accumulator precharge irrespective of whether the accumulator is fully or partially discharged. The variables required to determine this condition are charging pressure, temperature, and piston displacement.

Figure 54 shows the variation of piston displacement versus precharge pressure for a 50 in³. accumulator. Figure 55 shows a plot of piston displacement versus precharge pressure versus temperature at constant 3000 psi pressure. Figure 56 is a nomograph developed to determine precharge pressure.

In order to measure accumulator piston displacement, precharge pressure (accumulator pressure), and precharge temperature, various methods were investigated to ascertain their suitability to accumulator applications. These specific sensing methods will be defined in subsequent paragraphs.

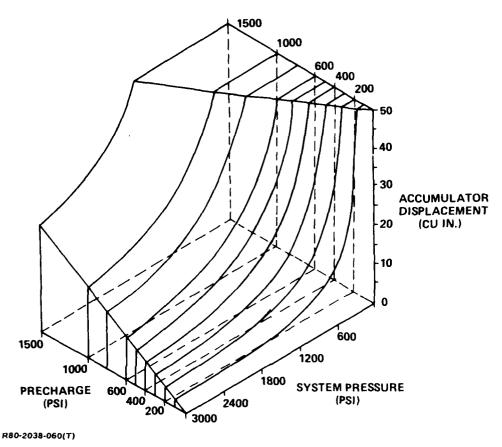


Figure 54. Accumulator piston displacement versus precharge and system pressures at constant (70°F) temperature.

1.3.4.2 Piston Displacement Sensors

Several methods of determining piston displacement within a pressurized accumulator were investigated. They include:

- A direct type in which a rod attached to the piston passes through a dynamic seal
- A reflected energy type which measures reflected IR energy from a movable surface.

The first direct type seemed to offer less development risk than the other method since the output could be processed easier with the microprocessor circuits. This direct type included a linear potentiometer with its axis parallel to the accumulator piston axis. By affixing the movable piston rod to the linear potentiometer, a direct

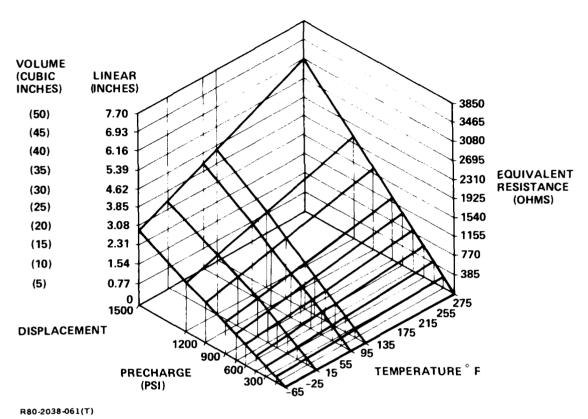


Figure 55. Accumulator piston displacement versus precharge pressure versus temperature at constant (3000 psi) system pressure.

relationship can be obtained by measuring resistance versus displacement. A 4 k Bournes potentiometer was chosen for this application. Figure 57 shows this configuration installed in the A-6E test vehicle. In order to provide for potentiometer extension clearances, the mounting bracket was offset.

Normally, it has been necessary to empty the fluid from the accumulator to measure precharge pressure. However, utilizing a newly developed equation involving system pressure, volume, temperature, and displacement it is now possible to determine precharge pressure without displacing the fluid. Displacement is expressed as a ratio of resistances measured by a linear potentiometer. The equation, graphically displayed in the nomograph of Figure 56, is derived as follows:

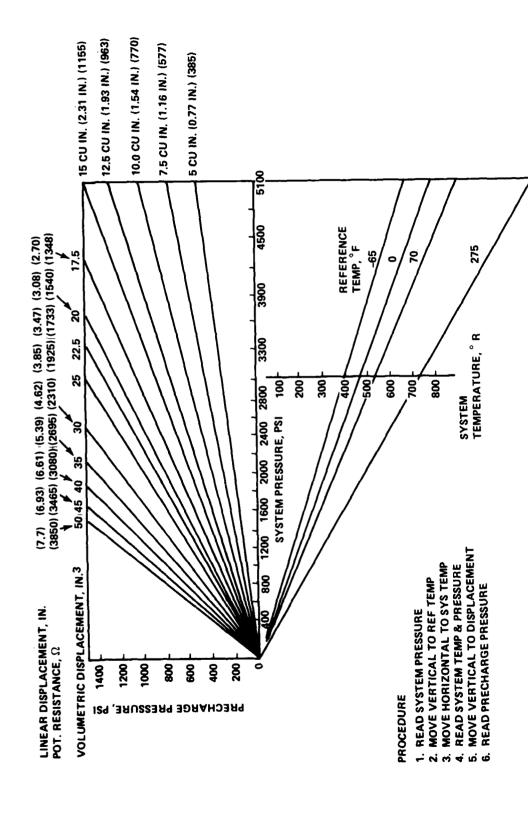


Figure 56. Precharge pressure nomograph.

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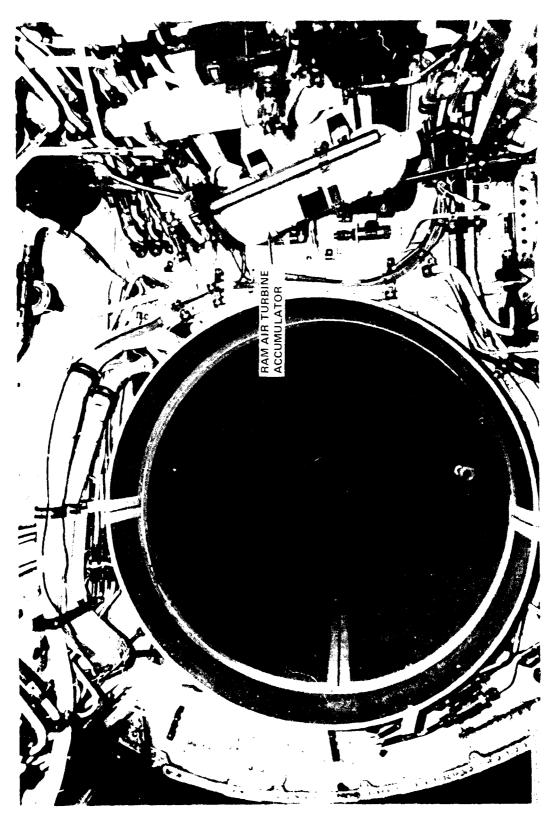


Figure 57. Ram air turbine accumulator installation.

$$\frac{P_1V_1}{T_1} = \frac{P_2V_2}{T_2}$$

$$P_1 = P_{\text{Precharge}} (P_{\text{pr}}), \quad V_1 = 50 \text{ in}^3., \quad T_1 = 70 \text{ °F} = 530 \text{ °R}$$

$$P_2 = P_{\text{system}} (P_{\text{sys}}), \quad V_2 = \text{Volumetric Displacement} = 50 \left(\frac{R}{3850}\right)$$

$$T_2 = (T_2 + 460) \text{ °R}$$

$$\frac{(P_{\text{pr}}) (50)}{530} = \frac{(P_{\text{sys}}) (50) (R/3850)}{(T_2 + 460) \text{ °R}}$$

$$(530) (P_{\text{sys}}) (50) (R/3850) = (P_{\text{pr}}) (50) (T_2 + 460)$$

$$P_{\text{pr}} = \frac{(530) (P_{\text{sys}}) (R/3850)}{(T_2 + 460)}$$

Another indirect method of determining piston position using reflected IR energy was investigated. This concept, shown in Figure 58, utilizes an external IR light source whose energy is reflected from the bottom side of the accumulator piston and picked up by an IR photodiode. Preliminary nonpressurized test results are plotted in Figure 59. It should be noted that the curve is relatively flat up to approximately 4 in. of stroke and then changes markedly. The test circuit wiring is shown in Figure 60.

1.3.4.3 Pressure Transducers

The Entran EPS-1032 (Entran Devices, Little Falls, New Jersey) miniature pressure transducer is a thread-mounted semiconductor strain-gage sensor which fits into a 10-32 UNF threaded boss. The transducer employs a face seal and has a full-scale output of 143 mV at 3000 psi pressure with 5 V input (room temperature). There is, however, a temperature shift when tested at -40 and 250°F. Calibration curves for this unit, shown in Figure 61, are very linear over the normal operating range (0-3000 psi). Sensitivity of the transducer is 0.0485 mV/psi. The unit is normally compensated for linearity by using an external compensation module from 80 to 180°F. The wiring diagram is shown in Figure 62.

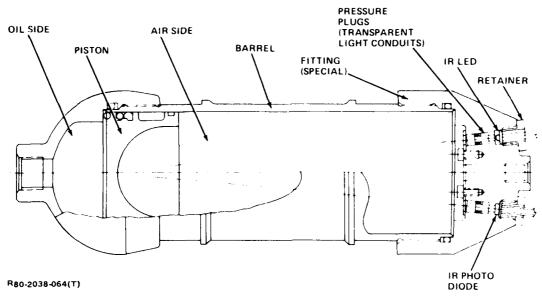


Figure 58. Photo-optic accumulator piston displacement sensor.

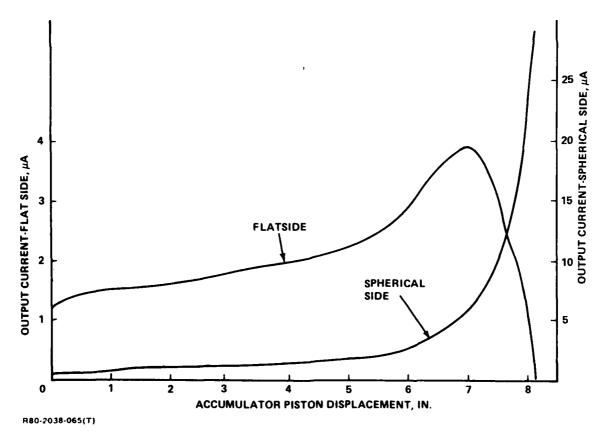


Figure 59. Photo-optic accumulator piston sensor test results.

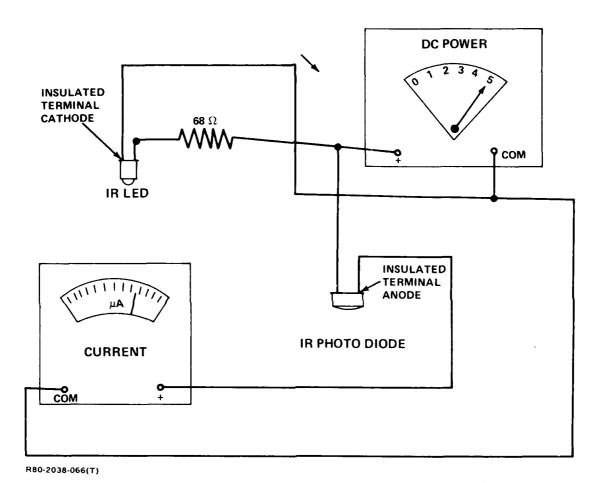


Figure 60. Photo-optic displacement sensor wiring diagram.

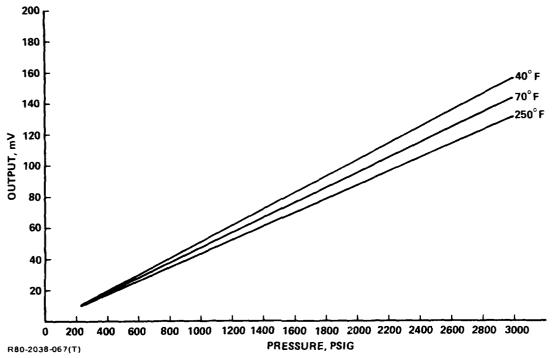


Figure 61. Entran transducer: output voltage versus pressure.

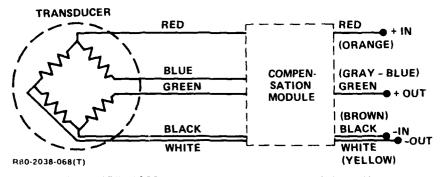


Figure 62. ESP-1032 pressure transducer wiring diagram.

Since the intended application encompassed broader temperature ranges, an extended calibrated temperature range was made. Table 6 shows performance data for the Entran ESP-1032 transducer. Envelope dimensions for a typical unit are shown in Figure 63 (Ref. 7).

TABLE 6. ENTRAN ESP-1032 TRANSDUCER DATA

MODEL: EPS -1032-2500 (.33), S/N 10 H8H-C1-1

• TYPE: MINIATURE PRESSURE • RANGE: 2500 PSIG

• EXCITATION: 6.0 TO 8.0 V

• OVERPRESSURE: 4000 PSIG

OPERATING TEMPERATURE: -60 TO 250 °F

• TEMPERATURE COMPENSATION: -60 TO 250 °F

• EXCITATION: 6 VDC

SENSITIVITY: 0.0469 mV/PSIG AT 77 °F

• THERMAL SENSITIVITY SHIFT, mV/100 °F: <± 2%/100 °F

 \bullet THERMAL ZERO SHIFT, mV/100 °F: $<\pm$ 1.5% FS/100 °F

• INSTALLATION TORQUE: 15 IN.-LB

• IMPENDANCE: INPUT: 430 Ω

OUTPUT: 239 Ω

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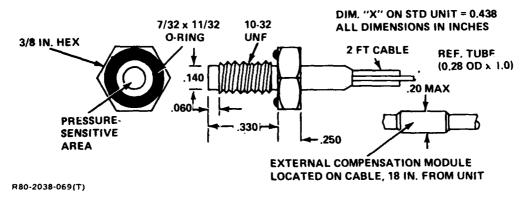


Figure 63. Pressure transducer envelope.

1.3.4.4 Temperature Sensor

The temperature sensor used in the accumulator circuit is the same as that used in the hydraulic reservoir circuit. This sensor assembly uses an analog device: the AD540C integrated circuit temperature transducer. A complete description and test data can be found in Subsection 1.3.1.4.

1.3.5. Rudder

1.3.5.1 Description

As part of the control logic, the rudder was selected to demonstrate the disconnect logic. The concept was to measure and compare input-output signals at or close to the input source rudder pedal and rudder pivot axis.

Since accessibility of the rudder pedal area was not prevalent, the input potentiometer was installed in the turtle deck area.

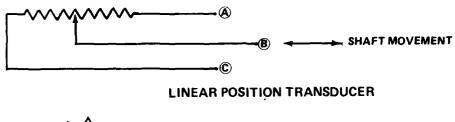
1.3.5.2 Rudder Differential Displacement Circuit

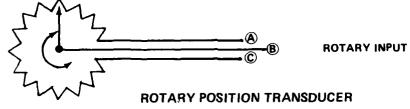
In some aircraft systems, mechanical disconnects have occurred due to disengagement of a bolt or clevis pin in the mechanical/electromechanical linkage. This would not be evident in aircraft which do not have flight-control surface display indicators on the cockpit panel.

System disconnects can be detected by comparing an input signal to a corresponding output signal. If the output signal does not follow or null out the input signal, micro-processor circuitry will indicate a disconnect condition until corrective action is taken.

Linear or rotary potentiometers are another type of displacement measuring device. Rotary or rectilinear movement of the input shaft positions a contactor (wiper) along or around a continuous resolution resistance element. These devices have practically zero backlash, are insensitive to vibration, and are compact and lightweight. In addition, their cost is low. Rotary transducers are made in multiples of 360° rotation; some cover 3600° (10 turns). Figure 64 shows typical transducer wiring diagrams and a representative plot.

The signal on both transducers are fed to a bridge circuit which detects a variation or omission of an input signal. When this imbalance occurs, the HYCOS circuit is energized.





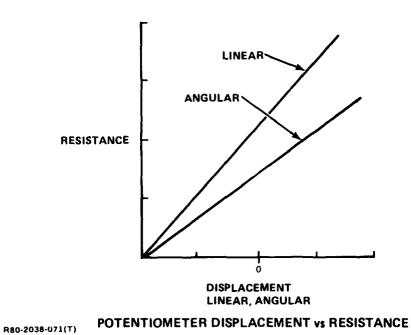


Figure 64. Potentiometer transducers.

Table 7 lists pertinent information on transducers used on the A-6E rudder actuator circuit. Figure 65 shows the turtle-deck potentiometer installation, and Figure 66 shows the rudder position potentiometer installation.

Calibration curves for the installations are shown in Figure 67.

TABLE 7. A-6E RUDDER POTENTIOMETER TRANSDUCERS.

TRANSDUCER	MANUFACTURER	SPEC NO.	TYPE	VALUES	LINEARITY
RUDDER POSITION POTENTIOMETER	ALLEN BRADLY	MIL-R-94	RV45A45D103A	10,000 Ω 2 W	' 10%
TURTLE DECK BELLCRANK POTENTIOMETER	ALLEN BRADLY	MIL-R-94	RV45A45D103A	10,000 Ω 2 W	. 10%
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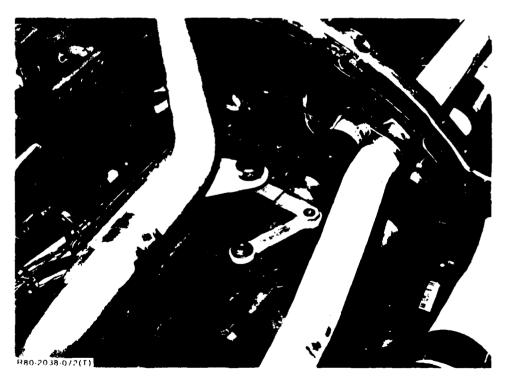


Figure 65. Turtle deck bell crank potentiometer installation.



Figure 66. Rudder position potentiometer installation.

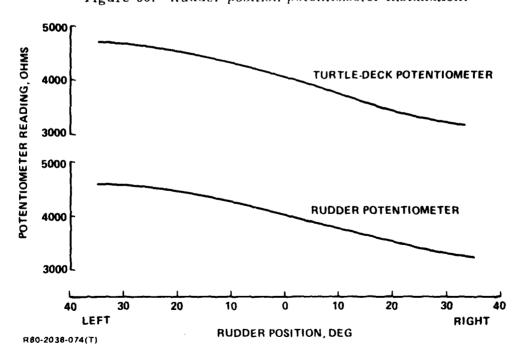
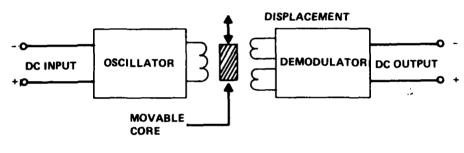


Figure 67. Rudder differential displacement potentiometer calibration.

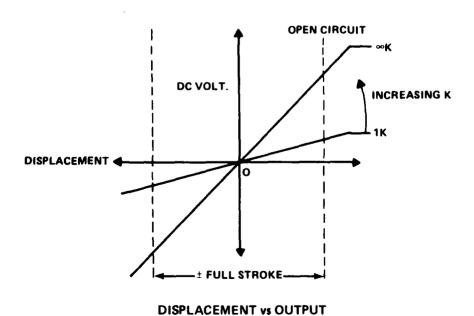
Two basic types of systems were originally considered:

- DC-DC displacement transducers
- Linear or rotary potentiometers.

In DC-DC displacement transducers, an oscillator is used to generate an AC signal which then couples a multiple-leg transformer to a moveable core. The coupling efficiency of the core then determines the position of the element being measured. The signal is then demodulated or rectified to a DC output. Figure 68 shows a typical circuit diagram and output curve.



CIRCUIT DIAGRAM



R80-2038-075(T)

Figure 68. DC-DC displacement transducer.

1.3.6 Display Panel

1.3.6.1 Description

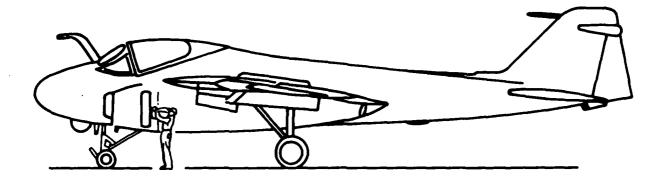
The readout panel is a ground-accessible unit which has clearly labeled lights for indicating component failure conditions. The panel is not accessible to the pilot during normal flight, although certain circuits could be interfaced with a caution-warning panel in the cockpit. Figure 69 shows a typical accessible HYCOS panel location on an operational aircraft. The panel can be interrogated both with and without aircraft or ground-support power.

The primary display panel is a self-contained unit measuring approximately 12 in. by 6.5 in. by 4.5 in. This size was chosen primarily to fit into an available existing space in the proposed flight-test vehicle. When required the size, shape, and weight could be configured to specific vehicle installations. The panel weighs 6.0 lb and contains microelectronic circuits and associated interface elements which are described in detail in subsequent subsections.

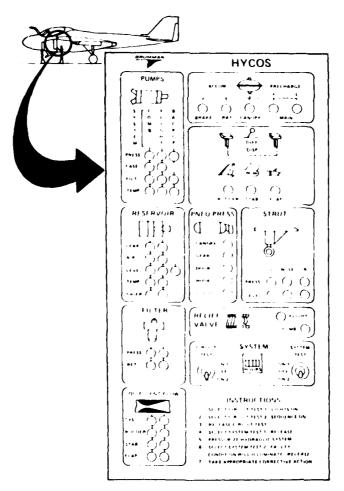
Basically, the panel houses:

- Display grain of wheat lamps
- Fiber-optic interface outlets
- Lamp drivers
- Counters
- Shift registers
- Power interface
- Sensor and system test circuits
- Microprocessor
- Analog-to-digital converters
- Memories
- Rechargeable NiCd batteries
- Battery heating and charging circuits.

Figure 70 shows the display panel connector interfaces, while Figure 71 shows the panel installed on the flight test vehicle.

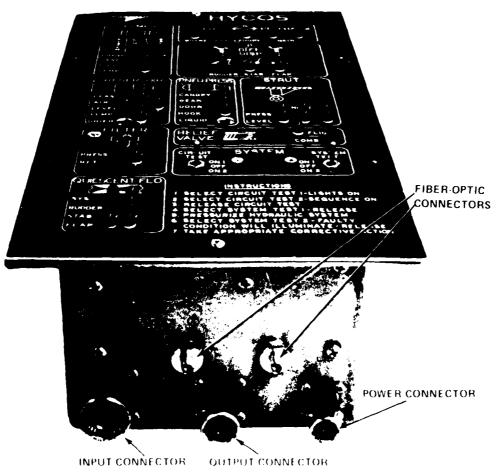


TYPICAL HYCOS ACCESS LOCATION



R80-2038-076(T)

Figure 69. HYCOS panel location on typical aircraft.



R80-2038-077(1)

Figure 70. HYCOS panel showing bottom connectors.

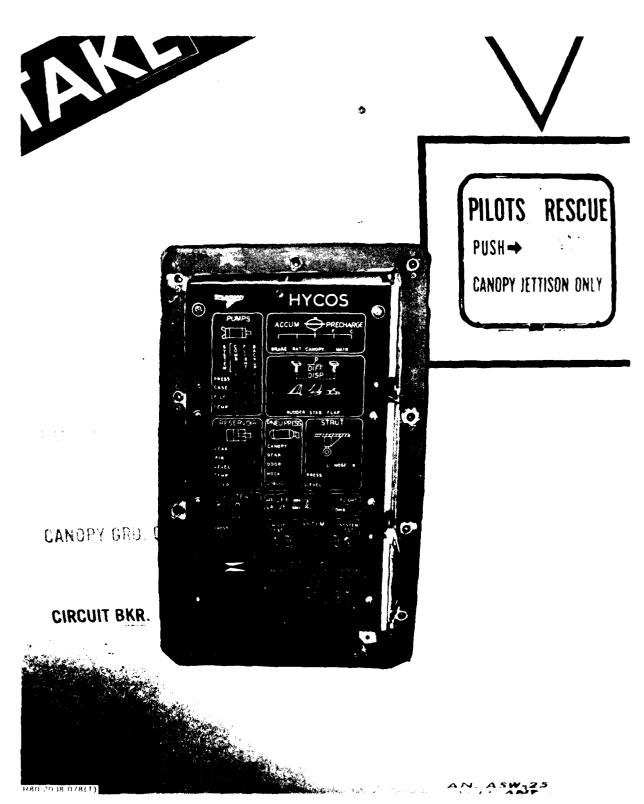


Figure 71. HYCOS installation in flight test vehicle.

1.3.6.2 Display Panel Indicators

Several types of display indicators were considered at the beginning of the program. These included LEDs, LCDs, LCDs with backscatter lighting, and subminiature incandescent lamps. Subminiature incandescent lamps are called "grain of wheat" bulbs due to their small size. After careful evaluation, the decision was made to utilize subminiature incandescent lamps since they offer good visibility during daylight and have an acceptable operating temperature range.

LEDs have some advantages but are not readily visible during daylight high-sun conditions. Since the intent of HYCOS is to place the display panel in an external ground-accessible area, the subminiature incandescent lamp was selected.

Table 8 compares the indicators considered. Size-for-size, the subminiature incandescent lamps exhibit good visibility under sunlight conditions. Although their current drain is higher than the other types considered, their ability to provide good daylight visibility became an overpowering factor. The use of lamps with a 60 mA rating would provide good service life (5000 hr average) and adequate illumination under sunlight conditions. Figure 72 illustrates the basic types of indicator displays (Ref. 8). Figure 73 is a plot of spectral output for various display types as observed by human eye response.

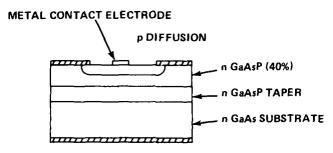
Since as many as 50 display indicators could light up under circuit test conditions, the NiCd battery momentary current drain could be 3 A or higher, neglecting the power requirements for the microprocessor and associated circuits. This condition occurs when the ship's battery and/or engine electrical power is on. This is a momentary high drain for the NiCd battery and did not significantly affect service life. With ship's power on, adequate monitoring panel and sensor current is available.

Another technique for reducing power drain is to use the microprocessor timer to sequentially test each subsection when the circuit test button is depressed. Under system test conditions, it is highly unlikely that more than five components would indicate failure modes and require power at any one time.

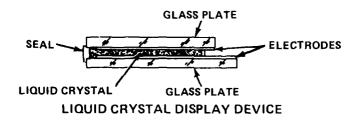
All grain of wheat bulbs are replaceable from the front of the panel by first removing the red plastic cover. Individual and collective circuit and bulb tests can be performed to verify the integrity of each indicator bulb.

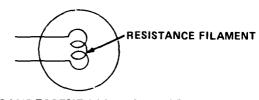
TABLE 8. HYCOS DISPLAY INDICATOR CONSIDERATIONS.

	POWER RE	POWER REQUIREMENTS	1	VISIBILITY	<u>ر</u>	
TYPE	VOLTAGE, V	CURRENT, mA	SUNLIGHT	NIGHT	BRIGHTNESS	COMMENTS
LED (LIGHT-EMIT) ING DIODES)	ഗ	20	POOR LIMITED WITH LIGHT FILTER	0005	30-300 FOOT.	 OPERATING TEMPERATURE RANGE: 58 TO 212°F LONG LIFE LOW OPERATING VOLTAGE RUGGED SMALL SIZE RESPONSE TIME, NANOSECONDS
LCD (LIQUID CRYS. TAL DISPLAYS)	w	30 (6 SEGMENTS)	0000	POOR	PASSIVE DISPLAY REO. UIRES AMBIENT OR SEPARATE LIGHT SOURCE	 OPERATING TEMPERATURE RANGE: 14 TO 140°F (0 to 60° C) BECOMES SLUGGISH AT LOWER TEMPERATURES RELIES ON EXTERNAL LIGHT SOURCE FOR VIEWING AT NIGHT
LCD WITH BACK SCATTER LIGHTING	ഗ	30+ (15 FOR BACKSCATTER LAMP)	GOOD	GOOD TO FAIR	SIMILAR TO INCANDESCANT	COMPLEX, BULKY. TEMPERATURE. LIMITED
SUBMINIATURE INCANDESCANT LAMPS	w	15 TO 60	G00D	G000	> 1000 FOOT.LAMBERTS	 LIMITED BY MULTIPLE LAMP CURRENT DRAIN DURING BATTERY OPERATION HEAT DISSIPATION A SIGNIFICANT CON- SIDERATION BRIGHTEST OF ALL DISPLAYS LOW VOLTAGE REQUIREMENTS RESPONSE TIME IN MILLISECONDS
R80-2038-079(T)						 VIBRATION-RESISTANT IN SMALL SIZES



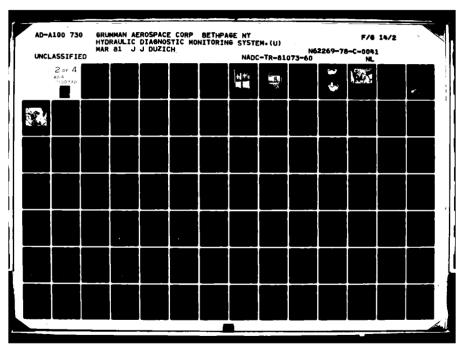
METAL CONTACT ELECTRODE
GALLIUM ARSENIDE PHOSPHIDE LIGHT-EMITTING DIODE





INCANDESCENT LIGHT SOURCE

Figure 72. Types of display indicators.



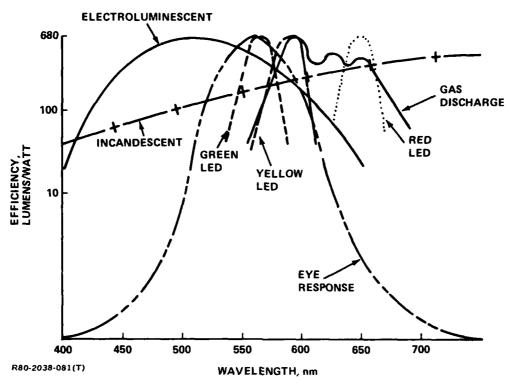


Figure 73. Spectral output of various displays compared to response of human eye.

1.3.6.3 Microprocessor

The Intel 8748 (Ref. 9) is a single-component, 8-bit microcomputer fabricated on a single silicon chip using the N-channel silicon gate MOS process. Unlike the 8048, the 8748 has an erasable program memory which can be varied for tests and evaluation during the prototype and reproduction stages. The 8748 is early programmable and has sufficient room for additional programs and/or add-on functions. In particular, it:

- Is an 8-Bit CPU containing ROM, RAM, I/O, and a Timer in a single package
- Is powered by a single 5 VDC power supply
- Responds in a 5.0 μ sec cycle. All instructions use one or two cycles
- Has a 1K by 8-bit EPROM, 64 by 8-bit RAM, and 27 I/O lines
- Contains an internal timer/event counter
- Has a single-level interrupt.

A block diagram of the 8748 is shown in Figure 74. Figure 75 shows a typical pin arrangement for this unit.

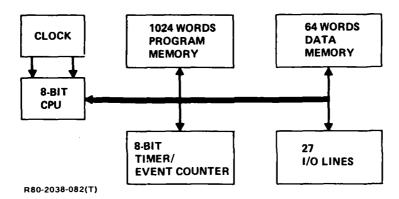


Figure 74. Intel 8748 block diagram.

1.3.6.4 Charging Circuit

A charging circuit was designed into the system to keep the twelve nickel-cadmium batteries charged when the vehicle is on ground-support power or on an operational mission.

A transformer is used to step-down the 115 VAC, 400 Hz power supply. Rectification is accomplished by a diode to a DC value slightly higher than the 5 VDC system. Since nickel-cadmium batteries are difficult to charge below 0°C, external heaters are used to maintain battery temperatures above this value.

1.3.6.5 Heating Circuit

Since the NiCd batteries must be charged with the vehicle flying at various altitudes, thermostat-controlled battery strip heaters are incorporated. When the temperature drops below 0°, the heating strip functions until the surface temperature reaches 32°F. This thermal cycling enables the batteries to achieve and retain a full charge. Figure 76 shows charging characteristics of NiCd batteries as a function of temperature (Ref. 10). During the flight test programs, modifications were made to the battery charging circuit to reduce the charging rate and provide for an external access connector. This connector was used to check status on battery voltages and provide an external dedicated recharge capability. Both battery analysis and external battery charging circuits are discussed in Appendix I.

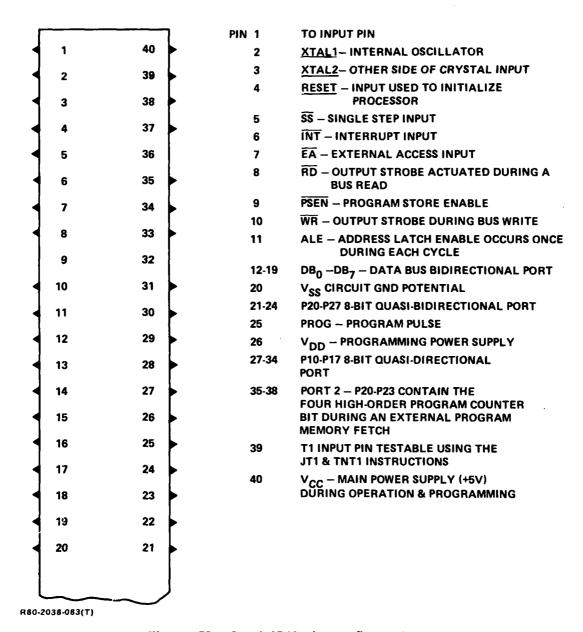


Figure 75. Intel 8748 pin configuration.

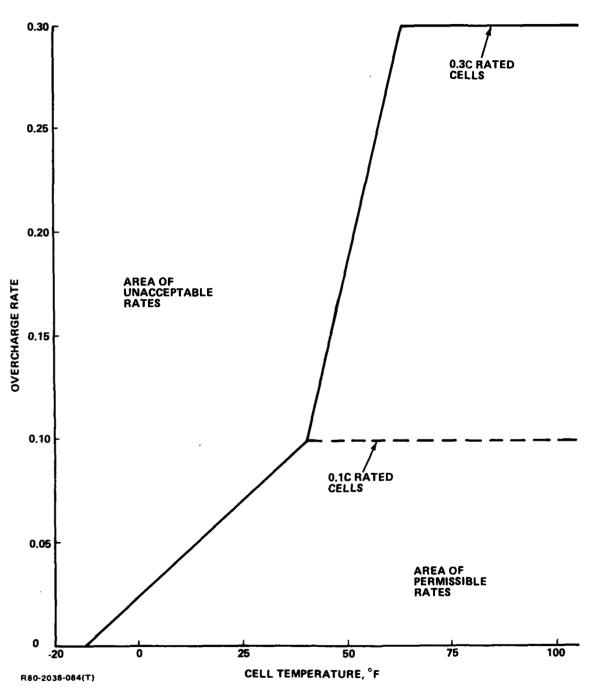


Figure 76. Nickel-cadmium battery charge characteristics.

1.3.6.6 Wiring Circuit

The basic wiring circuit is shown in Appendix I. Four removable display cards (Figure 77) comprise the major portion of the circuit and consist of the following:

- Card No. 1: Microprocessor memory and display drivers
- Card No. 2 & 3: Counters and A/D converters
- Card No. 4: Interface circuits.

Figure 78 shows the HYCOS panel with its cover removed.

Basic card element functions are as follows:

- Microprocessor unit, controls all calcuations
- Lamp Drivers supplies current to display lamps
- Output expanders receives three inputs and delivers eight different outputs
- Dual flip-flops used for data storage
- A/D converters receives analog data and converts it to a 8-bit digital word
- Hex Buffer used to drive data bus
- Counter latch; seven-segment driver counts pulses, stores value, and drives seven-segment display
- Transistors amplifies pulse input and potentiometer signals
- Schmitt Trigger used to square waveshapes
- Diodes used for lamp test isolation and to rectify AC for battery charging
- Batteries 1 A-hr battery drives high-power circuits and 100 mA-hr battery supplies low-power requirements.

1.3.6.7 HYCOS Flow Diagram and Program Limits

Program limits are established for the particular subsystem in question. A math model was first established which defines the normal operating parameters. When these limits are exceeded either individually or collectively, the program subroutine detects the discrepancy and provides the proper circuit response.

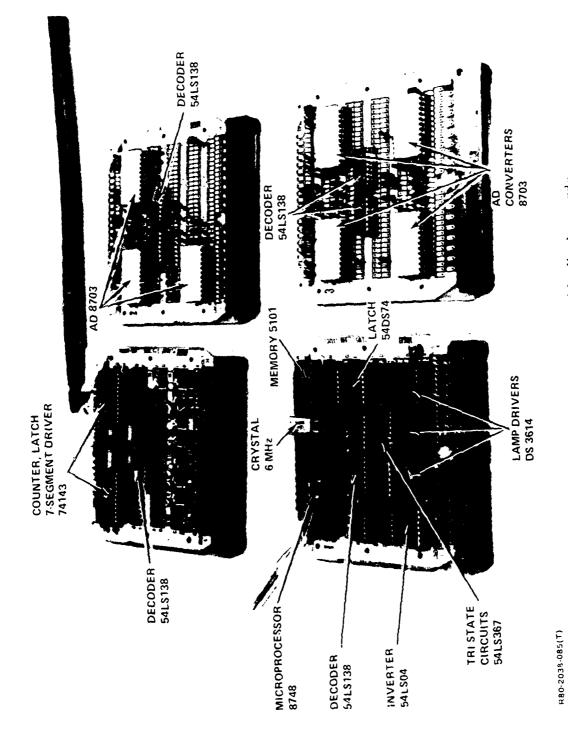
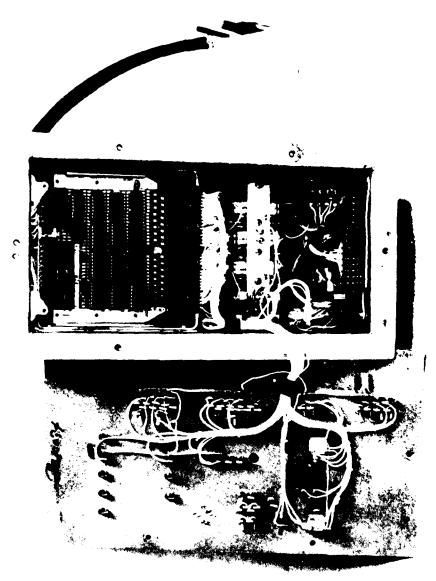


Figure 77. Removable display cards.



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Figure 78. HYCOS panel with cover removed.

The program flow diagram is broken down into six basic routines:

- Executive Routine
- Sequence Routine
- RAM Load Routine
- Rudder Routine
- Reservoir Routine
- RAT Routine.

Additional details of the flow diagram and the microprocessor program are listed in Appendix K.

1.3.7 Hydraulic Filters

1.3.7.1 Filter Differential Pressure Indicators

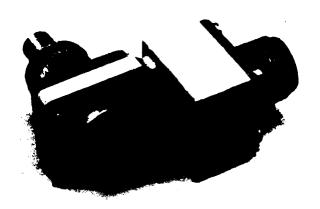
Filter differential pressure indicators, commonly used in the fluid power industry, are an indirect means of identifying contaminated filter elements which require servicing. The indicator is usually mounted to the filter head or bowl and provides a visual signal whan a predetermined element differential pressure has been exceeded. In order to take into account fluid viscosity changes due to thermal conditions, various means are employed to preclude indicator operation before the system reaches normal operating temperature. One method uses a bimetallic sensing unit placed in close proximity to the visual indicator; another employs a temperature-sensitive gas, fluid, or elastomer.

To provide remote indication capability, an electrical switch may be mechanically or otherwise actuated by the primary sensor indicator. Resetting the mechanical indicator also resets the electrical circuit.

A boot or transparent cap is provided over the indicator to improve reliability by making it less susceptible to extrinsic debris and fluid. This cap is physically restrained or bonded to the adjacent element. Figure 79 shows a typical interchangeable differential pressure indicator. An actual installation photograph is shown in Appendix J.

1.3.7.2 System Fluid Sampling

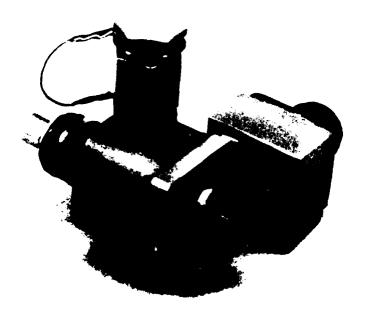
Another version of the delta-p indicator contains a sampling port which permits fluid extraction from the upstream side of the filter element while the system is pres-



R80-2038-087(T)

Figure 79. Filter differential pressure indicator.

surized. One such type of "Multicator"* is shown in Figure 80. Figure 81 shows an installation in the pump case drain filter.



R80-2038-088(T)

Figure 80. Filter differential pressure indicator with sampling valve.

^{*} Multicator is an APM Trademark

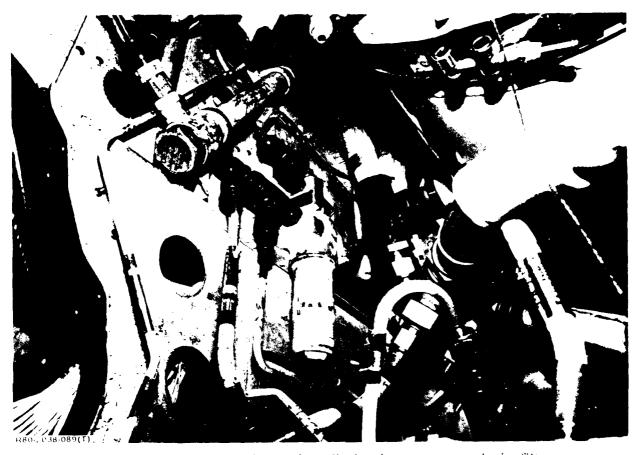


Figure 81. Multicator indicator installation in pump case drain filter.

A special wired plug is used to protect the sampling port when not in use, and also acts as a redundant pressure seal.

Grumman Specification 202 defined the pertinent parameters of each unit used for the HYCOS Program.

It should be noted that most visual and electrical indicators are usually discrete signals (Go/No-Go type). In cases where an analog signal is required, this may be provided by using the approach shown in Figure 82. This concept utilizes a linear output Hall Effect sensor actuated by a movable permanent magnet which is coupled to a spring-biased piston. Movement of the sensing piston magnet affects the magnetic flux density seen by the Hall Effect sensor, reducing the output signal. Since the sensor output varies as a function of ambient temperature, temperature compensation must be provided.

1.3.8 Flight Control Hydraulic Backup Package

A Klixon overtemperature switch was bonded to the flight control backup module to measure system and closed-loop surface overtemperature conditions. The switch conforms to Grumman Specification 201 and has a trip setting of $300 \pm 20^{\circ} F$. It is manually resettable through a neoprene overmold. Figure 83 (Ref. 11) shows typical switch characteristics. Actual installation on the flight control backup module is shown in Figure 84. Operation of the hydraulic backup package occurs during preflight check and only if one hydraulic system is lost.

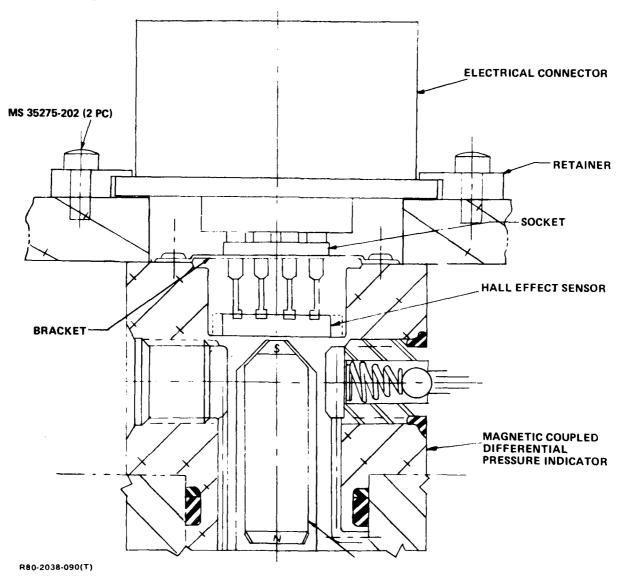


Figure 82. Linear output Hall Effect differential pressure indicator.

- SNAP-ACTION SWITCHING
- NORMALLY OPEN OR NORMALLY CLOSED
- AUTOMATIC OR MANUAL RESET
- SPST OR SPDT
- OVERMOLD OPTIONAL

PERFORMANCE CHARACTERISTICS

DIELECTRIC STRENGTH:
1250 VAC, RMS, 60 CYCLES FOR ONE
MINUTE (1500 VAC RMS AVAILABLE ON
SPECIAL REQUEST)

AMBIENT TEMPERATURE RANGE: NON OVERMOLD — 65° F TO 450° F NEOPRENE OVERMOLD — 65° F TO 160° F SILICONE OVERMOLD — 65° F TO 450° F

SWITCH ACTION:

SPST OR SPDT (SNAP-ACTION)

LIFE CYCLE:

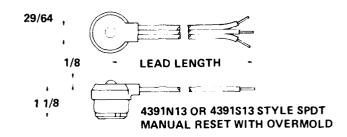
SEE ELECTRICAL RATING TABLE

VIBRATION:

STANDARD CONSTRUCTION 5-500 CPS, 3G's HIGH VIBRATION CONSTRUCTION 5-500 CPS, 5G's

WEIGHT:

WITHOUT OVERMOLD 21 GRAMS AVERAGE WITH OVERMOLD 56 GRAMS AVERAGE



ELECTRICAL RATINGS (RESISTIVE)

	AMPERES		
30 VAC/DC	125 VAC	250 VAC	LIFE CYCLES
10	4	2	100,000
11	6	3	50,000
12	8	4	25,000
13	10	5	10,000
14	12	6	5,000

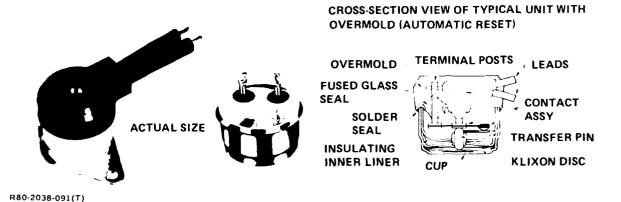


Figure 83. Resettable temperature switch characteristics.

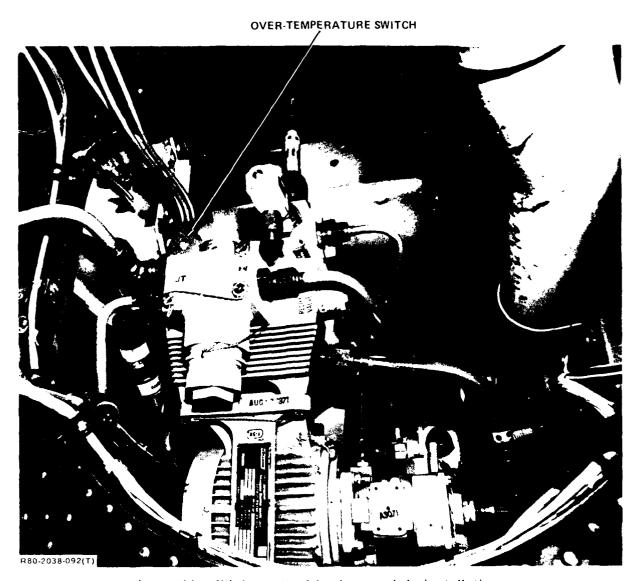


Figure 84. Flight control backup module installation.

Section 2

GROUND AND FLIGHT TESTS

2.1 SYSTEM DEBUGGING

During the early part of 1979 all sensors, hard lines and wiring were installed during vehicle buildup. In mid-May, the vehicle with sensors and HYCOS wiring was subjected to and passed the hydraulic ground check and acceptance testing. These tests verified hydraulic system integrity on both the flight system and the combined system on which HYCOS was installed.

Debugging included rerunning hydraulic reservoir displacement calibration to verify the laboratory values. All HYCOS wiring was checked between the sensor interface and display panel for continuity. A rudder differential displacement check was made after calibrating both potentiometers. Continuity checks were also made on the fiber-optic circuits. After the first flight in October 1979 it was found that the elapsed time meter (ELT) was not functioning. Investigation showed that the ELT operated through a relay after the panel switch was energized. A wiring change was made to the ELT circuit. This enabled the ELT to register every time the combined system was monitored or AC power was available on the aircraft. While the panel was being rewired, an IC chip was also replaced. Details of the wiring change is shown in the appendix.

2.2 DEVELOPMENTAL MODIFICATIONS AND IMPROVEMENTS

2.2.1 HYCOS Display Panel

Modifications were made at the onset of the program to the battery charging circuits to improve NI-CAD battery reliability. During the early phases of the program the NI-CAD batteries discharged when the aircraft was stored in the hangar over the weekend. A HYCOS battery analysis was conducted (See Appendix K) which indicated that the batteries were adequately sized and that the charging rates should be reduced from 100 mA-hr to 50 mA-hr for the 5-volt battery. The charging rates for the 3.6V and -6V batteries was reduced from 10 mA-hr to 5 mA-hr.

The analysis also indicated that the panel should be equipped with an external accessible connector to provide direct connections to the battery plus and minus terminals. The connector would then allow external monitoring of battery voltages without removing the panel from the vehicle, and it would also provide charging access to the NI-CAD batteries using a dedicated ground support charger.

Both improvements were incorporated. A dedicated battery charger was fabricated but seldom used since, after subsequent initial charging, the ship's electrical buss maintained the batteries in a usable state.

Another improvement area was in modifying the internal power circuit to the elapsed time meter. This was done so that power to the elapsed time meter would occur when both AC and hydraulic system power was available. When the system is interrogated on the ground in the static condition no power reaches the elapsed time meter. In the same circuit, the relay was replaced with a heavy duty Leach DM 2-5.

In order to reduce the number of sequential operations, the system test switch was modified by replacing the ON, center OFF, ON configuration to an ON momentary at the panel. This reduced the system test functions to only 1:

- With the system test switch in its ON position, power is supplied to the elapsed time indicator if hydraulic power is on
- System test "ON 2" without hydraulic power checks air in the reservoir and discrete circuits
- System test "ON 2" with hydraulic power checks the reservoir, ram air turbine accumulator, and rudder differential circuit.

The addition of a top hat to the desiccant color detector terminal improved color transmission visibility at the panel.

2.2.2 Panel Support Structure

During the early part of the program, a doubler plate was added to the access plate to provide additional clearance for the load bearing fasteners. This improvement corrected the fastener retention problem caused by marginal material thickness.

2.2.3 Sensor Light Sources

As the flight test program evolved, it was determined that a more intense light source was needed at the desiccant color detector and pneumatic liquid bottle detection circuits. Three halogen lamps were added with specially designed housings for this purpose. There was a significant improvement in available light intensity.

2.2.4 Flow Sensor Indicators

Environmental vibration during a normal flight schedule caused two of the flow sensors to indicate incorrectly. After investigation and vibration testing, it was found that the resonant frequencies of the lockout solenoid armature/spring occurred. The armature/spring mass was redesigned to move the resonant frequency out of the operational envelope.

2.2.5 Desiccant Color Detector

Several improvements were made to this sensor. These included increasing the light intensity at the surface, optimizing the reflected transmitter, receiver angle, and finally developing a new desiccant color disc mounted internally in the air stream. Color transmission from irregular granular surfaces proved difficult because of the irregular granular surfaces.

Fiber-optic cable junctions should be minimized and cable runs must be carefully laid to avoid sharp bends.

Crazing of the transparent plastic tube developed later in the program. This tube was replaced with another unit of the same type. Examination of the part indicated that crazing was caused by over torquing the sensor body to its outside diameter.

Section 3

PERFORMANCE AND EVALUATION/ASSESSMENT

3.1 PROCEDURES AND METHODS

3.1.1 Objective

The purpose of the Flight Test Program is to evaluate the HYCOS System under actual operating conditions and to determine its effectiveness in detecting system and component malfunctions. It in no way replaces the normal maintenance schedules, but may be used in conjunction with such maintenance actions.

3.1.2 Procedure

This procedure defines a systematic method of conducting a "HYCOS" Interrogation. All data is to be recorded on the provided HYCOS Log Sheet and HYCOS Check-out Logic Sheet.

Three (3) checks are required:

- "A" Preflight static check is conducted with the flight vehicle in the hangar prior to towing to flight line. This provided the initial condition prior to flight. Any abnormalities or malfunctions would be corrected at this time.
- "B" Postflight dynamic check is required to measure internal system and pump leakage with no mechanical input into the control surfaces. During the time the system is pressurized, power is supplied to the elapsed time meter which keeps track of system operational time.
- "C" Postflight static check is conducted after the vehicle was moved to the hangar. This approach was used to detect any changes that may have occurred since the preflight static check.

3.1.3 Log Sheet Description

Using the HYCOS LOG SHEET:

- Enter DATE System is integrated
- Enter FLIGHT NUMBER
- Enter FLIGHT DURATION in hours
- Enter Elapsed Time Meter reading
- Enter CHECK in applicable Flight Interrogation column
- MALFUNCTION List ANY Hydraulic System Malfunction that occurs on the combined or Flight Hydraulic System
- MAINTENANCE ACTIONS List any maintenance actions taken on either Combined or Flight Hydraulic Systems.
- Check if malfunction or maintenance action was indicated by or on HYCOS Panel
- Plane Captain/Technician Write name of plane captain conducting interrogation and technician performing maintenance action.

3.1.4 HYCOS Interrogation Procedure

This sheet is used in conjunction with the Log Sheet but presents more detailed information. The switch positions are broken down into three categories:

- Category "A" designates a pre-flight static check.
- Category "B" designates a post-flight dynamic check (right engine running no power control input).
- Category "C" designates a post-flight static check.

In conducting the <u>preflight static check</u>, select <u>CIRCUIT TEST ON 1</u> and hold. Record by code those display lights that do and do not illuminate, in column "A". Release switch.

Select and hold <u>Circuit Test On 2</u>. All red lights should sequence in a sub-block order. Record. This check verifies that the microprocessor timer is functioning. Release switch.

Select and hold <u>Systems Test On 2</u>. Record illuminated lights. This step illuminates those sensors that are out of tolerance and require visual verification. Upon visual verification conduct necessary repair or maintenance action. Record all information in Log Sheets.

3.1.5 HYCOS Display Criteria

- PUMP (Sub-Category)
 - <u>PRESS</u> Illuminates when system pressure drops below approximately 2,200 psi in the combined Hydraulic System. The light extinguishes when the system is pressurized
 - <u>CASE</u> Illuminates when pump case flow is excessive and may require pump removal. Excessive pump case flow is an indication of a worn or degraded pump
 - <u>FILT</u> Illuminates when case drain flow filter button pops indictating required maintenance action. After performing maintenance action, reset the visual filter delta "P" button. This rests the electrical circuit
 - <u>TEMP</u> Illuminates when the pump case drain fluid temperature is excessive (caused by high bypass). This is used in conjunction with pump case flow circuit
- RESERVOIR (Sub-Category)
 - <u>LEAK</u> Illuminates when level drops two inches or more during flight. Also, illuminates if reservoir is not filled to specification
 - AIR Illuminates if reservoir piston moves greater than one inch from unpressurized to pressurized
 - <u>TEMP</u> Illuminates if reservoir level temperature is excessive. Indicates possible fault in system and requires additional troubleshooting
 - <u>DRIER</u> When pale blue desiccant is still serviceable, when color changes to pink or pale pink, replace desiccant cartridge in system and desiccant in sensor

- FILTER (Sub-Category)
 - <u>PRESS</u> Illuminates when pressure filter is clogged and requires replacement. When filter is serviced and indicator button is reset, light will extinguish
 - RET Illuminates when return filter is clogged and requires replacement.

 When filter is serviced and indicator button is reset, light will extinguish
- QUISCENT FLOW (Sub-Category)
 - SYSTEM Indicates excessive internal system leakage. This is taken during dynamic check with no control input. Flow sensor must be manually reset after taking corrective action
 - RUDDER Indicates excessive rudder actuator internal leakage. Also taken during dynamic check with not control input. Flow sensor must be manually reset after taking corrective action. Note: Flow sensors will not indicate properly unless system is pressurized
- ACCUM PRECHARGE (Sub-Category)
 - RAT Indicates low accumulator precharge irrespective of accumulator piston position. If light illuminates with system test "ON 2", service accumulator
- DIFF DISP (Sub-Category)
 - RUDDER Indicates disconnect between push pull rods on and rudder actuator. Combined system must be pressurized. Rudder position follow rudder pedal inputs
- PNEU PRESS (Sub-Category)
 - <u>CANOPY</u> Illuminates when canopy bottle (15 in.³) pressure is low and requires servicing
 - GEAR Indicates when gear door bottle (30 in. 3) pressure is low and requires servicing
- RELIEF VALVE (Sub-Category)
 - <u>COMBINED</u> Indicates when main system relief valve is leaking (failure or improper seating)

- SYSTEM (Sub-Category)
 - <u>CIRCUIT TEST ON 1</u> Checks discrete circuits to sensors thru common and on leg
 - <u>CIRCUIT TEST ON 2</u> Checks microprocessor and lights in sub-block sequence
 - SYSTEM TEST ON 1 Programs the microprocessor when system is pressurized
 - SYSTEM TEST ON 2 Interrogates entired combined system (red lights only).

 When red lights illuminates this indicates a malfunction or requires maintenance action
 - ELAPSED TIME METER Runs when combined system is pressurized.

3.2 OVERALL EVALUATION OF HYCOS SYSTEM

As a preventative maintenance tool, the HYCOS System performed exceedingly well in determining the condition of the system. During the course of its program, it consistently detected:

- Low canopy and door gear dump pressures
- Low reservoir level during initial calibration
- Low system pressure during start up conditions
- Continuous elapsed time on system components.

There were no indications of hydraulic pump excessive case flow or case flow oil temperatures since the sensor limits were not exceeded.

Fiber-optic desiccant color detection proved difficult, even with the addition of more intense light sources. This was attributed to the improper installation of fiber-optic runs in which the bend radius were exceeded, causing excessive light loss. Another area requiring improvement is in optical terminal coupling, where losses can be considerable. Color transmission of red and pink is excellent; however, pale blue is not readily detectable.

The filter subsection gave no indication of tripped delta "p" indicators. This may be due to the fact that the vehicle flew over 150 hours and did not experience any hydraulic subsystem failures. Quiescent and rudder actuator flow sensors, when

interrogated under dynamic conditions, did not indicate excessive flows as originally established. There were, however, developmental problems caused by vibration which were subsequently solved.

The ram air turbine (RAT) accumulator functioned flawlessly with no indication of precharge loss. Pressure, temperature, and displacement sensors functioned as advertised. This component is used as an energy storage device and retains this capability even when the system is shut down.

Except for initial calibration, the differential displacement sensors operated satisfactorily since the rudder output follows the mechanical input. This portion of the circuit is not activated until the combined system is pressurized.

Indications of low pneumatic system pressure worked effectively and repeatedly within limits. Minor system leakage was detected after the vehicle remained in an inactive flight status for several days. Topping the bottles corrected this condition.

Since the relief valve did not malfunction, no indication was apparent on the display. Relief valves are usually passive devices until excessive pressures are exceeded. If this occurs and instability prevails, seat or poppet damage can occur. This results in leakage with subsequent system fluid temperature rise.

The circuit and system test switches functioned satisfactorily, but the system test switch was modified to a continuous ON 1 when the battery charging circuit was modified. Future procedures would eliminate the need for first selecting ON 1 followed by ON 2.

The lay-over time between flights determines the condition of the NI-CAD storage batteries. Although the battery charging circuit is adequate, infrequent ground charges may be necessary. This was readily accomplished by using the ground battery changer through the added electrical panel interface. This connector also provided test points to determine battery condition without removing power from the vehicle.

Section 4

RESTORATION OF THE AIRCRAFT

The flight test program terminated on November 15, 1980 when the aircraft was subjected to a debailment inspection before being turned over to Navy inventory as an updated A-6E. The inspection involved the following activities:

- The following special components were removed from the vehicle:
 - HYCOS Display Panel
 - Quiescent, rudder actuator, and pump case drain flow sensors
 - Pressure, filter, and temperature switches on the combined system pump
- The combined system reservoir was replaced with the original unit kept in storage
- Remote reading delta "P" indicators were replaced with original units
- The ram air turbine accumulator and supporting bracket was replaced with a standard unit.
- Potentiometers located on the turtle deck and rudder were removed in the differential displacement circuit
- Both the pneumatic pressure canopy and emergency gear door pump bottles were replaced with standard units
- The fluid thermal switch was removed downstream of the combined system relief valve
- All wire leads and fiber-optic cables peculiar to the HYCOS system were capped and lagged at both the panel and sensor interface
- The surface temperature switch was removed from the flight control backup module.

The power supply cable (110V 400 \sim AC) from the circuit breaker to the HYCOS panel was disconnected. The HYCOS access cover was permanently attached to the structure in accordance to an EO issued by the Structural Design Group.

After installation of standard production components, lines, and fittings, the vehicle was subjected to a hydraulic ground check to substantiate system integrity in accordance with the ATP. No problems were encountered during this refurbishment.

In addition, an engine ground run was successfully accomplished to verify flight worthiness since the port engine was removed to provide access to the keel where most of the HYCOS sensor components were located.

Section 5

CONCLUSIONS

- The flight test program met all the requirements of the work statement
- The HYCOS accumulated over 150 hours flight time during a 1-year flight test program
- Preflight checkout time takes only 1-1/2 minutes using the HYCOS, as compared to 20 - 30 minutes for a manual checkout
- The HYCOS consistently identified:
 - Low pneumatic bottle pressure
 - Low reservoir level
 - Low system pressure
 - System operating hours
 - Malfunctioned components on a post-flight check
- All other sensors operated normally and did not indicate malfunctions
- The microprocessor functioned flawlessly after final programming and integration. It also has capacity for additional fault-detection via changes in microprocessor programming
- The system is capable of detecting the health or malfunctions of components located in hazardous areas, such as when engines are operating
- The HYCOS did not impair or restrict the normal function or the combined hydraulic system
- HYCOS has demonstrated its capability as a preventative, failure, and maintenance tool
- HYCOS sensors were of the prototype configuration and were not optimized for size or weight

- As a result of the test program, it was found that the system can be further improved by:
 - Relocating the panel away from the inlet duct area
 - Reducing fiber-optic coupling & terminations and optimizing bend radii
 - Utilizing a dedicated disc detector and selecting fiber-optic cable having wider bandwidth to provide more efficient color transmission
- Since prime contractor service and maintenance is excellent, few hydraulic system malfunctions occurred during the test program. In actual squadron use, the benefits of such a system would be realized in:
 - Reduced preflight checkout time
 - Increased availability
 - Reduced turnaround time
 - Extended service intervals
 - Radio component fault indication
 - Utilization of less-skilled personnel
 - Ability to readily check inaccessible components on a preflight basis.

Section 6

RECOMMENDATIONS

- Continue developmental effort on alphanumeric (smart) terminal displays to provide quantitative information on status or malfunction in terms of order of magnitude
- Continue sensor development specifically adapted for lightweight hydraulic system vehicles with continuous monitoring
- Incorporate sensors or make provisions for adaptation/inclusion of sensors in selected components within redundant and dedicated power systems
- Expand the use of fiber-optic circuits in conjunction with digital sensors
- Determine the feasibility of a universal microprocessor display capable of multiple vehicle use
- Incorporate several advanced systems in a training squadron in order to obtain a more representative evaluation (larger statistical sample)
- Update current military component specifications to provide for optional (dedicated) sensors in major flight-critical components.

Section 7

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- 3. NAVAIR 01-85ADA-6-4 Landing Gear Emergency Operational Check.
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APPENDIX A

HYCOS LOG SHEET FORMAT AND TYPICAL FLIGHT LOG SHEET

DATE: FLIGHT NO			<u>-</u>			A6E M						
REVISION "A"											-	
	CIRCUIT TEST SWITCH POSITION						SYSTEM TEST					
SENSOR						SWITCH POSITION						
	ON1		ON2			ON1			ON2			
PUMPS	Α	В	С	Α	В	С	Α	В	С	Α	В	С
PRESS.								L!				<u> </u>
CASE		_						L				
FILT		_		ļ.,						_		
TEMP				ļ								
RESERVOIR												İ
LEAK				-								<u> </u>
AIR		 	<u> </u>					<u> </u>	-			<u> </u>
LEVEL		 		 					- i			-
TEMP								-			-	
DRIER		·	<u> </u>	\vdash								<u> </u>
FILTER			1]	
PRESS.	,			_				├ ─			-	-
RETURN		 	ļ					-				<u> </u>
QUIESCENT FLO						}					1	
SYS				<u> </u>					-			<u> </u>
RUDDER												<u> </u>
ACCUMULATOR RAT												
DIFF DISP												
RUDDER												-
PNEU PRESS]]								
CANOPY		<u> </u>									-	-
GEAR		1	 	 								
LIQUID				 								
COMBINED		<u> </u>										
NOTES: 1. DRIER 2. "A" DE "B" DE "C" DE 3. MARK	SIGNA SIGNA SIGNA	TES P TES P TES P	REFL OSTF OSTF	IGHT LIGH LIGH	CHECT CHE	CK (STA CK (D) CK (ST	ATIC) YNAMI 'ATIC)		ik			L

Figure A-1. HYCOS log sheet format used during program.

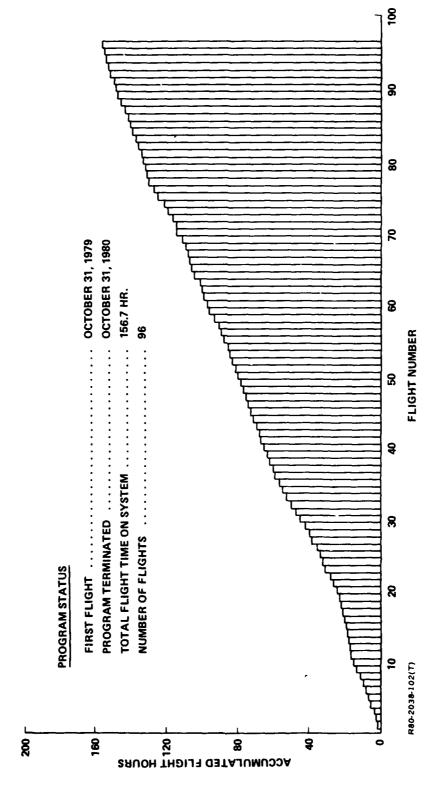
DATE: <u>08/06/</u> FLIGHT NO			-			A6E I	S CHEC	KOU' 9 B/N	T LOG 1556:	SIC 28		T TIME
REVISION "A"									-			
		CIRCUIT TEST			SYSTEM FEST							
SENSOR		SWI	TCH P	OSIT	ION		t	SWIT	CH P	OSITI	ON	
		ON1 ON2			ON1 ON2							
PUMPS	Α	В	С	Α	В	С	A	В	С	Α	В	С
PRESS.	<u> </u>	ļ	Ļ	L	ļ							
CASE	X	×	X	ļ	ļ	<u> </u>		<u> </u>		Х		X
FILT	X	X	X	<u> </u>	ļ	ļ						
TEMP	X	X	X	ļ	ļ	<u> </u>	ļ	ļ		ļ	<u> </u>	ļ
RESERVOIR		1		l			•					
LEAK	X	X	<u> </u>	ļ	<u> </u>	<u> </u>	<u> </u>	L				
AIR		x	X	 		Ĺ						
LEVEL	x_	×	X	ļ				L				
TEMP	x	X	X		<u>-</u>		ļ	<u> </u>			<u> </u>	
DRIER	×	X	_ x_	<u> </u>	lc.	<u> </u>			ļ	0	_0_	0
FILTER		}	1	GHTS	IGHTS	IGHT]					
PRESS.	х	_x_	X	SE-				<u> </u>				
RETURN	x_	X	X	<u> _</u> E	SEQU	SEQUENCE		ļ				
QUIESCENT FLO			1	QUENCE	JENCE	E E	<u> </u>					: I
SYS	X	X	X		유		l					!
RUDDER	X	х	х	Ş	<u> </u>	- ્						
ACCUMULATOR			ļ									
RAT	x	x	x								[
DIFF DISP												
RUDDER	×	х	×							Ì	}	
PNEU PRESS	×	×	×						j			
CANOPY	×	×	×									
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RELIEF VALVE	x	x	v						ł	Ì	ł	
COMBINED	<u> </u>	^	X		<u> </u>							
NOTES: 1. DRIE	R LIGHT	TRA	NSMIT	s co	LOR	IGHT	BLUE T	O PIN	ıĸ			
	ESIGNA							_ ,				
"B" D	ESIGNAT	TES P	OSTF	LIGH	T CHE	CK (D'	YNAMI	C)				
	ESIGNAT											
3. MARK	("X" IN	вох	TO IN	DICA	TE LI	GHT O	N.					
R80-2038-099(T)	ELT PRE-											

Figure A-2. Typical HYCOS flight log sheet.

APPENDIX B FLIGHT-HOUR ACCUMULATED LOG

FLIGHT-HOUR ACCUMULATED LOG

SHIP #		, n	MODEL	E	BUREAU #		
M22	9	<u> </u>	A-6E		15562		
FLT NO.	FLT-HR	ACCUM FLT-HR	FLT NO.	FLT-HR	ACCUM FLT-HR		
1	1.5	1.5	49	1.4	79.2		
2	.5	2.0	50	1.7	80.9		
3	.7	2.7	() 51	1.7	82.6		
4 5	2.2	4.9	52	1.5	84.1		
5 6	1.5 1.5	6.4 7.9	53	1.4	85.5		
7	1.4	9.3	54 55	1.1 2.0	86.6 88.6		
8	2.0	11.3	56	1.2	89.8		
9	2.2	13.5	57	2.5	92.3		
10	1.6	15.1	58	2.2	94.5		
11	1.3	16.4	59	2.4	96.9		
12 13	1.1 1.0	17.5 18.5	60	0.8	97.7		
14	.6	19.1	61 62	2.0 1.0	99.7 100.7		
15	1.0	20.1	63	1.4	100.7		
16	1.0	21.1	JJ 64	3.6	105.7		
17	.6	21.7	65	1.4	107.1		
18 19	1.6	23.3	 66	8.0	107.9		
20	.3 1.3	23.6 24.9	67	0.9	108.8		
21	2.0	26.9	68 69	1.2 2.4	110.0 112.4		
22	1.6	28.5	70	2.8	115.2		
23	2.3	30.8	71	2.0)		
24	1.8	32.6	72	2.5	117.7		
25 26	1.7	34.3	73	2.5	120.2		
26 27	2.3 2.1	36.6 38.7	74	2.3	122.5		
28	1.5	40.2	75 76	3.0 3.0	1∠5.5 128.5		
29	2.5	42.7	177	1.8	130.3		
30	3.0	45.7	78	1.0	132.3		
31	2.4	48.1	79	1.2	132.5		
32 33	2.1	50.2	80	1.3	133.8		
33 34	2. 9 1.9	53.1 55.0	81	1.2	135.0		
35	2.1	57.1	82 83	1.3 1.9	136.3 138.2		
36	2.7	59.8	84	1.4	139.6		
37	.5	60.3	85	1.1	140.5		
38	2.2	62.5	86	1.5	142.2		
39 40	1.2	63.7	87	1.9	144.1		
40 41	2.3 1.6	66.0 67.6	88	2.0	146.1		
42	.9	68.5	90	2.1 1.0	148.2 149.2		
43	1.4	69.9	91	1.0	150.2		
44	1.8	71.7	92	1.7	151.9		
45	1.6	73.3	93	1.6	153.5		
46 47*	1.6 1.0	74.9 75.9	94	0.3	153.8		
48	1.9	77.8	95 96	1.4 1.5	155.2 156.7		
*HYCOS REMO	VED FOR REPAIR						



APPENDIX C

ABBREVIATED CHRONOLOGICAL LOG

Dec. '77

- Kickoff meeting
- Display panel daylight visibility
- Started specifications

Jan. '78

- Generated specifications for sensor
 - Thermal switch
 - Delta p indicators
 - Flow sensors
 - Pressure switch

Feb. '78

- Continue sensor specification generation
- Start RLS layout defining panel block diagram
- Proceed with panel layout

May '78

- Review flow sensor; develop pressure probes
- Established display panel size and configuration

April '78

- Reservoir sensor development continues
- Mockup model of panel fabrication

May '78

- Installed sensors in F-14 reservoir
- Started A-6 reservoir layout
- Desiccant color detector
- Pressure transducer investigations
- Started installation of F-14 simulator

June '78

- Calibrated F-14 reservoir, issued P/O for A-6 reservoir parts
- Started testing pressure tranducers at high and low temperatures
- Flow sensor manufacturing is in progress
- E.E.D. manufactured panel test set

July '78

- Started modification of A-6 reservoir
- Installed panel on F-14A hydraulic simulator

August '78

- Received flow sensors
- Received optical sensors
- Acceptance-tested thermal switches
- Completed F-14 simulator wiring

September '78

- Develop desiccant color detector
- Develop liquid detector
- Started programming microprocessor for F-14 system

October '78

- Completed A-6 reservoir modifications
- A-6 flow sensors at vendors test

Nov. 178

- Ran displacement calibration on A-6 reservoir
- Ran F-14A HYCOS simulator demo

Dec. '78

- Flight-test vehicle tentatively established Mod 229
- Continue sensor development

Jan. '79

- Authorization received from NAVAIR to install HYCOS on Mod 229
- Vehicle is in second stage of buildup
- Issued Engineering Orders for
 - Brackets
 - Lines
 - Component modification
 - Sensor installation in keel area

Feb. 179

- Installation continues on wiring and hardware installation
- Continue sensor development and integration
- Conducted pressure seal tests

March '79

- Start hydraulic hard lines mockup
- Wiring runs for sensor installation begun
- Start sensor installations on port keel

April '79

- All hydraulic hard lines fabricated
- All wiring before sensor and display panel completed
- System pressurized

- Start electrical run line check
- Submitted interim report

May '79

- Completed hydraulic ground check and acceptance testing
- Instrumentation lines with exception of F/O circuit installed
- Vehicle passed through paint shop
- · Vehicle ground run tested

June '79

- Vehicle delayed 5 weeks due to structural bulkhead repairs
- Continue fiber-optic color detection development; investigate halogen lamp

20 June '79

- Investigate halogen lamps
- Added resistor to reduce voltage from 5 VDC to 3.5 VDC

30 July '79

- Ordered incandescent lamps
- Started interface and ground checkout on bailed A/C

August '79

- Structural mods made to vehicle to accept panel
- Started debugging system

Sept. '79

- Started rudder differential displacement calibration
- Reservoir calibration information supplied to E.E.D. for burn-in

Oct. 179

- Calibration rudder differential displacement
- Run circuit check using panel jumper
- Flew A/C for 1-1/2 hr
- ELT not operational

Nov. '79

- Removed panel
- Replaced I/C chip for ELT problem
- NICAD batteries nearly discharged. Changed battery charging rate from 0.100 A to 0.200 - 0.300 A

Dec. '79

- Rudder and quiescent flow sensor found tripped after flight
- Modified optical viewing port at panel terminal
- Conducted lab tests on halogen lamp; 20 to 1 improvement verified
- Received solenoid rework to negate armature resonance on flow sensors

Jan. '80

- Reduced NICAD battery charging rate (50 MAH for 5 V batteries and 5 MAH for +3.6 and 6 V batteries)
- Added regulated power supply to ELT circuit
- Modified system test switch from 2 momentary ON (ON center of ON) to ON ON (ON momentary ON)
- Added battery test plug on panel face for external charging and battery checking
- Reprogramed M/P to eliminate erroneous over temp light (Rev. 18, Jan. 80)
- EO 128FT80001 installs improved light source on reservoir pressurization circuit
- 128FT80002 installs wiring to light sources
- 128FT80003 changes flow sensor locking solenoids
- 128FT80005 supplies BATT power instead of transformer power to both light sources
- Conducted resonance vibration test on flow sensors 18-25 Hz resonance occured. Made improvements. Modified solenoid has no resonance points at 5-2000 Hz @ 5, 10, 15 G ranges

Feb. '80

- High intensity of F/O pneumatic circuit improved at display panel
- Color intensity transmission requires additional development

- External battery charger completed at Plant 14
- ELT stops functioning suspected relay
- Generated EO 128FT80006 which installs second high-intensity light at pneumatic bottle test circuit
- Issued EO 128B1636 to add spacer on access door

March '80

- Dessicant sensor approach using internal fiber investigation not successful
- Fabricated third high-intensity source for pneumatic bottle circuit; EO 128FT8006 will install unit in vehicle
- Procured high-capacity ELT relay

April '80

- Developed new dessicant sensor (cobalt chloride/potassium bromide disc)
- Installed access door spacer

May '80

• Improved optical dessicant sensor with plastic spacer for isolation due to chemical reaction

June '80

- Added short fiber cable link between modified dessicant optic receiver and junction
- Increased light loss

July '80

- Detected poor F/O cable runs with 32 dbm losses instead of 10 dbm, which might be expected
- Investigate F/O improvements

August '80

• Continue flight test program

Sept. '80

• Continue system interrogation and assessment

Oct. 180

• Continue system flight test and assessment

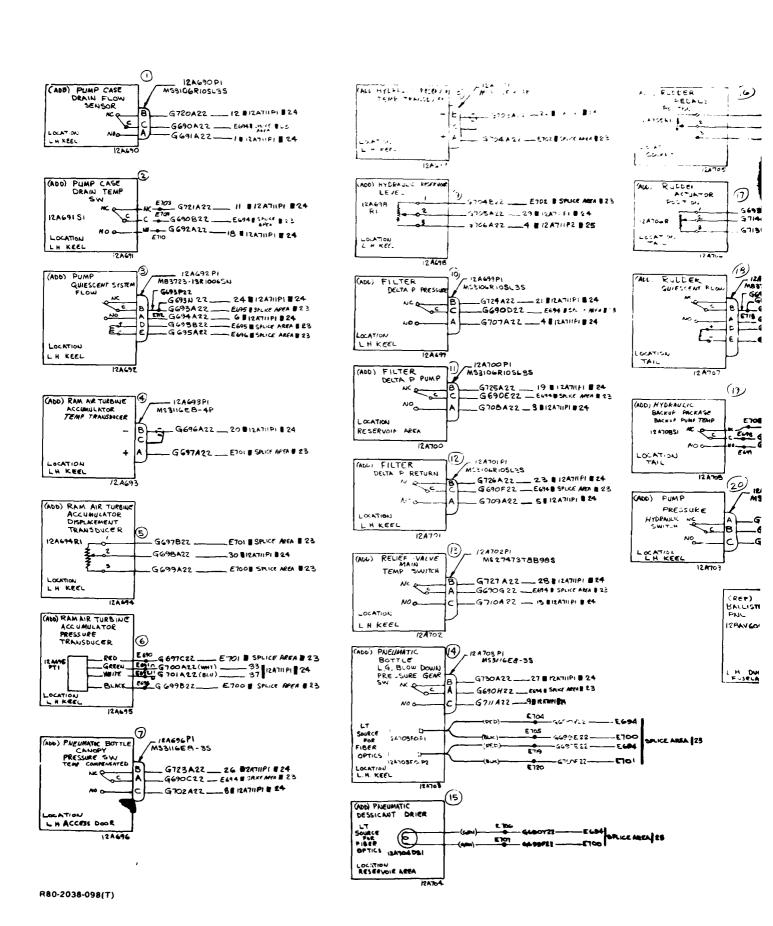
Nov. '80

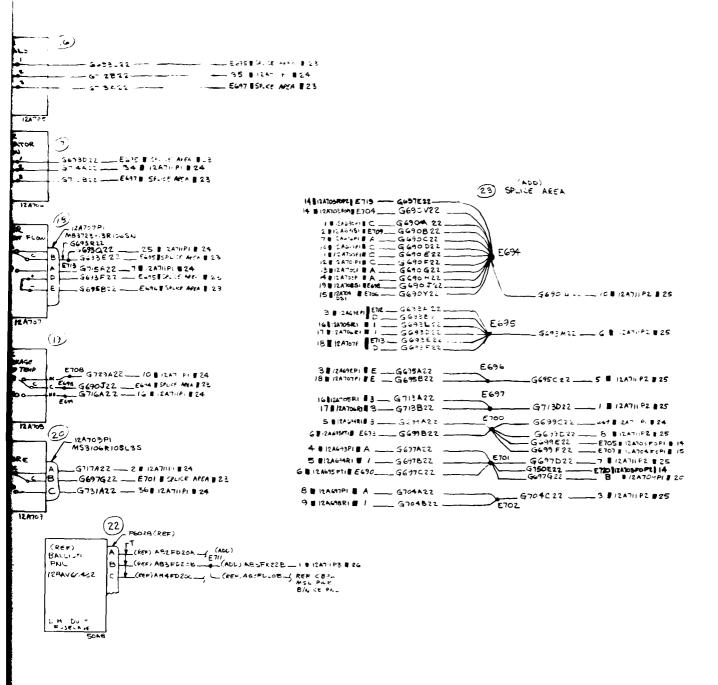
• Issue system debailment EO for HYCOS

Dec. '80

- Return test vehicle to U.S. Navy
- Complete final report

APPENDIX D HYCOS WIRING DIAGRAM





.

24) 12A711 PI M81511/56FD9153 (ADD) DISPLAY FANEL G725 A22
G720 A22
G720 A22
G724 A22
G724 A22
G725 A22
G727 A22
G730 A22
G708 A22 19 FILTER DECTA P PUMP 12 PUMP CASE DRAIN FLOW 11 PUMP CASE DRAIN TEMP 11 # 12A700PI # B PUMP CASE DRAIN TEMP
BACKUP PUMP TEMP
FILTER DELTA P PRESSURE
5 FILTER DELTA P RETURN
1 PHEUMATIC BOTHE (MOMPY PRESSURE
7 PHEUMATIC BOTHE (MOMPY PRESSURE
7 PHEUMATIC BOTHE LE BLOW DIMM PRESSURE
MIND CASE DRAIN FLOW
FILTER DELTA P PUMP
PUMP CASE DRAIN TEMP
BACKUP PUMP TEMP
BACKUP PUMP TEMP
FILTER DELTA P PRESSURE
PILTER DELTA P RETURN
PHEUMATIC BOTHE CANOPY PRESSURE
PHEUMATIC BOTHE CANOPY PRESSURE
PHEUMATIC BOTTE LE BLOW DOWN PRESSUR
PREMIMATIC BOTTE LE BLOW DOWN PRESSUR
RELIEF VALVE MANN TEMP PUMP PRESSURE
PUMP QUIESCONT SYSTEM FLOW
RUDDER QUIESCONT FLOW 3 112AG92P1 18712 G693N 22 18 112A 707P1 18712 G693 Q 22 PUMP PRESSURE HYLPAUL SWITH
PUMP QUIESCENT SYSTEM FLOW
RUDDER QUIESCENT FLOW
RUDDER ACTUATOR POSITION
RUDDER PEDALS POSITION G703AZZ - 22 G705AZZ - 29 8 #12A697PI # B __ RESERVOIR TEMP 9 #RAMBRI# 2 ____ G705AZZ ___ RESERVOIR LEVEL 4 1 12A699PI B _____ 6696A22 ____ 20 20 RAM AIR TURBINE ACCUMULATOR TEMP 5 12A694R1 2 ____ G698A22 _ 30 RAM AIR TURBINE ACCUMULATOR DISPLACEMEN 6 12A69571 E691 G700A2C(6).0 11 33 RAM AIR TURBINE ACCUMULATOR PRESSURE
25 SPICE AREA 1200 G699C22 West Area 1200 G699C22 25 SPLKE AREA E700 ___ 20 8 12410 1P1 . C _ ___ G731A22 _ 36 PUMP PRESSURE HYDRAULIC SWIT H 12 ATI1 P2 (25) MBISII/46FBOISI 238 SPLICE AREA 8 E694 ____ G690422 . TO + T1 + 57 SW 238 SPLICE AREA # E 695____ G693M22 -23 8 SPLICE AREA # E696____ G695 C 22 _ GRD 23 # SPLICE AREA # E697____ G7130 22 _ GRD 23 SPLIKE AREA # E700____ G699D22 . GRD 23 # SPLICE AREA # E701 ___ G697022 -+ 5 V 23 # SPLICE AREA # E702 ____ G704C22 +5 > 9 # 124698RI # 3 ___ G706AZZ. GRD (26) 12A711P3 . M81511/46FA0151 22 P(028 | E7// ____ AB3FK228. 115 VAC 400 HE PH B PRIMARY __ G719A22N . GRD LOCATION LH BOARDING LADDER 17A31

D-3/4

1

20

APPENDIX E

PARTICIPATING FIRMS

Aircraft Porous Media	Glen Cove, N.Y.
Walter Kidde & Company	Belleville, N.J.
Valtec	West Boyleston, Mass.
Sigma-Netics	Mountain Lakes, N.J.
Sprague Engineering Corporation	Gardena, California
Bourns Incorporated	Riverside, California
Neo-Dyn Inc	Chatsworth, California
De Laval Special Products Division	Cleveland, Ohio
Entran Devices	Norwood, Massachusetts
Frisby Airborne Hydraulics	Freeport, N.Y.
E.I. du Pont de Nemours	Wilmington, Delaware
Intel Corporation	Santa Clara, California
Texas Instruments	Attleboro, Mass.
Hunter Spring Division of Ametek	Hatfield, PA
Russel Associates	Bay Shore, N.Y.
Eagle Technology	Arlington, Virginia
Kulite Semiconductor Products	Ridgefield, N.J.
Sealectro Corporation	Mamaroneck, N.Y.
Ultra Sensors	Minneapolis, Minnesota
Resistoflex Corporation	Vineland, N.J.
Analog Devices	Norwood, MA
Photodyne Incorporated	West Lake Village, CA
Polaroid Corporation	Cambridge, MA
Roylan Optics Company	Arcaria, CA

APPENDIX F

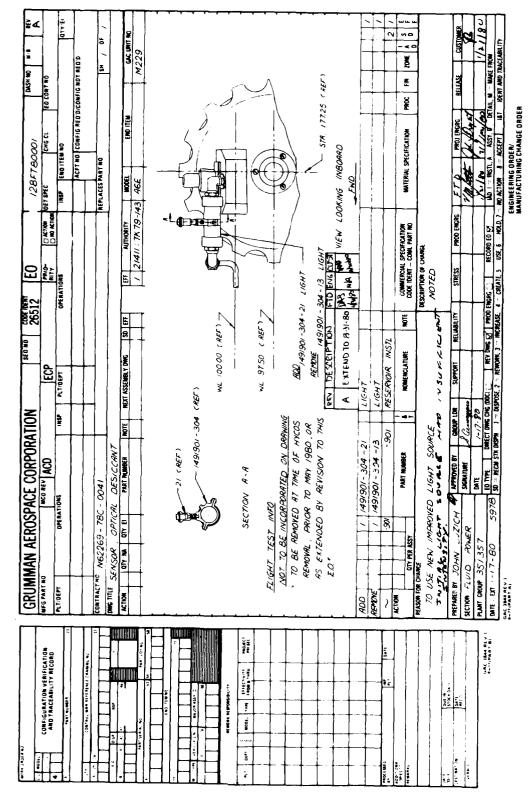
ESTIMATED WEIGHT OF PROTOTYPE FULL-BLOWN SYSTEM

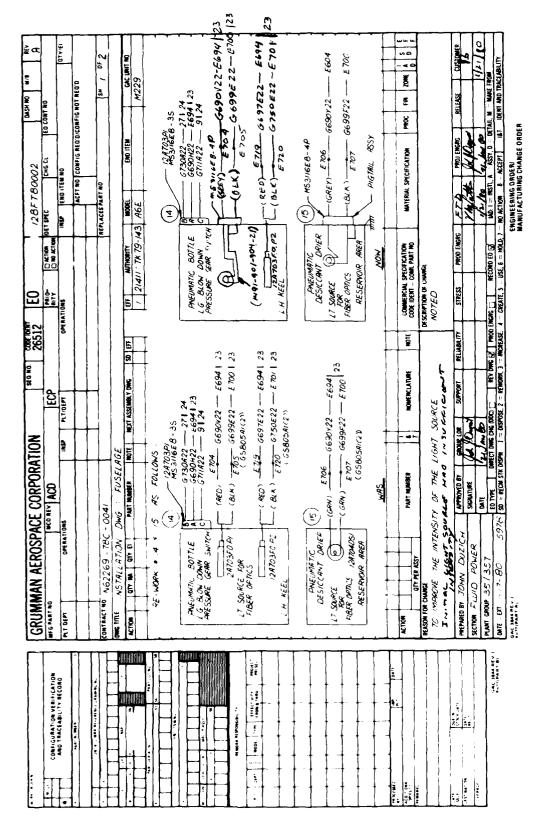
ITEM	DESCRIPTION	COMBINED	FLIGHT
1	DISPLAY PANEL	6.00	_
2	RESERVOIR		
	PISTON DISPLACEMENT		
	- POTENTIOMETER	0.08	0.08
	BRACKETS, ADAPTORS,		
	& HOUSING	2.38	2.38
	TEMPERATURE TRANSDUCER	0.12	0.12
3	FILTER DIFFERENTIAL PRESSURE		
ĺ	• INDICATORS	0.57 (6)	0.57 (5)
	• MULTICATORS	0.36 (1)	0.36 (1)
4	PRESSURE SWITCH		
	TEMPERATURE COMPENSATED	0.25 (5)	_
5	FLOW SENSORS		
	QUIESCENT	1.39	1.39
İ	 RUDDER ACTUATOR 	0.57	_
	PUMP CASE	0.52	0.52
6	PRESSURE SWITCH SYSTEM	0.09	0.09
7	TEMPERATURE SWITCH		
	• CASE DRAIN	0.13 (2)	0.13 (2)
	FILTER MODULE (R.V.)	1	
	 FLIGHT CONTROL BACKUP MODULE, TEMPERATURE SWITCH 		
			_
8	POTENTIOMETER ROTARY		
	RUDDER PEDALS	0.08	_
	RUDDER ACTUATOR	0.08	_
9	TRANSDUCER, PRESSURE	0.18 (3)	0.18
10	TRANSDUCER, TEMPERATURE	0.12 (3)	0.12
11	WIRING, CLAMPS & CONNECTORS, BRACKETS	3.00	3.00
12	DETECTOR, LIQUID	0.03 (5)	-
		20.78	11.35
		TOTAL:	32.13

APPENDIX G ENGINEERING ORDERS

NUMBER	TITLE
128FT80001A	Sensor, Optical Desiccant
128FT80002A	Installation Dwg, Fuselage
128FT80003A	Flow Sensor, Bypass Type
128FT80005A	Installation Dwg, Fuselage
128FT80006	Installation Dwg, Fuselage
128FT80007	Sensor, Optical Desiccant
128FT81003	Hycos, Removal
128EL10401AFZ	Lines Installation, Fuselage
128EL10401AF3	Lines Installation, Fuselage
128EL10401 -	Lines Installation, Fuselage
128EL4118T4	Lines Installation, Fuselage
128EL4222 -	Lines Installation, Fuselage
128EL10403T4	Lines Installation, Fuselage
128EL10403T5	Lines Installation, Fuselage
128EL66010L4	Lines Installation, Fuselage
128EL66013M1	Lines Installation, Fuselage
128EL66021L2	Lines Installation, Fuselage
128EL66041K5	Lines Installation, Fuselage
128EL66047M2	Lines Installation, Fuselage
128EL66053K5	Lines Installation, Fuselage
128EL66058F2	Lines Installation, Fuselage
128EL66060L4	Lines Installation, Fuselage
128AB60012	Exterior Markings
128AV66014U5	Installation Drawing, Fuselage
128AV66014V2	Installation Drawing, Fuselage
128B11380AB1	Duct Assembly, Fuselage
128C130001P1	Controls Installation, Directional

NUMBER	TITLE
128CS10000 -	Potentiometer Installation, Rudder
128CS10000W1	Potentiometer Installation, Rudder
128H10009V1	Components Installation
128H10009V2	Components Installation
128H10009V3	Components Installation
128H10049J1	Components Installation
128H10127F1	Reservoir Installation
128H10127F2	Reservoir Installation
128H10136N1	Regulator Installation
128H10136N2	Regulator Installation
128H10312G1	Installation, Components
128H10009W2	Components Installation





FUGHT TEST E.Q. NOT TO 8E NOCKP ON DIAG REMOVE REIOR TO 1 MAY 80. NOT TO 8E NOCKP ON DIAG REMOVE REIOR TO 1 MAY 80. NOT TO 8 NOT TO	AT POST PERSONNEL ST	GRUMMAN AEROSPACE CORPORATION	26512	E0	128FT 500CZ	DASH NO	ĕ ⊄
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Part 1986	SETION FLUID POWER	7	H		\vdash	1/4/6	11000		13
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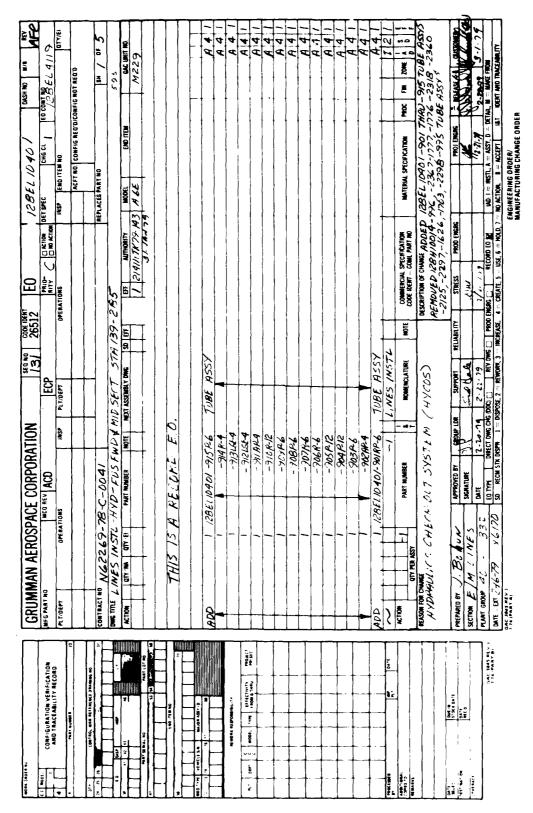
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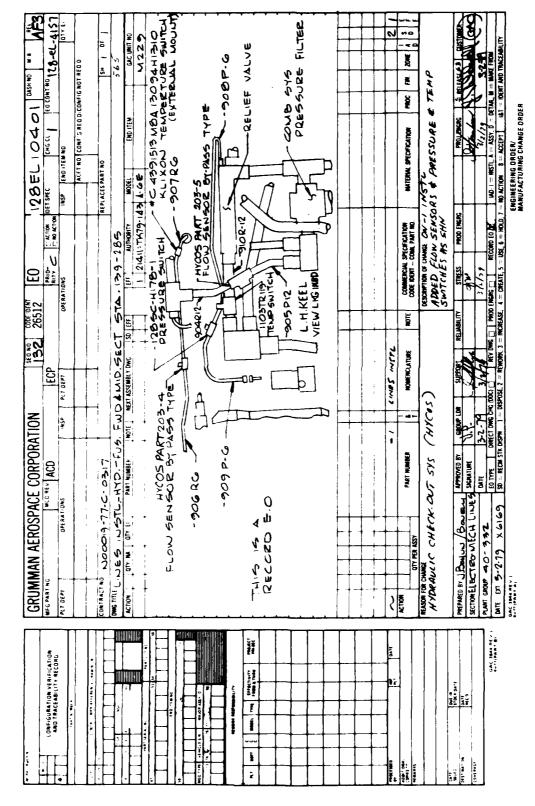
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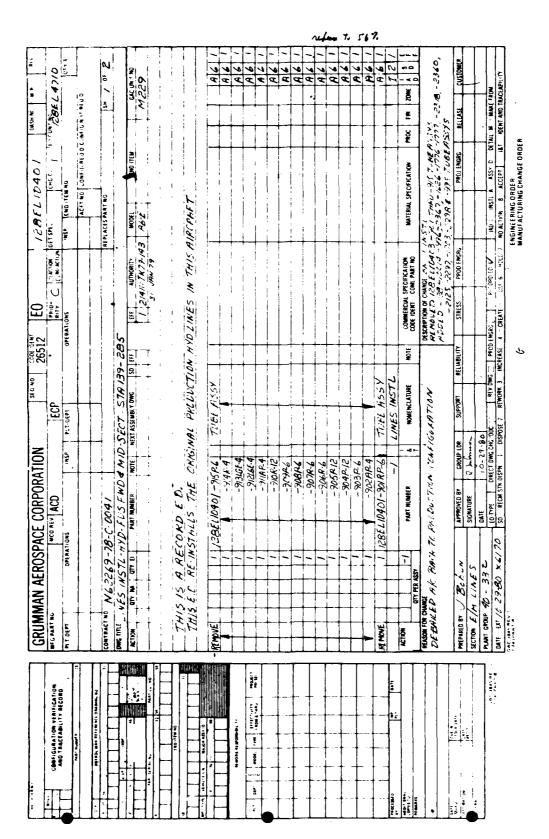
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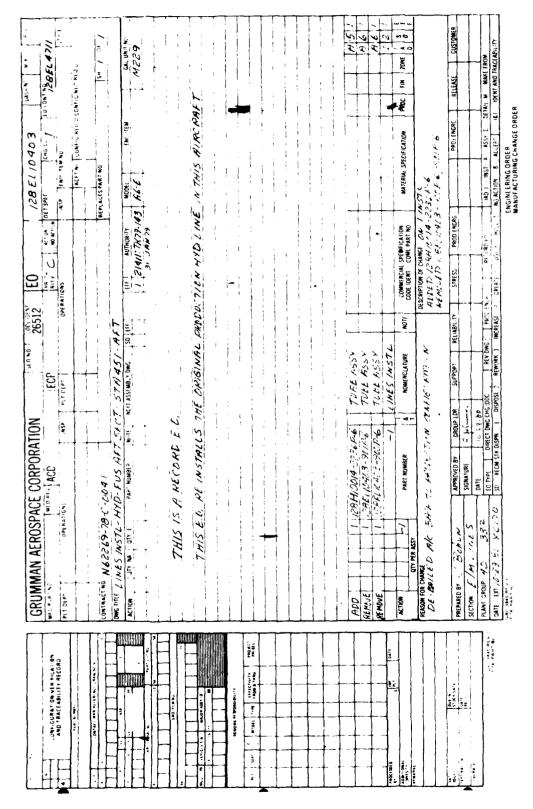
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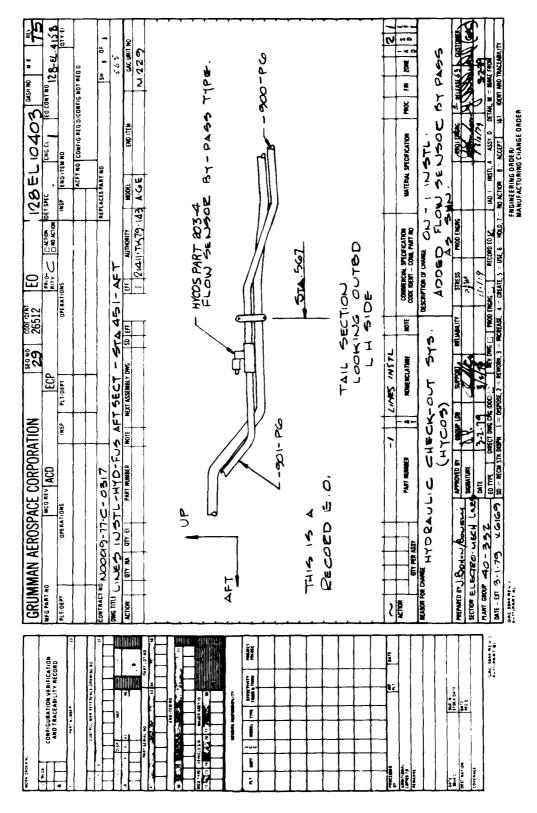




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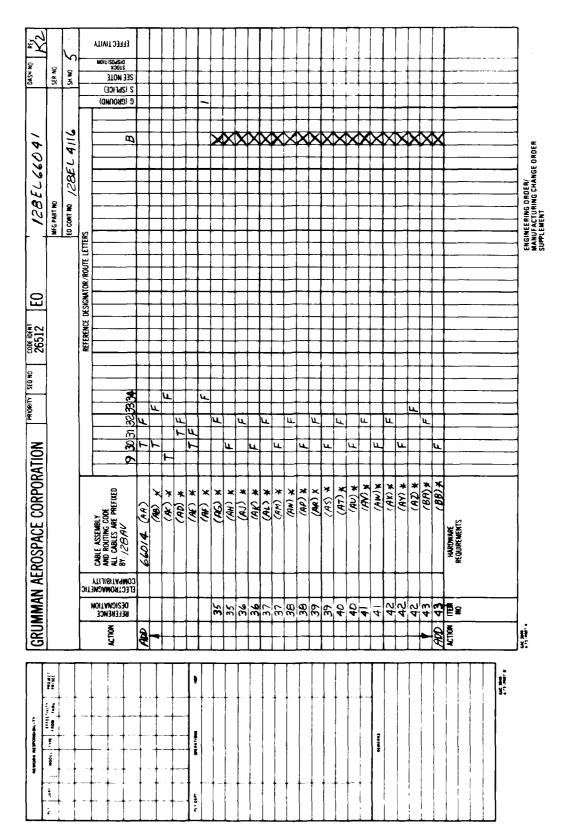
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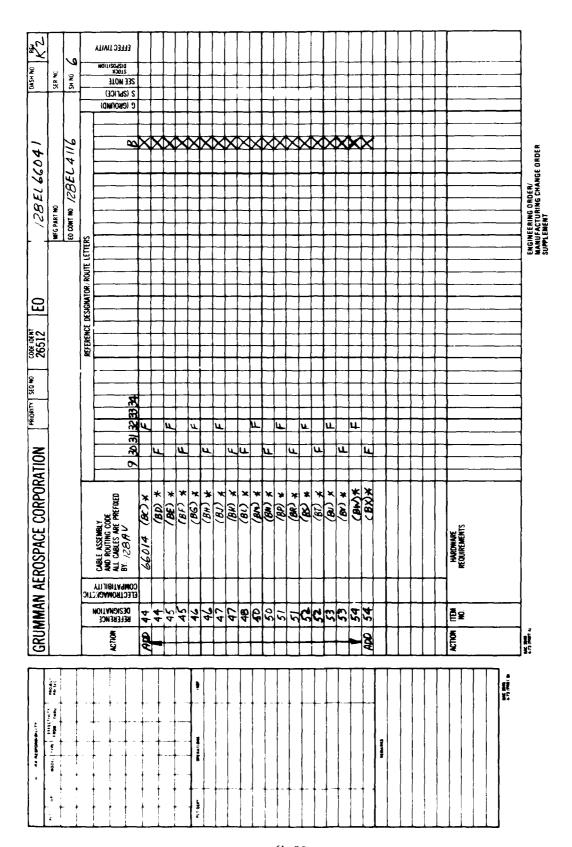
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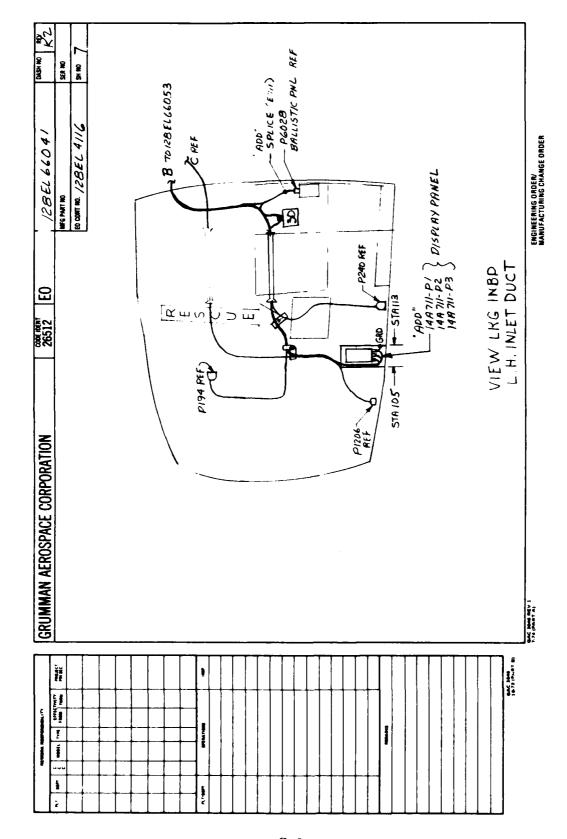
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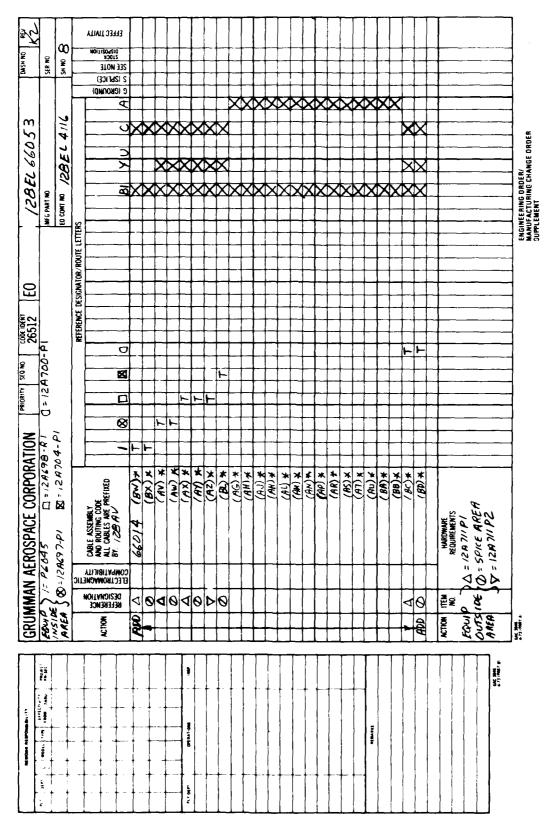
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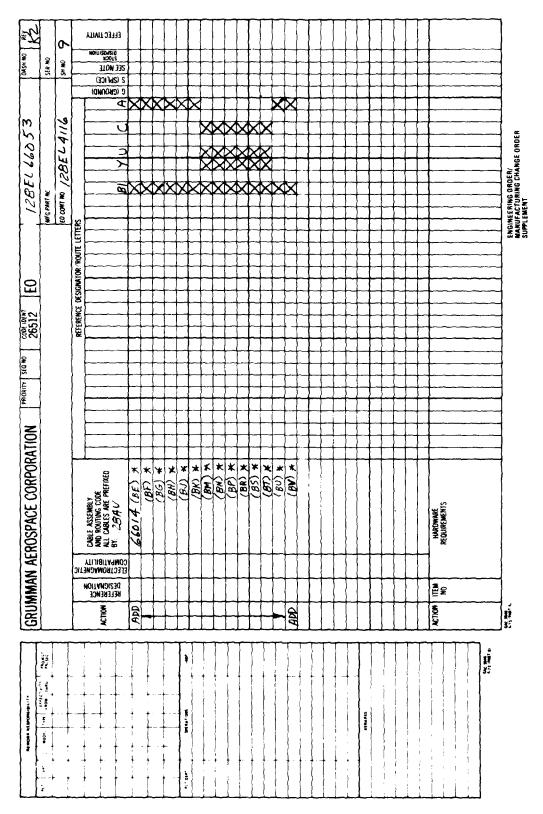


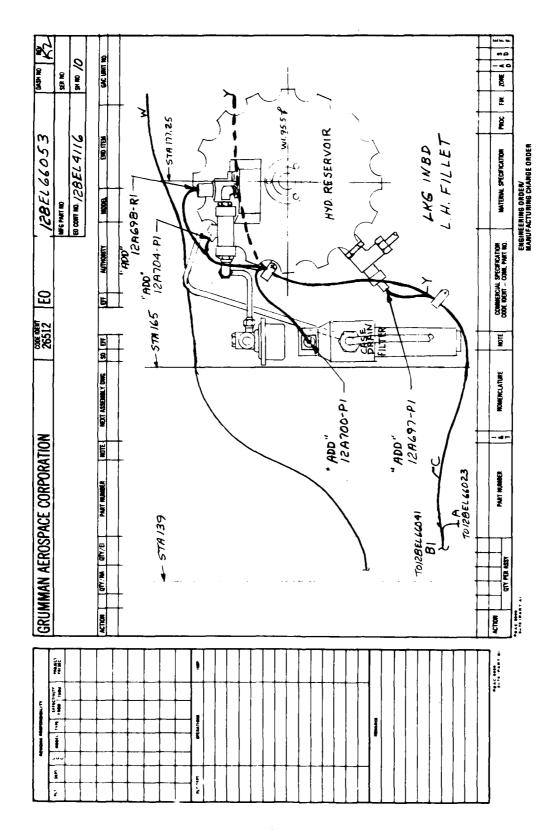


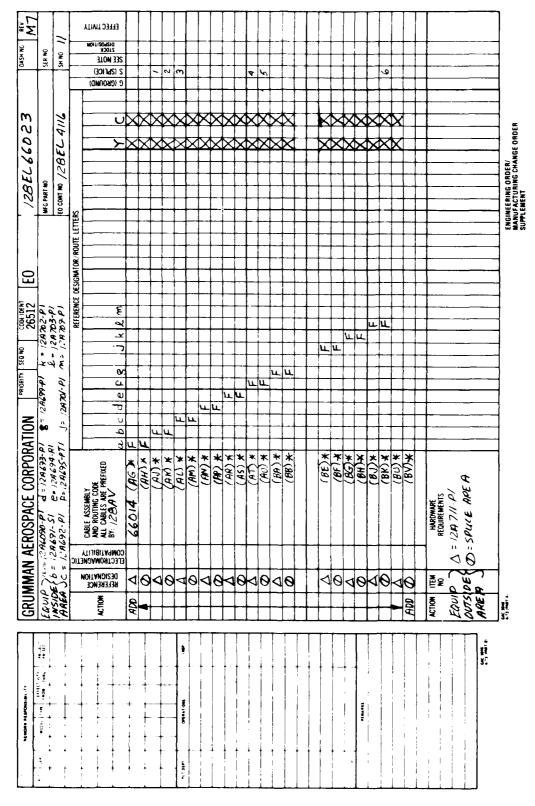


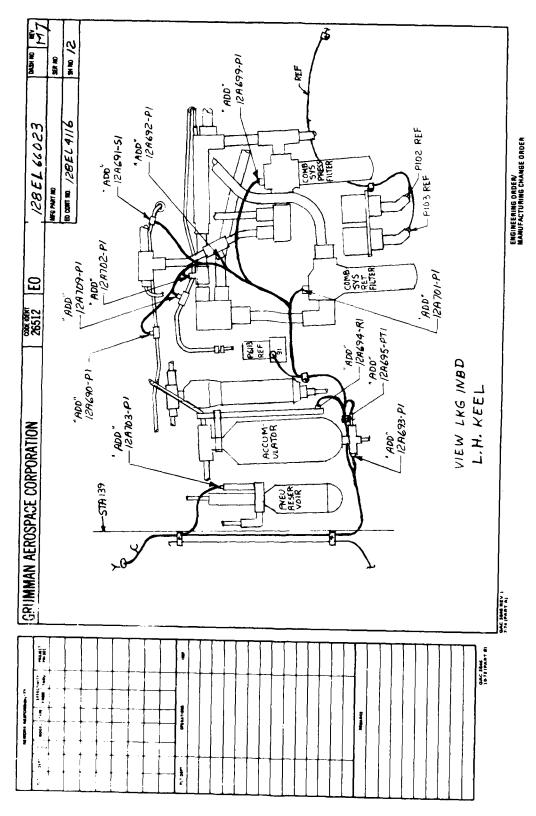


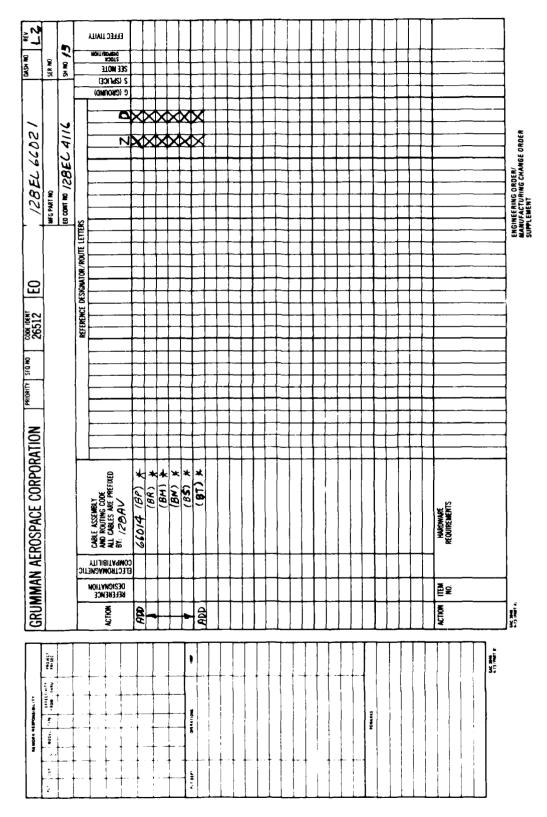
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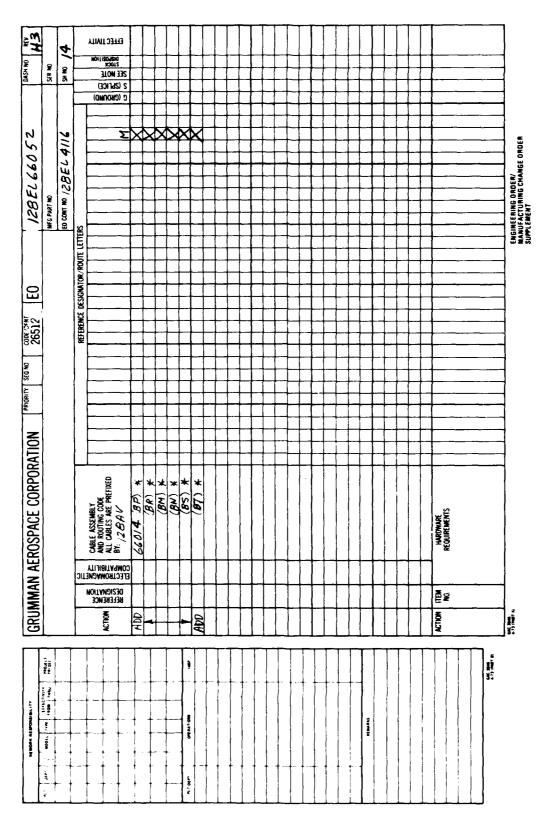


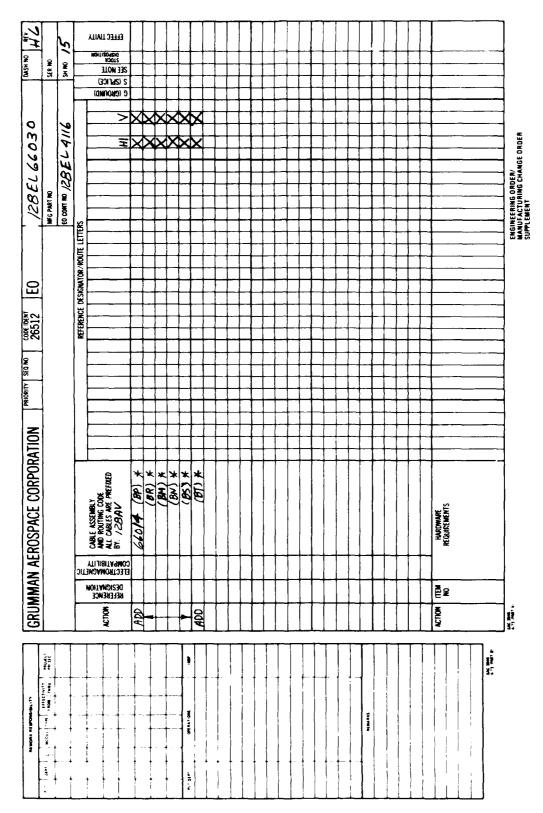


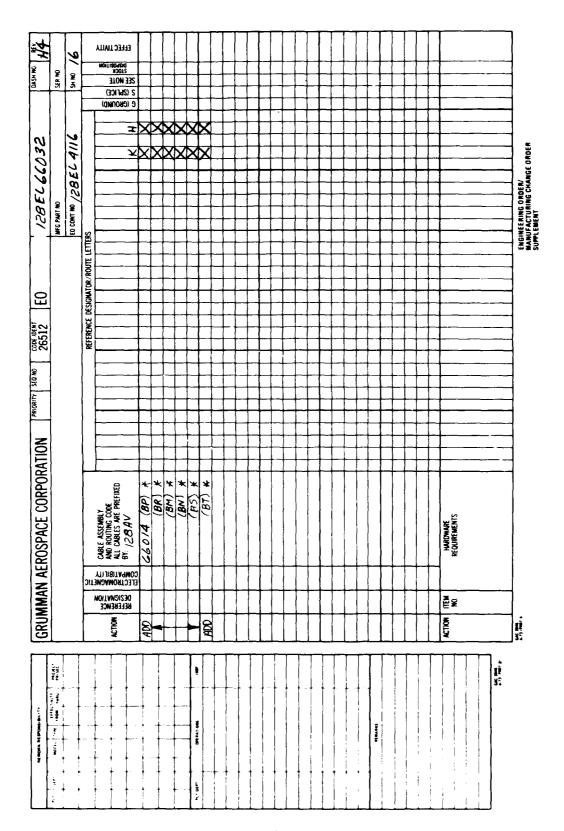


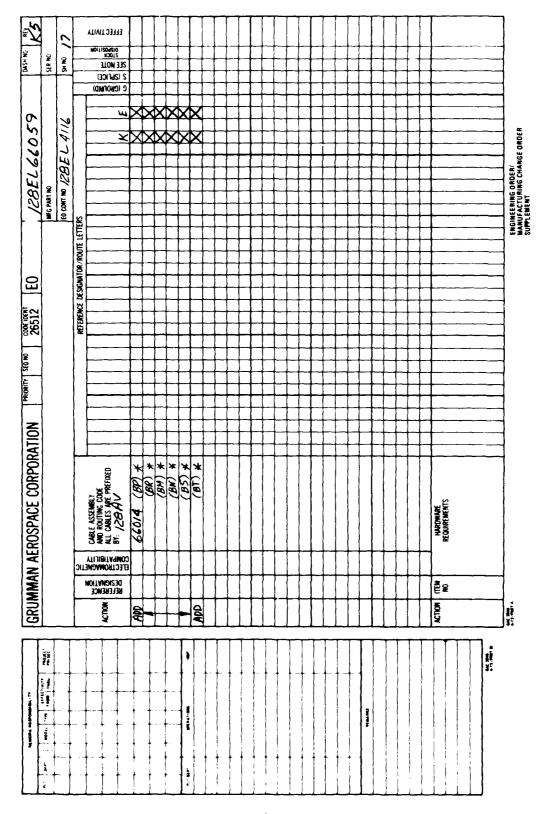


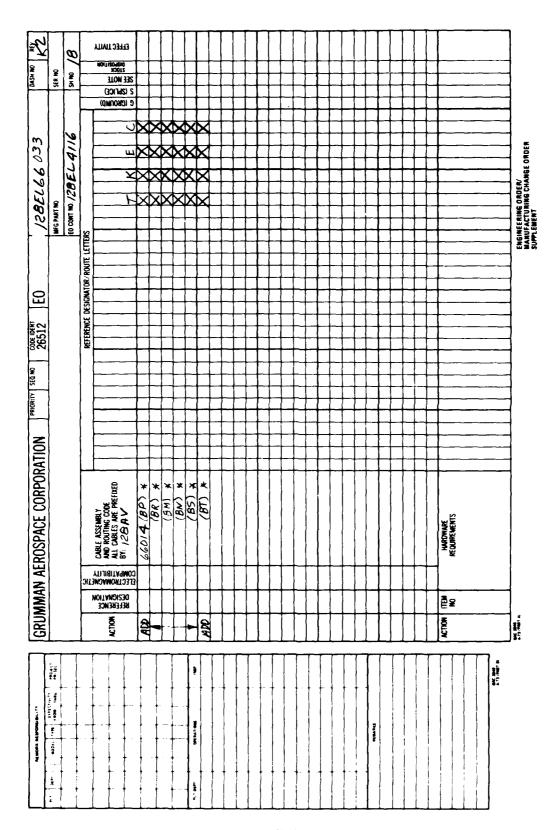


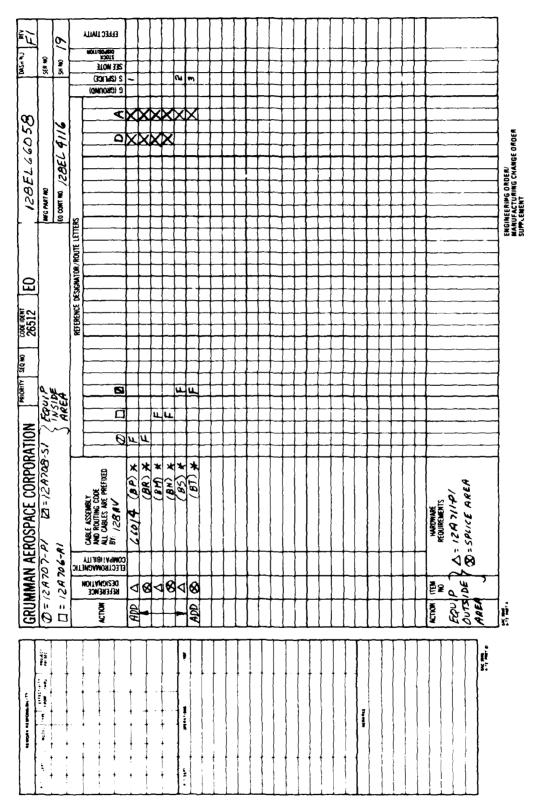


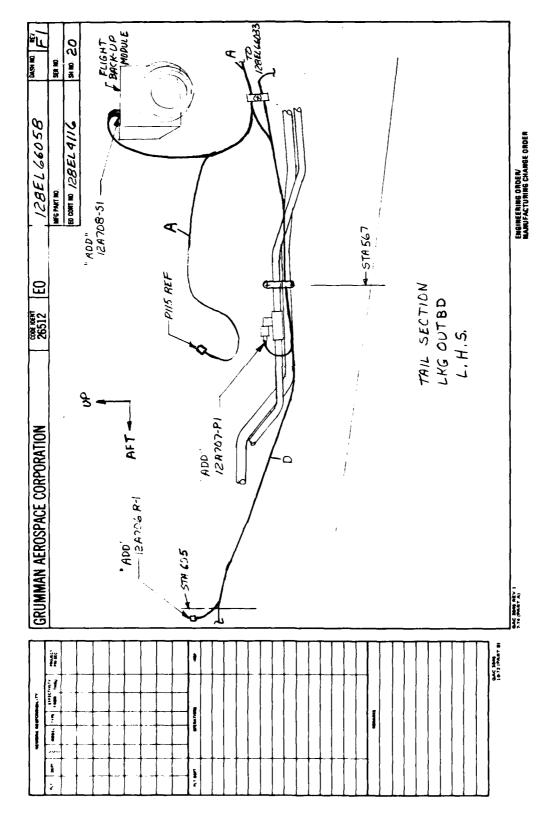


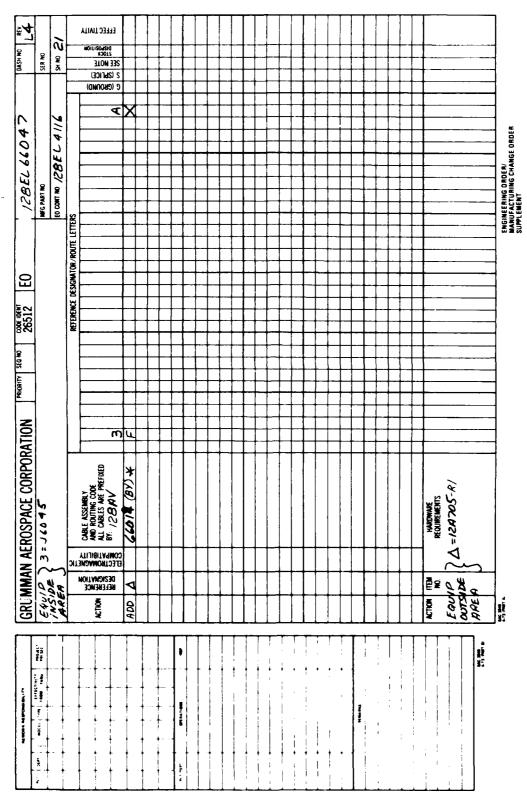


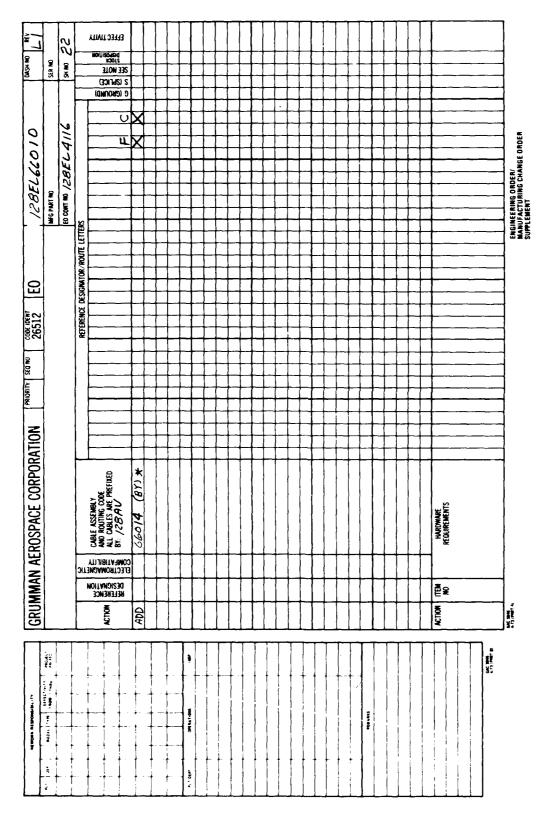


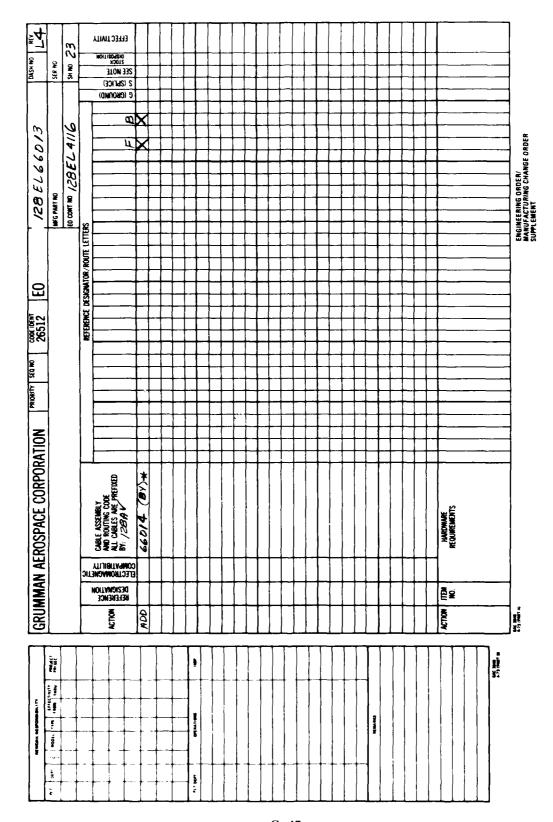


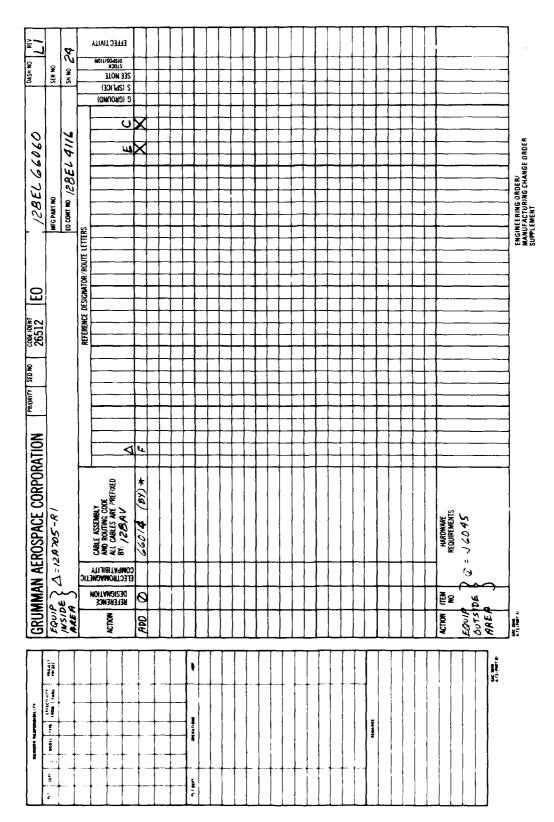


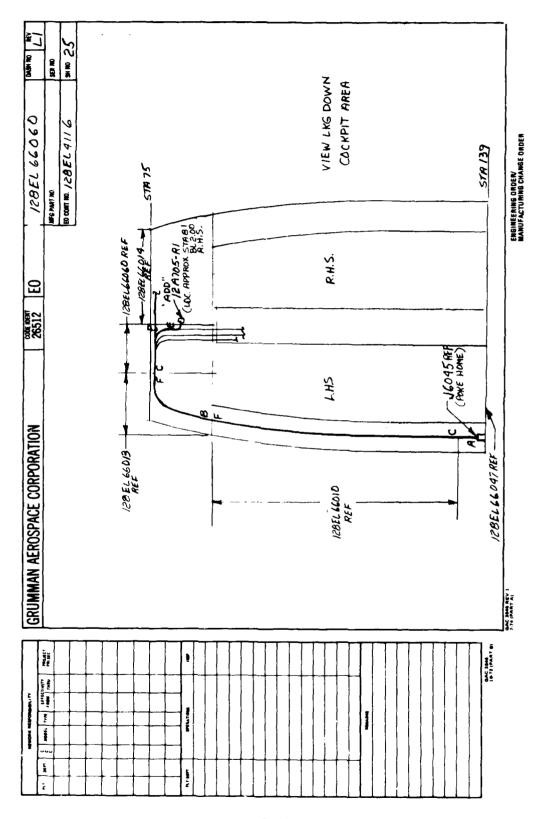


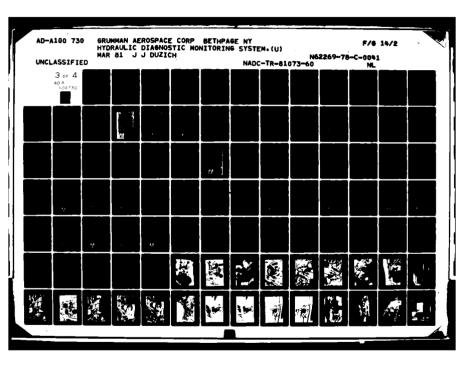










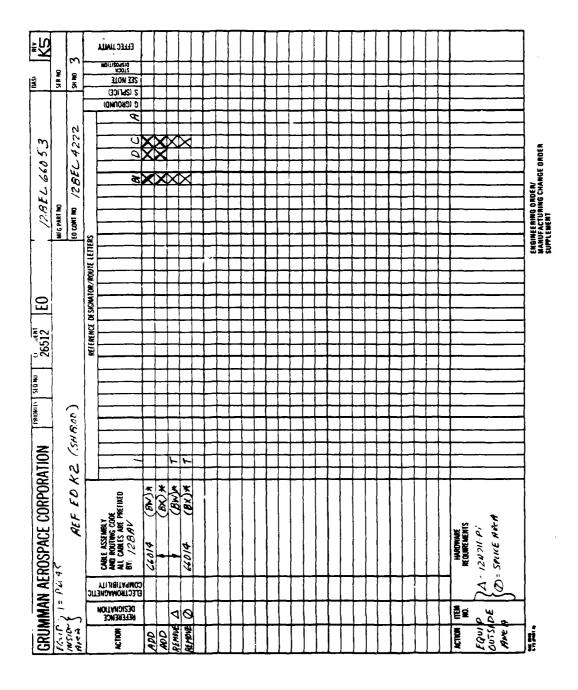


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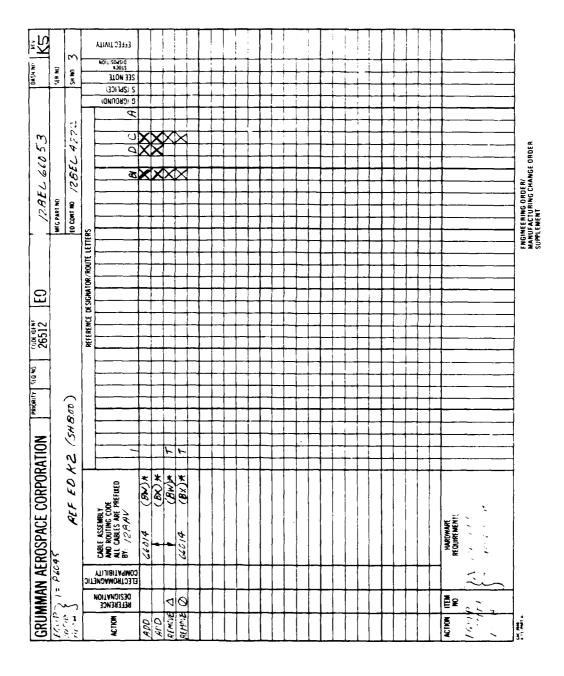
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ENGINEERING ORDER/ MANUFACTURING CHANGE ORDER

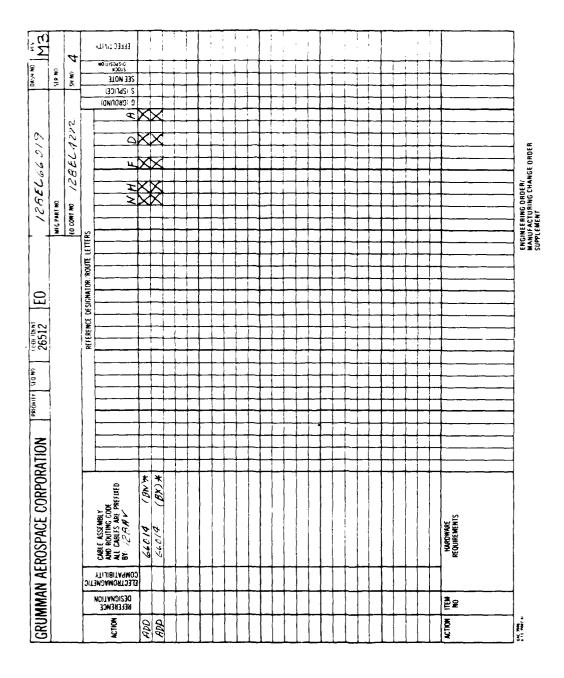
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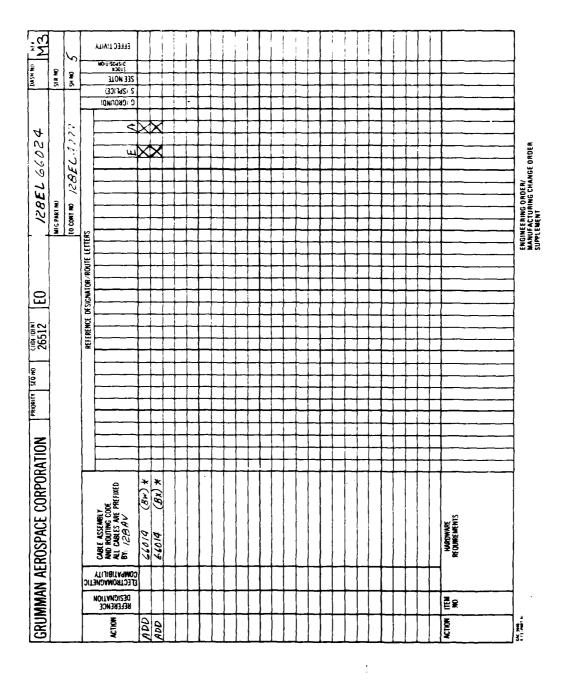
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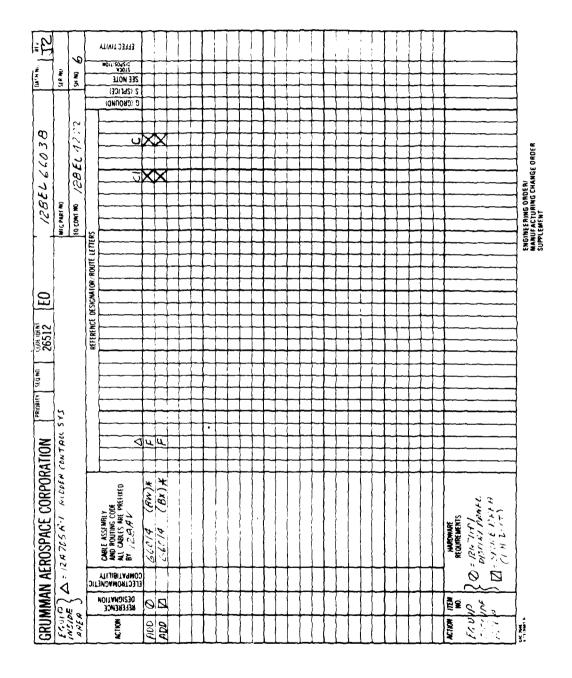
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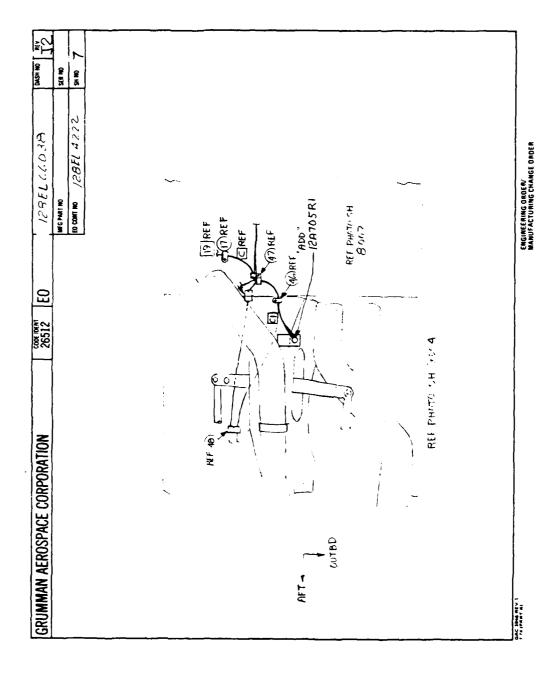


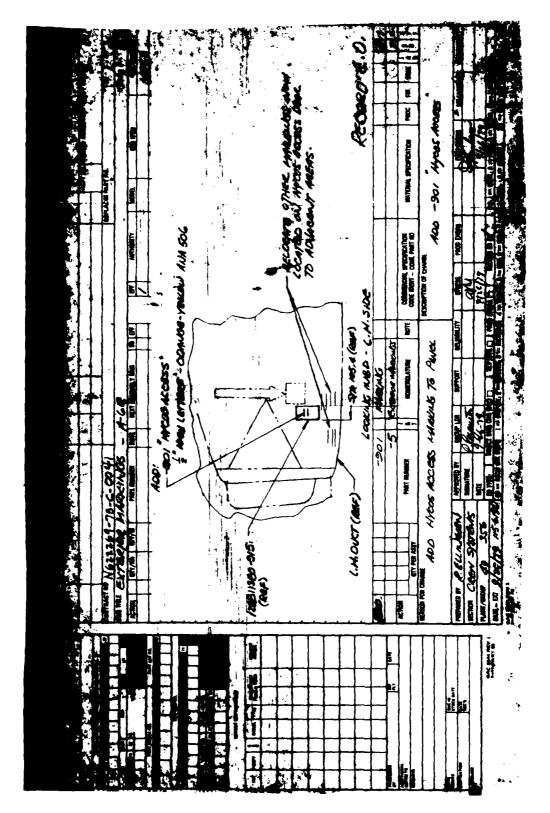
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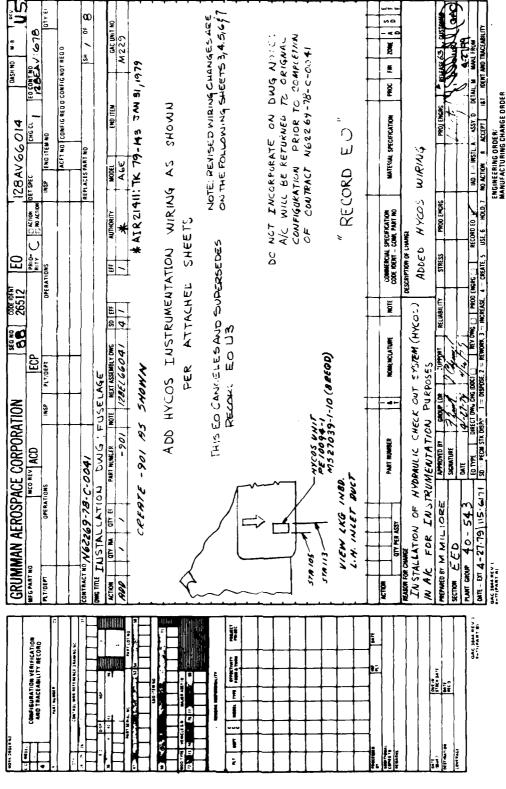
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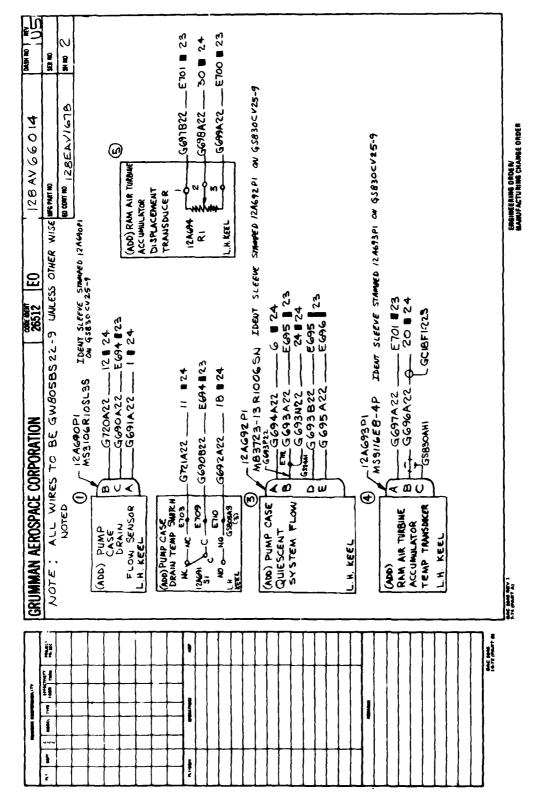


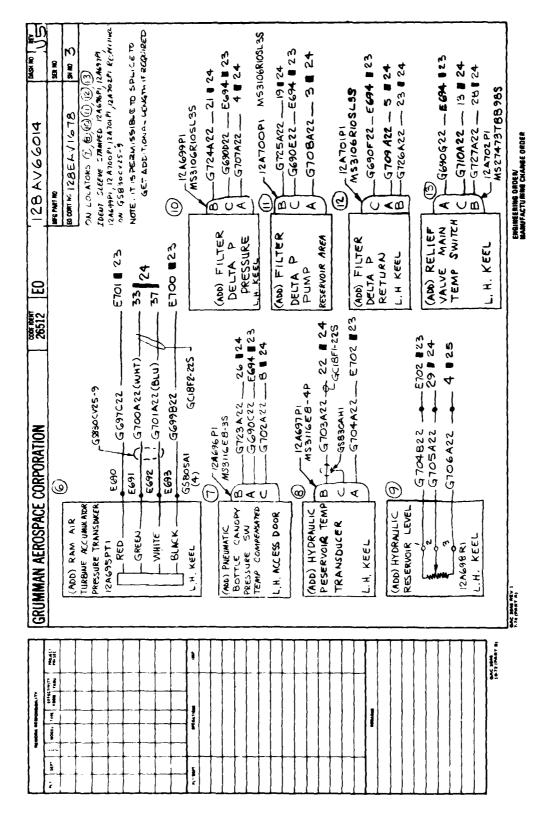




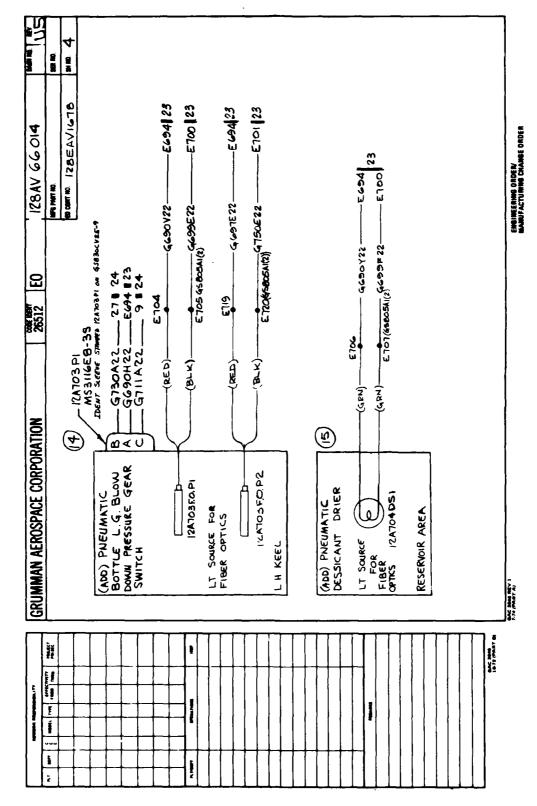
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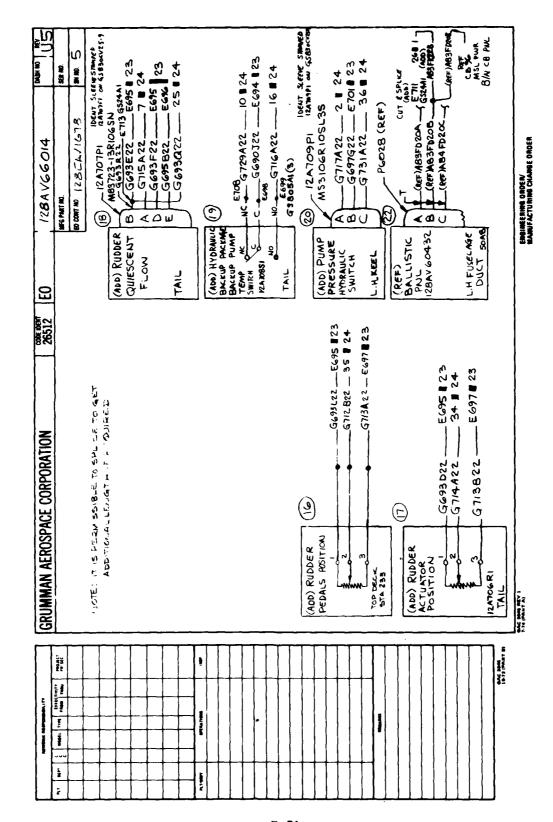




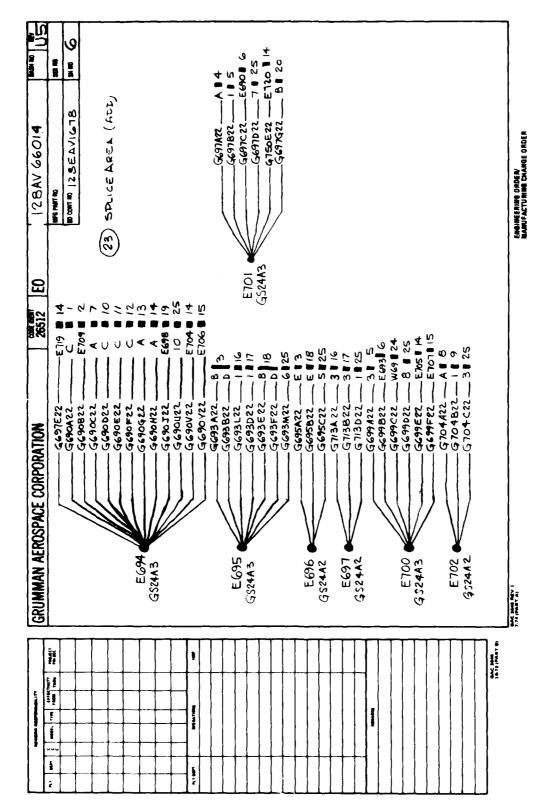


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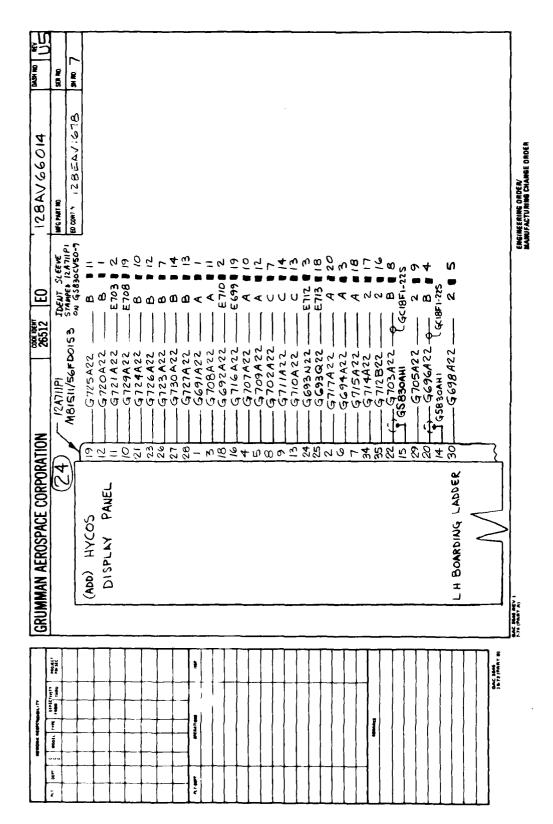


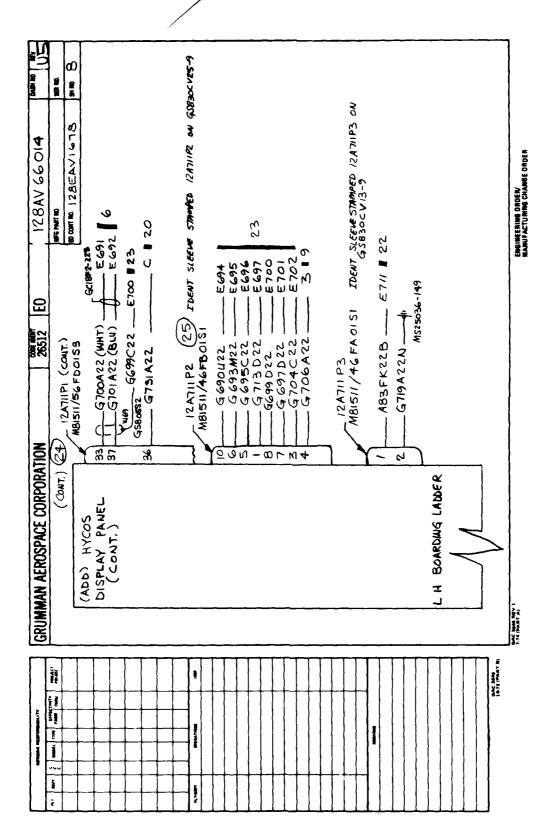


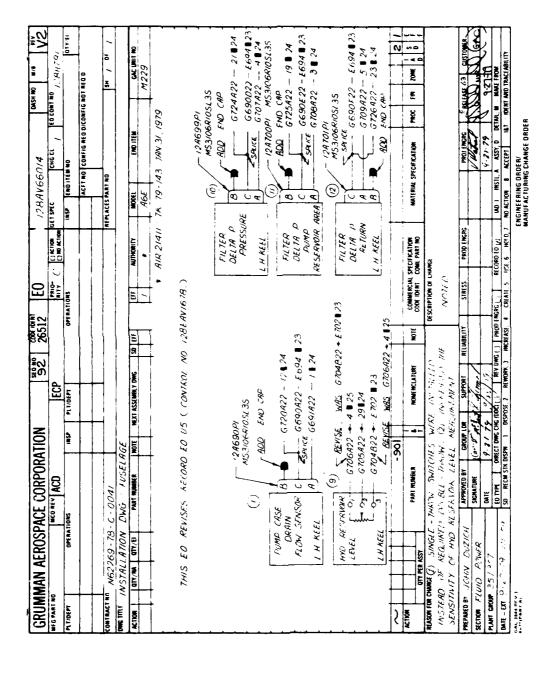
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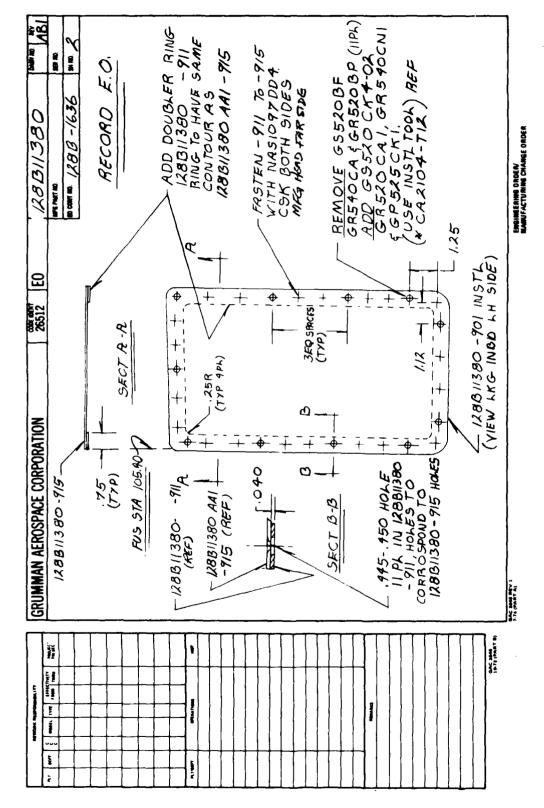


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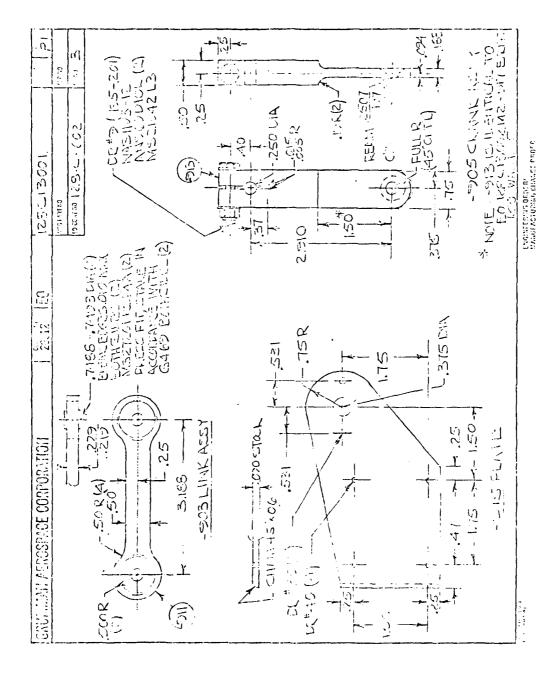
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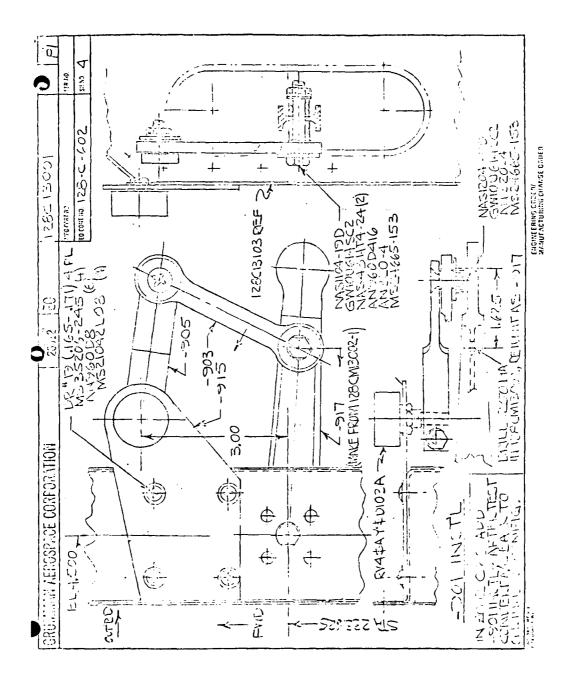
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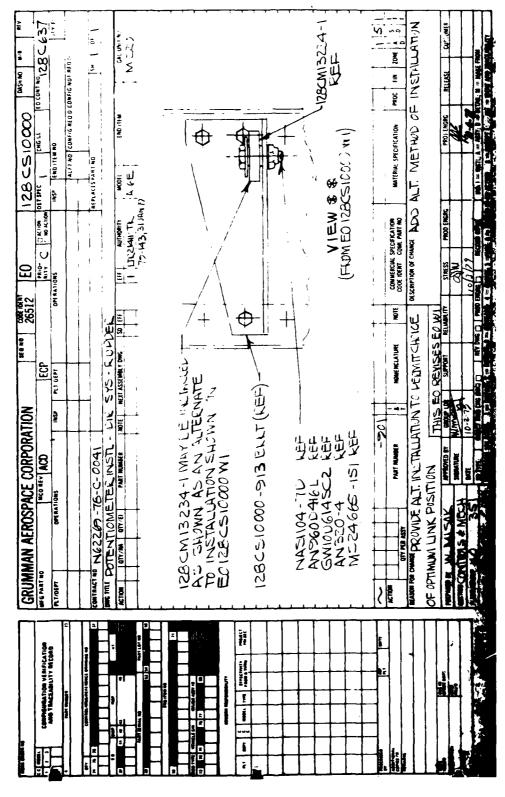
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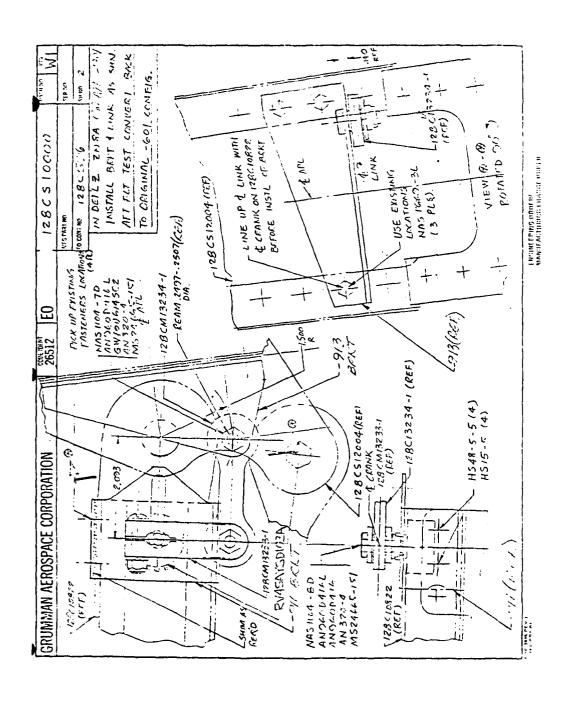
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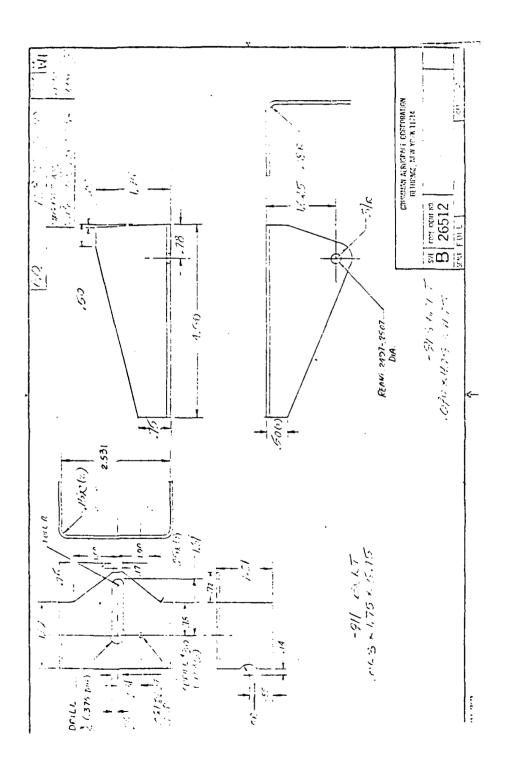






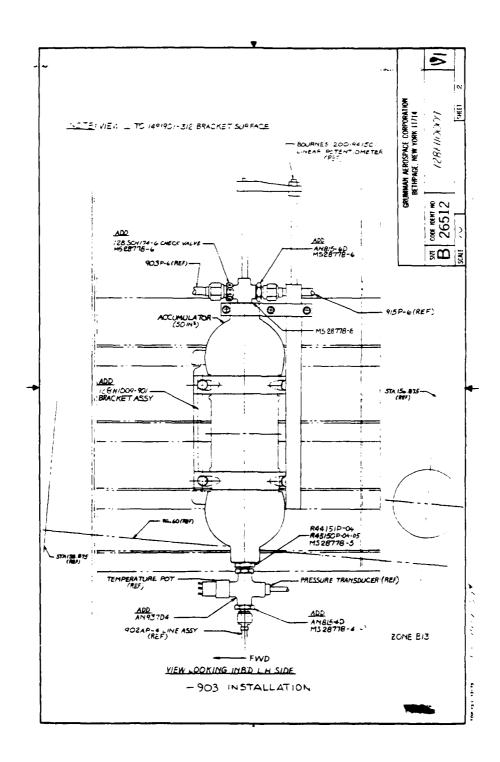
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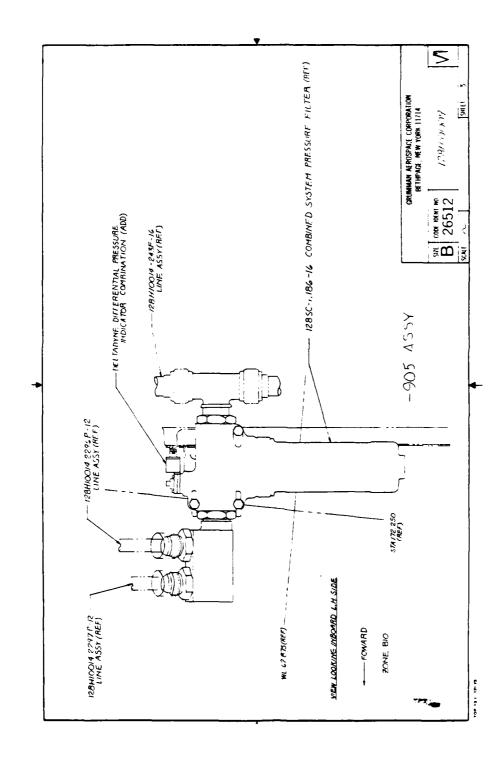


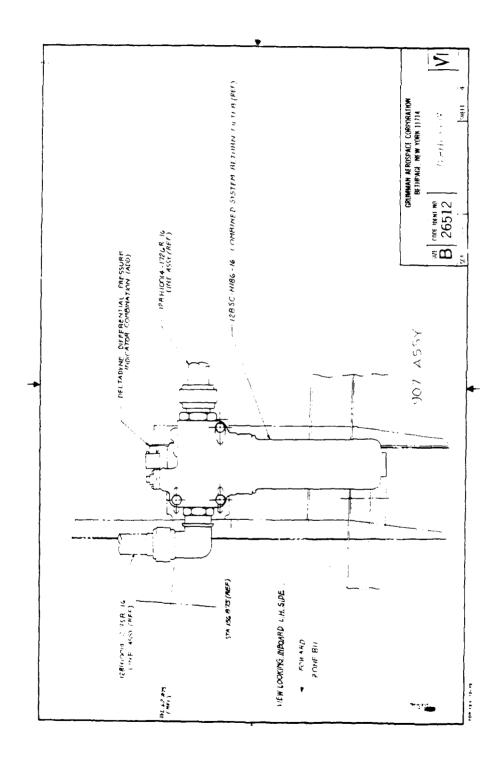


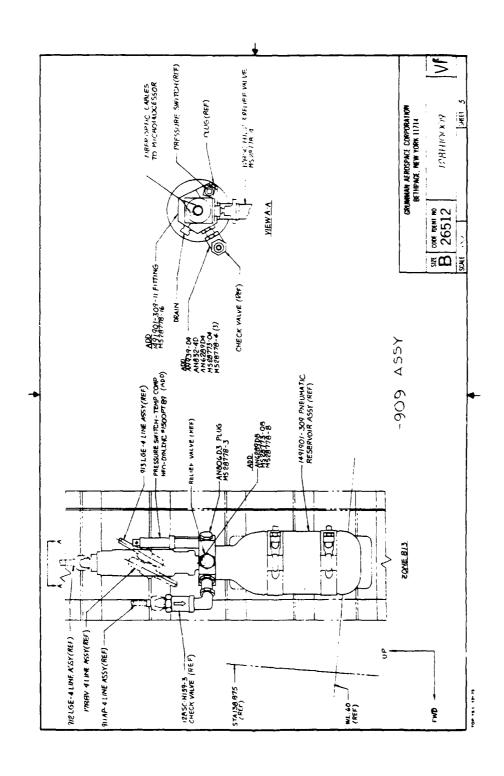
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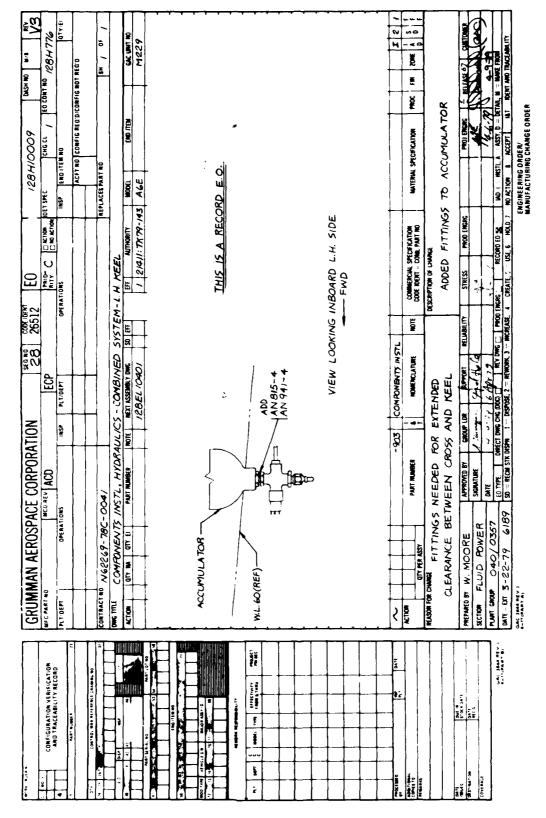






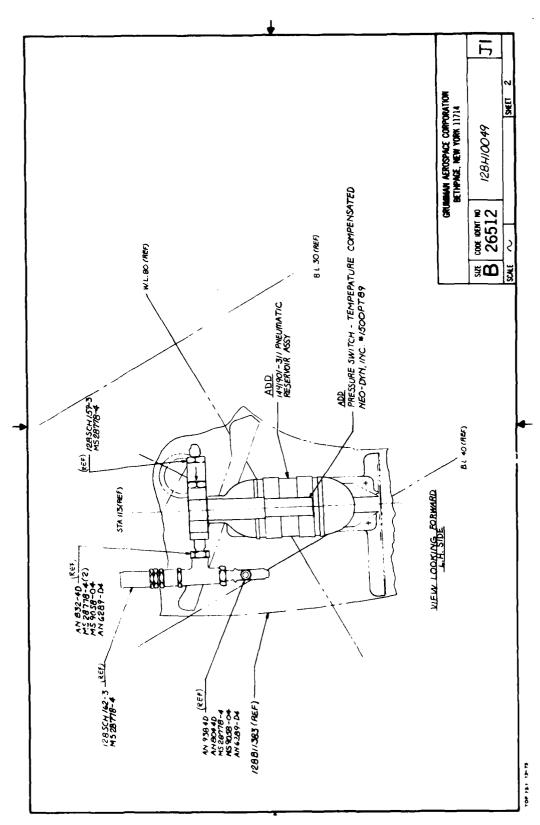


COMFIGURATION VERIFICATION AND TRACEASILITY RECORD	GRUMMAN AERONTAL	IMAN AEKUSPACE CURPURATION		27 26512	E0	128H10009	
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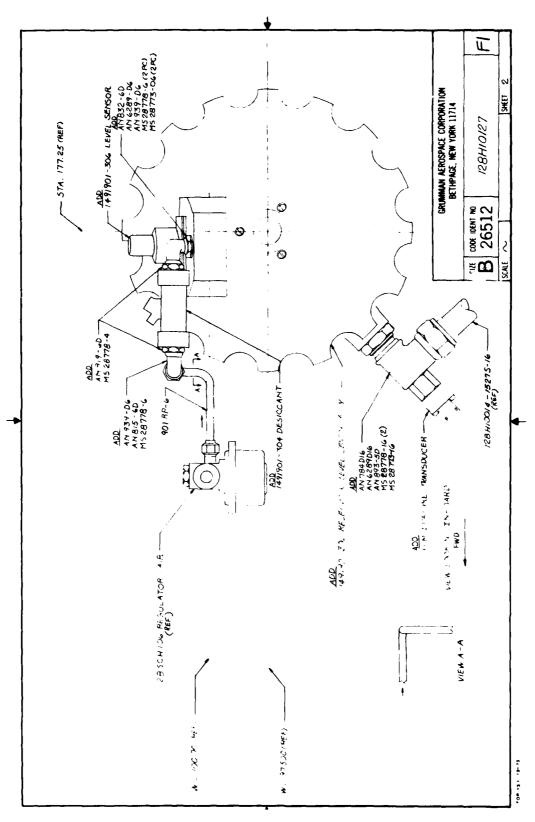


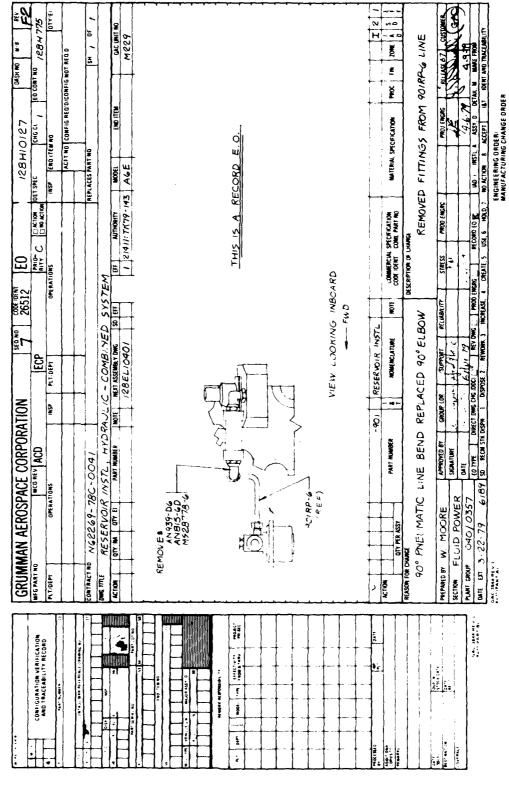
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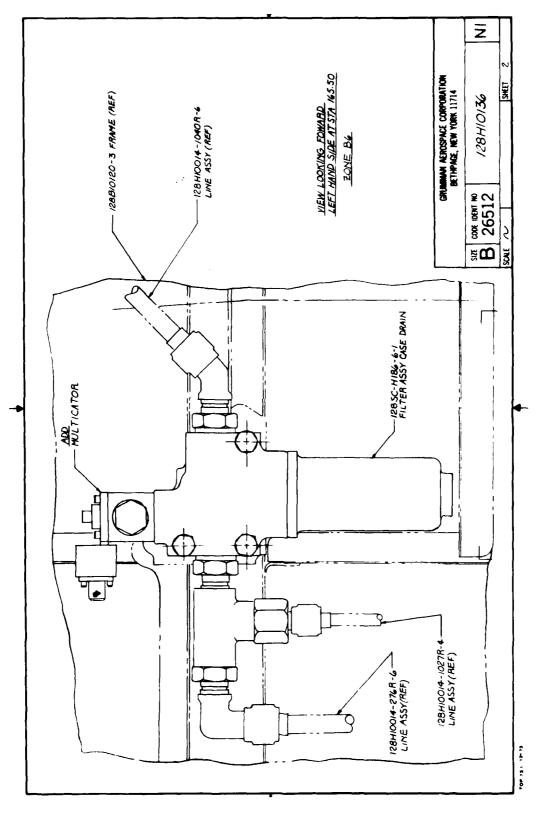


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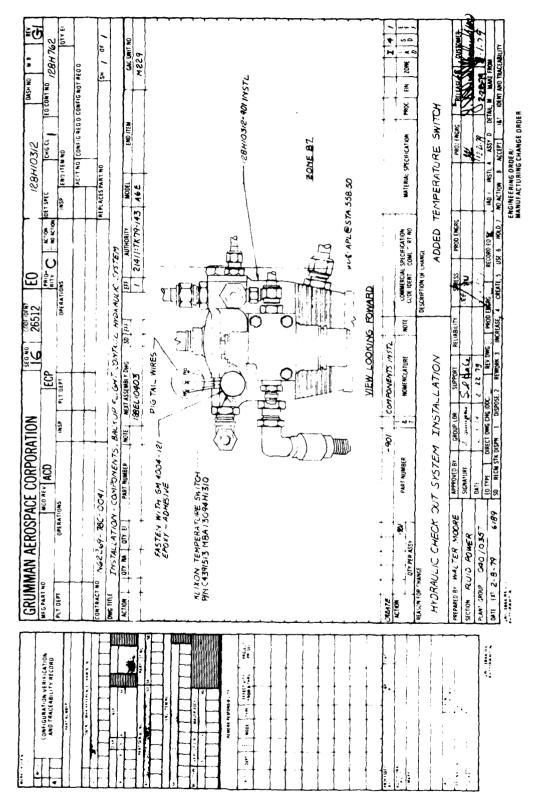


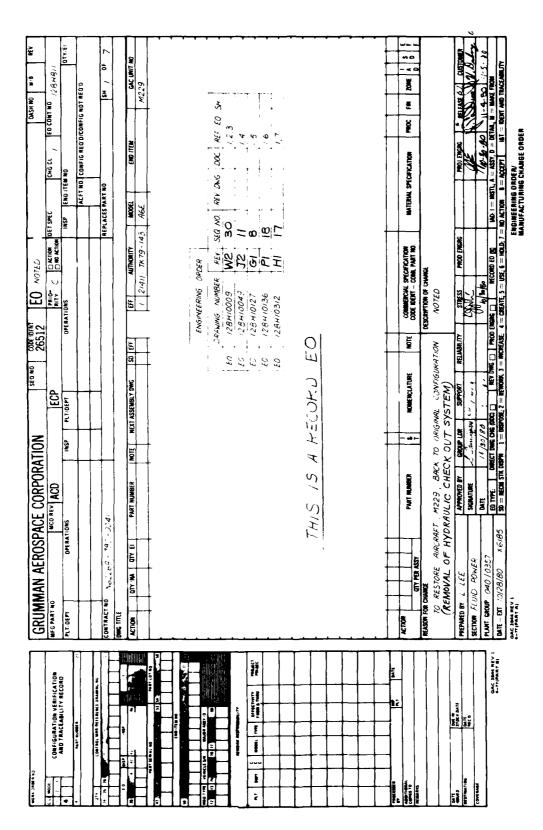


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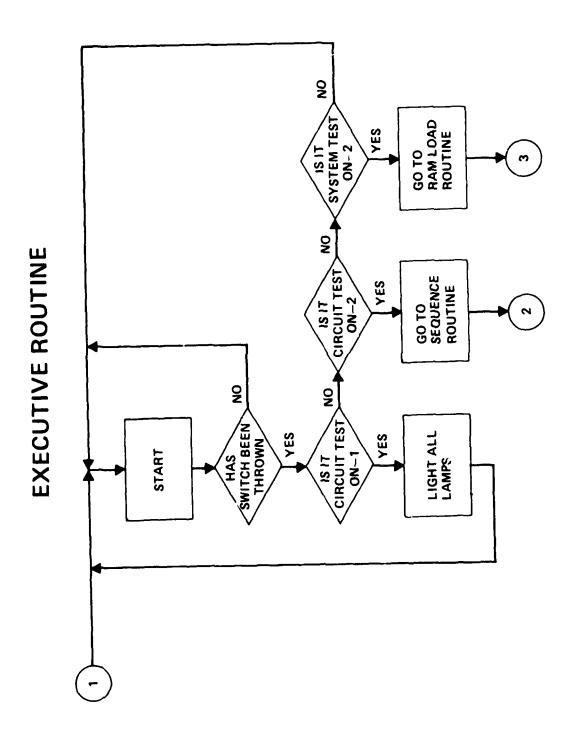
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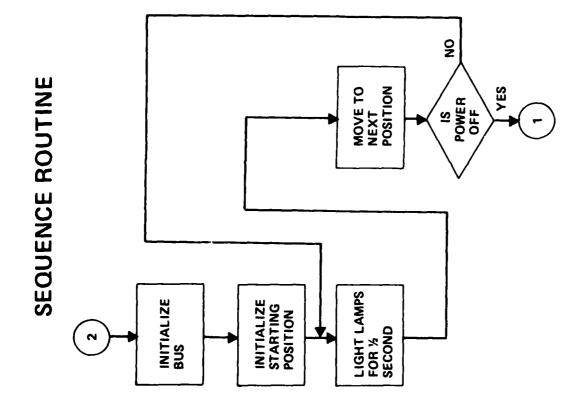
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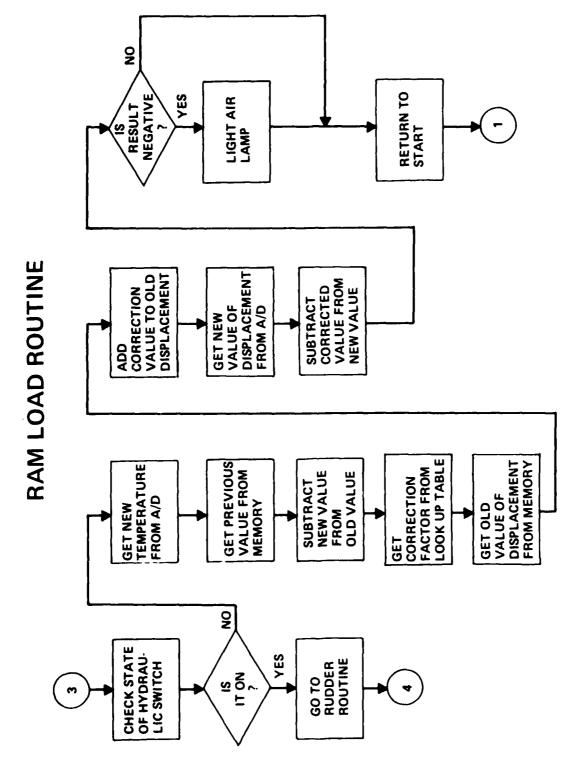
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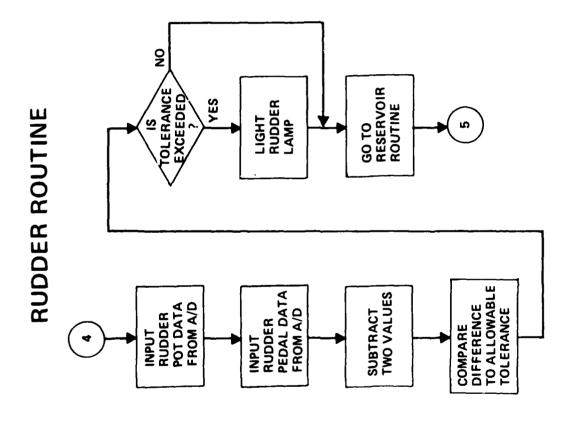
APPENDIX H HYCOS PROGRAM FLOW DIAGRAM

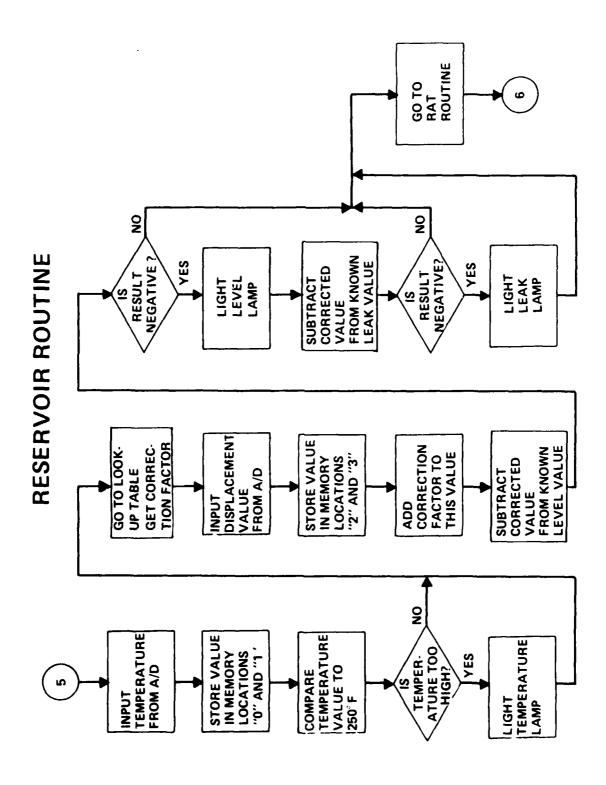


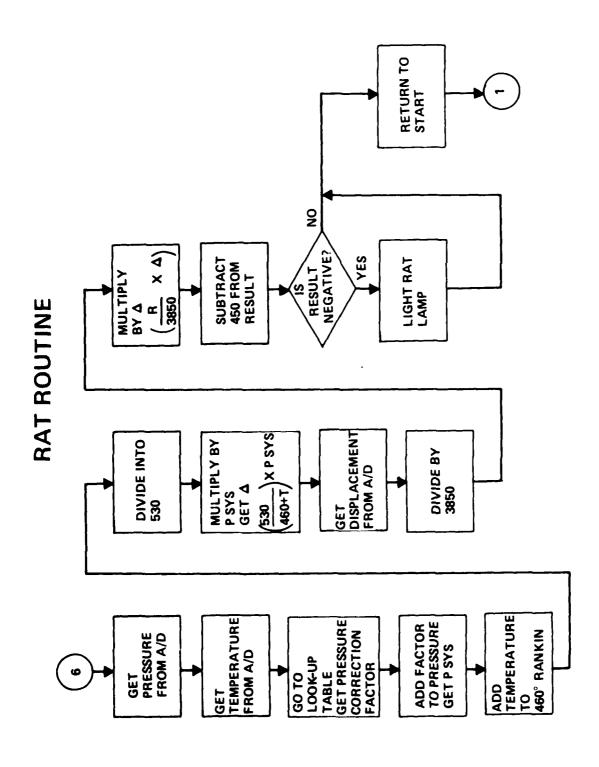




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APPENDIX I

HYCOS BATTERY ANALYSIS AND CHANGER WIRING DIAGRAM

The Hydraulic Checkout/Diagnostic Monitoring System (HYCOS) includes the following nickel-cadmium batteries:

- +5V Battery; 4 Series-connected, 1 A-H, G.E. cells (Gold Top type X GCR 1.0ST)
- +3.6V Battery; 3 Series-connected, 100 mA Hr GE cells (Gold Top type X GCR 100ST)
- -6V/-4.8V Battery; 5 Series-connected (-6.0V) cells with a 4-cell tap for -4.8V. Cells are the same as the +3.6V battery cells.

These batteries are located within the HYCOS panel (box) and are not readily accessible.

I.1 GENERAL HYCOS POWER UTILIZATION

When installed in an aircraft, HYCOS uses 115 VAC, 400 Hz ship's power (when "on") to support HYCOS functional requirements and to recharge the batteries. When ship's power is "off" or otherwise not available, HYCOS power is supplied by the batteries.

A typical checkout test will last about 1/2 to 1 minute. It is estimated that up to six of these tests could be performed over a period of up to 6 weeks where no battery charging takes place.

1.2 BATTERY DISCHARGE

I.2.1 +5V Battery

This battery (now) only supplies power during the actual test period. Loads on this battery include:

 All power to logic circuits which, based on H. Dreksler's analysis, is approximately 500 mA

- Power for a maximum of five 'grain-of-wheat' lamps/test at approximately 50 mA
 each, or 250 mA total
- Power for two fiber optic light source lamps at approximately 750 mA each, or 1500 mA total.

The total current drain on the +5 battery during the test period is approximately 2.25 A. Assuming a realistic maximum test period of one (1) minute, the energy output per test is approximately 3.75% of the nameplate capacity of the battery.

I.2.2 +3.6V Battery

This battery is used to sustain the CMOS RAM (M5101). It supplies current of between 2-200 μ A essentially all the time. Assuming a nominal current of 100μ A, the battery energy output would be approximately 2.4 mA-hr per day. At this rate the 100 mA-hr battery, if initially fully charged, could operate up to about 6 weeks without charging.

1.2.3 -6V/-4.8V Battery

This battery supplies power only during the actual test period to seven (7) 8703 A/D converters. The -6V output supplies approximately 7 x 20μ A or 140μ A, while the -4.8V output, obtained by tapping into the -6V battery, supplies 7 x 5 mA or 35 mA. Thus, the cells that form the -4.8V battery have a total current drain of 35 mA + 140μ A, or essentially 35 mA. On the basis of a one-minute test period, this -4.8V battery supplies about 0.6% of the nameplate capacity per test, while the additional cell used to obtain the -6V output supplies negligible energy/test (0.0023%/test).

On the basis of energy output requirements, each HYCOS battery would appear to be adequately sized. Even accounting for self-discharge of the batteries, which could range up to a loss of perhaps 50% capacity over a 6-week period (at normal storage temperatures of about 20°C), the batteries should have adequate capacity.

Note: The +3.6V battery, which is supplying memory-sustaining power while the other batteries are idle, should be marginally acceptable for a 6-week storage.

1.3 BATTERY CHARGING

The circuit used for battery charging is shown in Fig. I-1. Figure I-2 depicts the HYCOS Battery Charger. The recommended (by G.E.) constant current charge rate for the Gold Top batteries is between C/10 and C/20. These batteries can supposedly safely handle continuous overcharge at these rates.

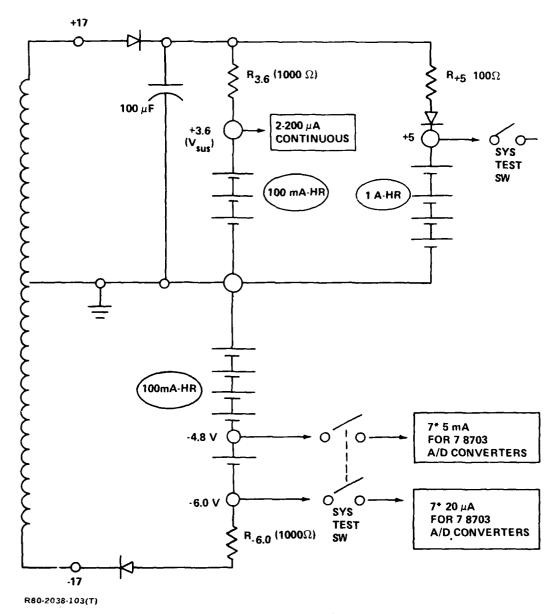


Figure I-1. Battery charging circuit.

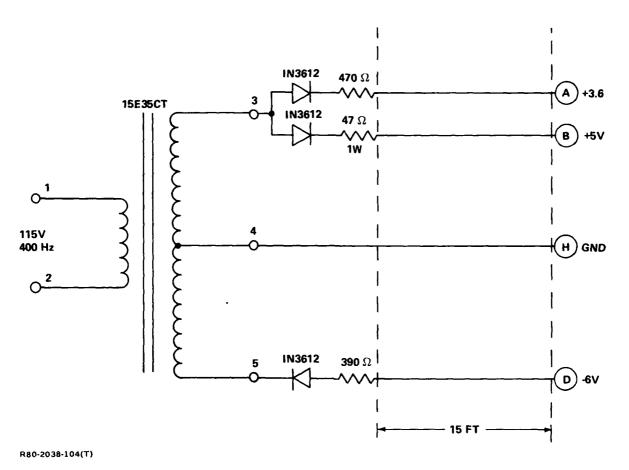


Figure I-2. HYCOS battery charger.

A fully depleted battery, in order to be fully charged at C/10, will require 14-18 hr of charge time and 30-35 hr of charge time at C/20. It is unlikely that HYCOS batteries will be provided this much time if charging is to be accomplished during aircraft flight.

Based on the questionable time available for recharge, it is recommended that the HYCOS panel be equipped with an externally accessible connector (Fig. I-3) that provides direct connection to battery + and - terminals, or connections to the input of the HYCOS battery charging circuit (i.e., 115 VAC, 400 Hz to transformer primary). The preferred approach is direct connection to the battery terminals. This connector would then allow:

- Monitoring or a status check on battery voltages
- Battery charging using a dedicated ground support charger.

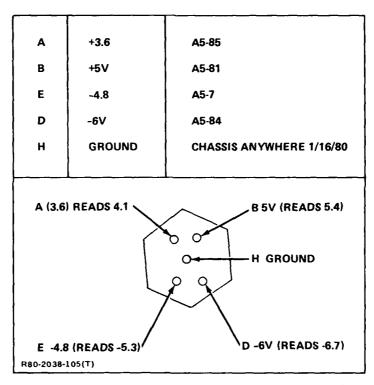


Figure I-3. Battery Test Panel Connector Interface.

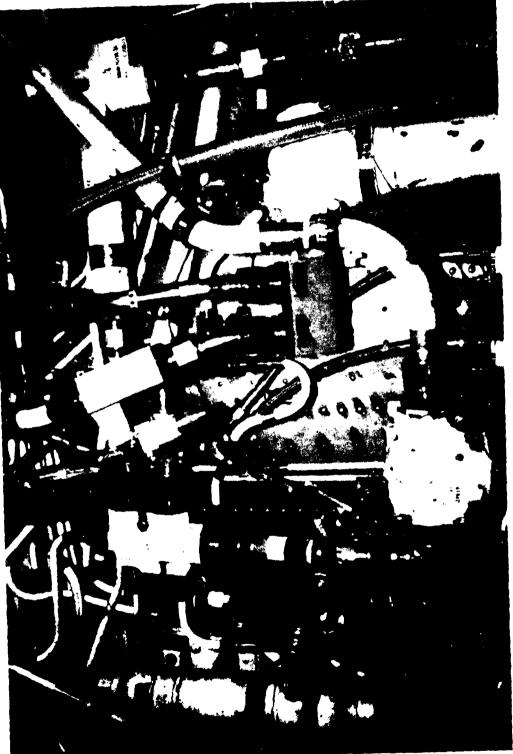
APPENDIX J SYSTEM INSTALLATION AND VEHICLE PHOTOS

рното по.	DESCRIPTION
J- 1	View showing temperature-compensated pressure switch mounted to 15 cubic inch pneumatic bottle.
J- 2	Port keel area showing quiescent flow sensor, system pressure switch, and pressure filter remote reading Delta P indicator.
J- 3	View showing temperature transducer in return line to reservoir.
J- 4	Combined system reservoir showing remote reading potentiometer and desiccant saturation detection unit.
J- 5	Port keel area showing probe-type temperature switch in pump case drain line. Also shown is system pressure switch.
J- 6	Port keel area showing probe-type temperature switch in pump case drain line. Also shown is system pressure switch. (Same as J-5.)
J- 7	Case drain filter showing APM multicator installation (provisions for fluid sampling case drain line).
J- 8	View looking forward at 30-cubic inch gear door dump bottle with temperature-compensated pressure switch on pedestal.
J- 9	View showing duct access area where HYCOS panel is to be mounted. Wire bundles are shown in area.
J-10	View showing bottom of Ram Air Turbine Accumulator with temperature and pressure transducer.
J-11	Forward port keel area showing Ram Air Turbine Accumulator with linear displacement transducer.
J-12	View showing bottom of Ram Air Turbine Accumulator with temperature and pressure transducer. (Same as J-10.)
J-13	Closeup of displacement rod on Ram Air Turbine Accumulator.
J-14	Closeup of displacement rod on Ram Air Turbine Accumulator (Same as J-13.)

PHOTO NO.	DESCRIPTION
J-15	View looking forward at RAT accumulator mounting.
J-16	Surface temperature switch mounted on flight control backup module.
J-17	Surface temperature switch mounted on flight control backup module (Same as J-16.)
J-18	Rudder actuator flow sensor on pressure line.
J-19	Rudder actuator flow sensor on pressure line. (Same as J-18.)
J-20	Pump case drain flow sensor installation.
J-21	A-6E Mod 229 flight test vehicle.
J-22	Plane Captain interrogating HYCOS system.
J-23	Closeup on HYCOS Display panel in flight test vehicle.

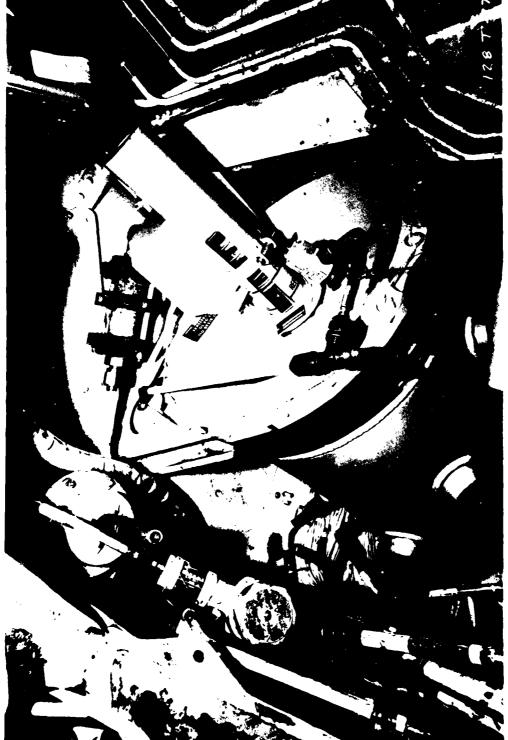


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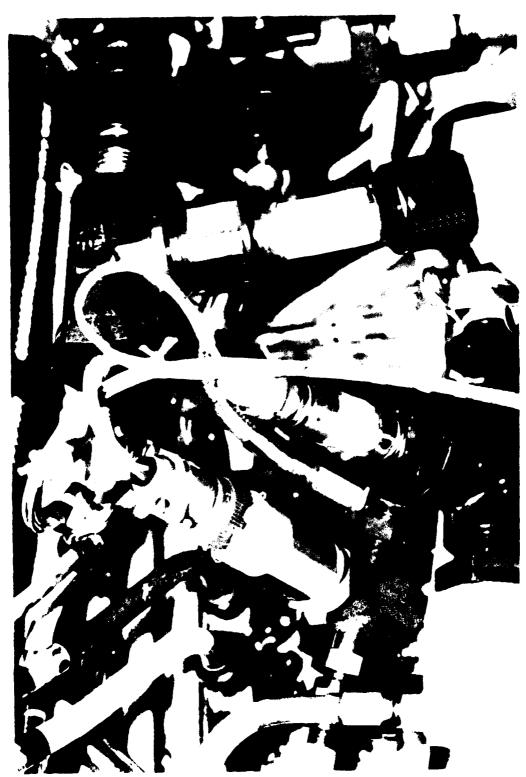
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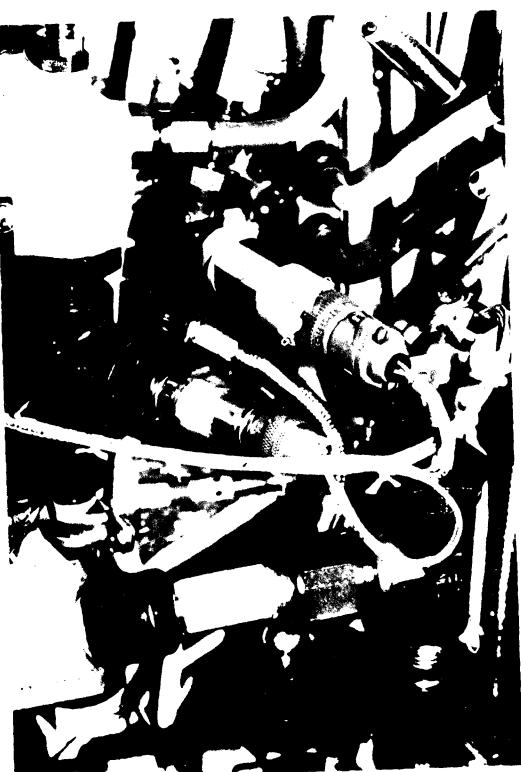


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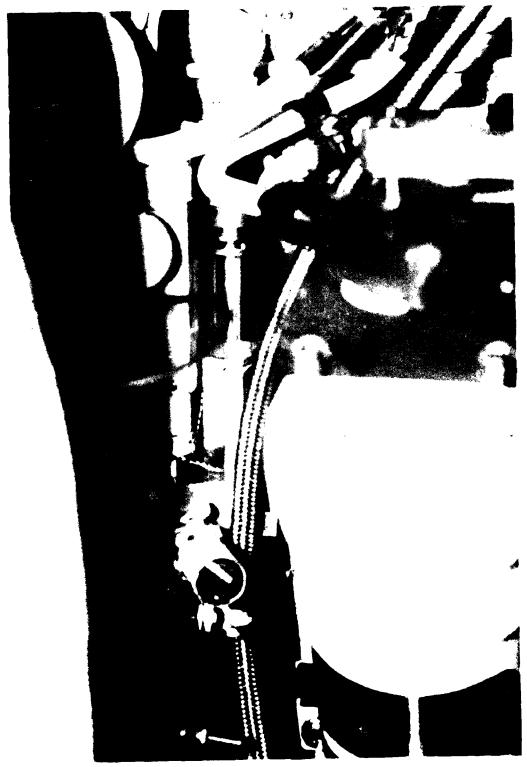
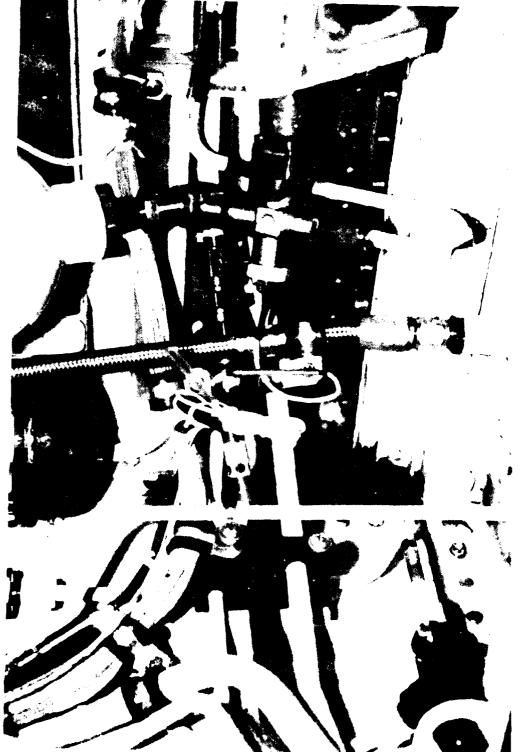


Photo J-8



.Photo J.9



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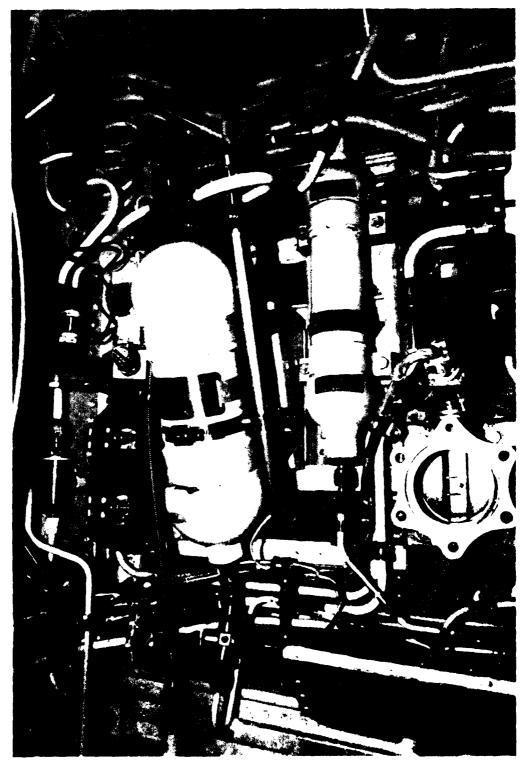
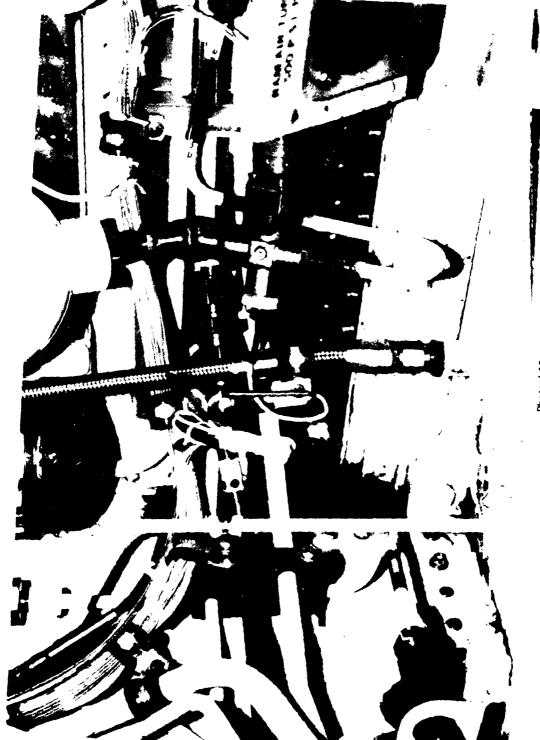


Photo J 11



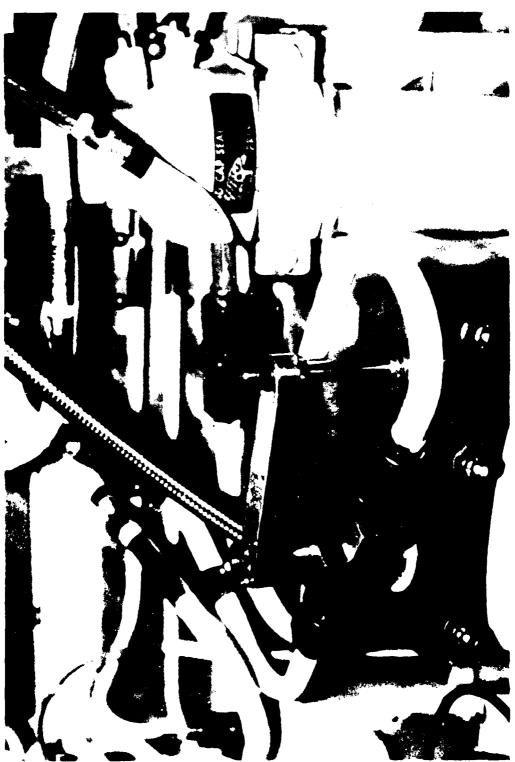


Photo J.13



Photo J-14

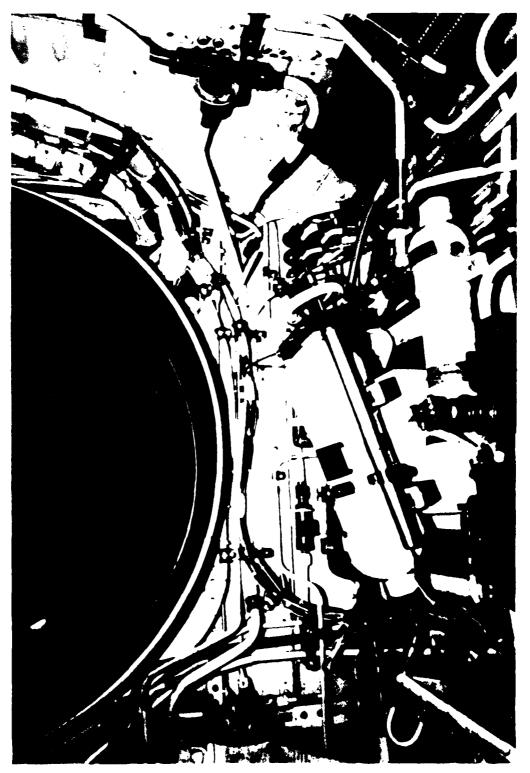
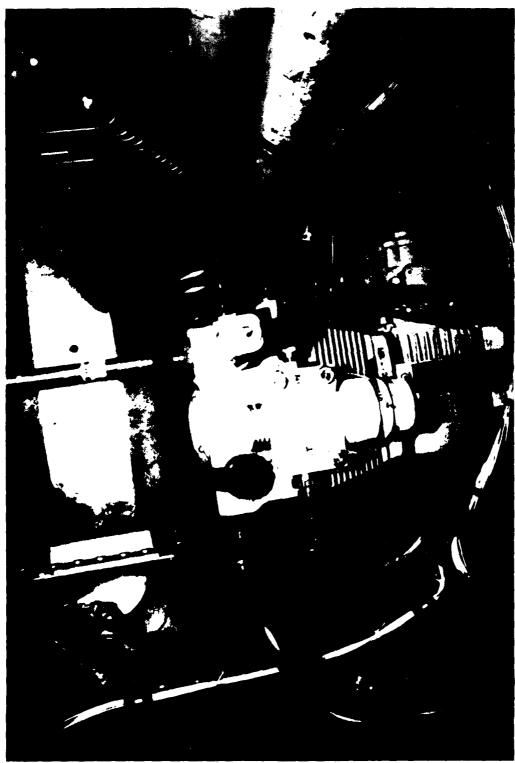


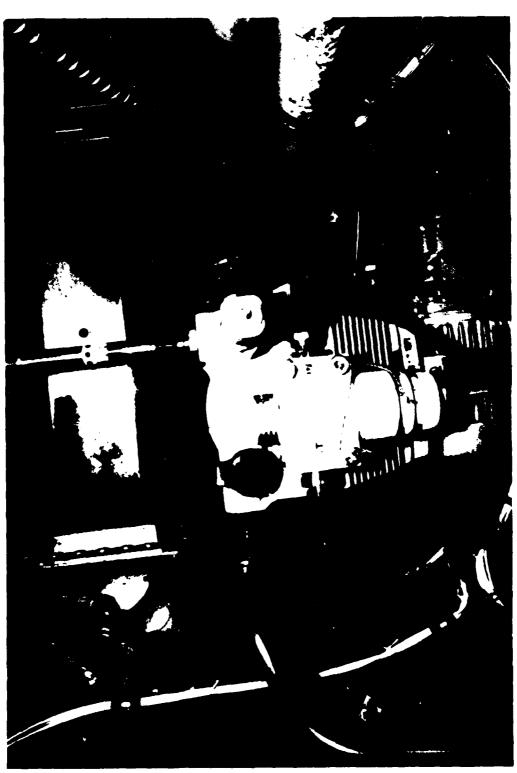
Photo J-15



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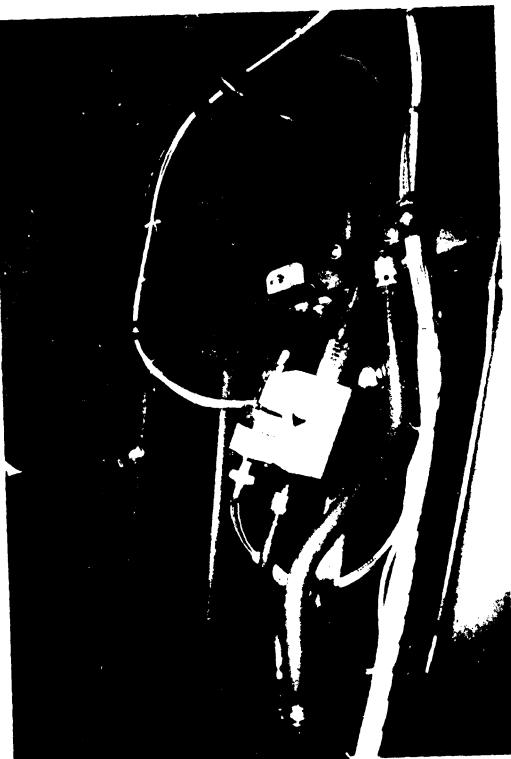
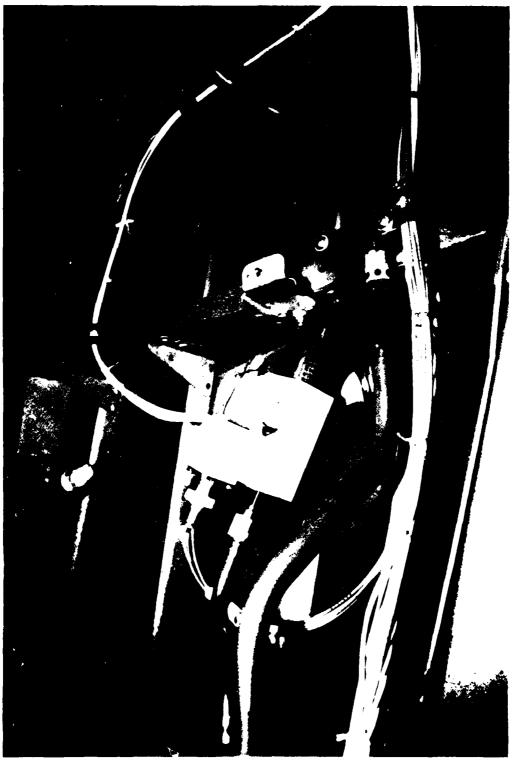


Photo J.18



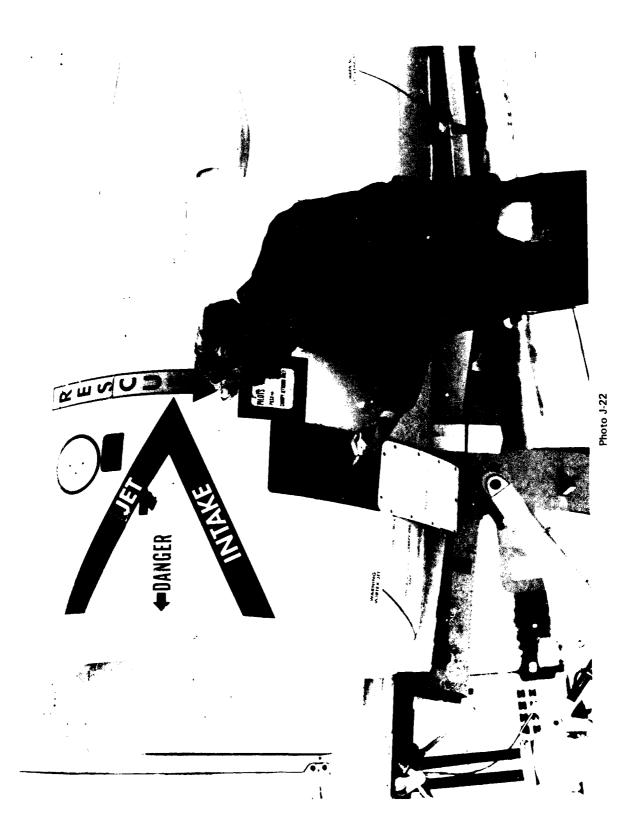
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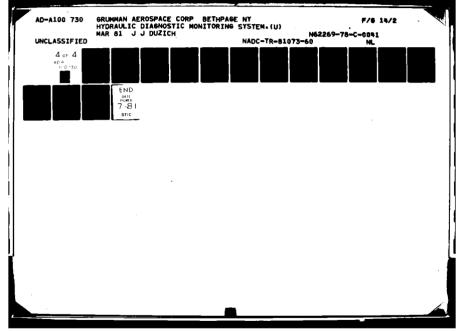
Photo J.20



Photo J.21







APPENDIX K MICROPROCESSOR PROGRAM

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0007 37 0008 39	25	OUTL PLA	; extra shot
9998 3616	26	JTØ SQNCE	; IF TO DO SEQUENCE ROUTINE
0000 5010 0000 5625	27	JT1 RMLD	; IF T1 DO AIR ROUTINE
999F 17	28	INC A	; CHECK STATE
0010 39	29	OUTL P1. A	, OF SYSTEM
0011 08	30	INS A, BUS	; TEST SHITCH
9012 3225	31	JB1 RMLD	; IF SWITCH IS ONL DO RAM LOAD
0014 0402	32	JMP START	
	33		
	34	SEQUENCE SUBROUTINE	The second secon
	3 5	THIS SUBROUTINE WIL	L LIGHT ALL THE LAMPS BY BLOCKS,
	36	FIRST THE PUMPS (5	LAMPS), THEN RESERVOIR (4 LAMPS).
	37		ON FOR 1.72 SECOND THEN SEQUENCE
	38	; TO NEXT BLOCK	
	39		
	40	MOV R, #889H	COUTPUT TO GET P27 AND TO
9916 2389	41 SQNCE	OUTL P2: R	DISABLE MEMORY FROM BUS
0018 3R	42 43	MOV R #01H	THE ST SECTION
9919 2391	44 TSTUT		
9918 82	45	MOV R2, #32H	; PRELOAD R2 FOR 1/2 SECOND TIP
0010 BA32 001E AB	45 46	MOV R3, A	FAVE POSITION OF LAMPS IN R3
001E NB	47	CALL MS10	GET 1/2 SECOND TIMING SUBROUT
001r 3436 0021 FB	48	MOV A.R3	RESTORE ACCUMULATOR
0021 FB 0022 E7	49	RL A	MOVE BIT IN ACCUM TO LEFT
0022 E1 0023 0418	5 <u>0</u>	JMP TSTUT	REPERT TEST
may y main			

PRGE 2

```
ISIS-II MCS-48/UPI-41 MACRO ASSEMBLER, V2.0
HYCOS - R6 REV 18 1/19/88
 L0C 0BJ
                  SEQ
                               SOURCE STATEMENT
                     53
                                FIF HYDRAULIC SMITCH IS AT A "0" ME GO TO THE AIR ROUTINE
                     54
                                FIF AT A "1" HE DO RESERVOIR ROUTINE
                     55
                                > (FOLLOWING THE RUDDER ROUTINE)
                     56
 0025 2392
                     57 RMLD:
                                        MOV A. 1892
                                                        FEMABLE STATE OF HYDRAULIC SHITCH
 8827 39
                     58
                                        OUTL PLA
                                                                   TO 805
 9928 98
                                                        FAND INPUT TO ACCUMULATOR
                     59
                                        INS R. BUS
 0029 1250
                     60
                                        JB8 RUDDER
                                                        ; IF R "1" DO RUDDER ROUTINE
                     61
                                F RIR ROUTINE:
                                FTHE SYSTEM IS UNPRESSURIZED , THE SYSTEM TEST SHITCH IS
                     62
                                ; UP OR DOWN. TEMPERATURE TI AND DISPLACEMENT RI ARE IN
                     63
                     64
                                : MEMORY LOCATIONS 0.4.1 AND 2.4.3 RESPECTIVELY. THE PRESENT
                     65
                                -TEMPERATURE TO IS IMPUTTED FROM THE TRANSDUCER THRU ITS A/D
                     66
                                ; CONVERTER AND CHECKED FOR OVERTENP . THEN TI IS SUBTRACTED FROM
                     67
                                FT2 TO GIVE DELTA T (2T). ZT = T2 - T1 ZT IS MULTIPLIED BY
                                CONSTANT 3.78 TO GET TEMPERATURE CORRECTION FACTOR, THE RESULT
                     68
                     69
                                $15 ADDED TO OR SUBTRACTED FROM R1 DEPENDING ON THE SIGN OF XT
                     79
                                FNEXT ADD 480 TO R1 TO ALLOW FOR A 1 INCH DISPLACEMENT AND GET
                     71
                                FR14 DISPLACEMENT R2 IS INPUTTED FROM THE RESERVOIR FOT AND ITS
                     72
                                #A/D.R1/ IS SUBTRACTED FROM R2 . IF RESULT IS POSITIVE DISPLACE-
                     73
                                THENT HAS MORE THAN I INCH AND HE LIGHT THE AIR LAMP.
                     74
                     75
                                EXPMPLE
                     76
                     77
                                RSSUME
                                                T1=135 C
                                                                T2=21 C
                     78
                                                R1=5500
                                                                R2=5600
                     79
                                        AIR=R2 - (R1 + 400 + (T2 - T1) X 3,78)
                     89
                     81
                     82
                                        R1 + 499 + (T2 - T1) \times 3.78 = R1'
                     83
                     84
                                        T2 - T1 = 21 - 135 = -114
                     85
                     86
                                        -114 X 3. 78 = -430
                     87
                                        RIR = 5600 - ( 5500 +400 - 430 )
                     88
                     89
                                            = 5600 - 5470
                     90
                                            = + 130
                     91
                     92
                                : ANSHER IS POSITIVE SO AIR LAMP LIGHTS
                     93
                                START WITH EQUATION ( T2-T1 ) X 3 78
                     95
 0028 348A
                                        CALL TMPCK
                                                        GET TO FROM TEMP AND CONVERTER
                     96
                                                        FINPUT TO ACCUM AND R2
                     97
                                                        FCHECK FOR OVERTEMP
 0020 27
                     98
                                        CLR A
                                                        , INITIAL CONDITION
 002E AD
                    99
                                        MOV R5/A
                    100
                                                        *R5 SETS UP MEMORY ACCRESS
 002F BE30
                    101
                                        MOV R6, #38H
                    102
                                                        -R6 OUTPUT USED FOR READ
 0031 39
                    103
                                        OUTL PLA
                                                        - CLEAR PORT 1 FROM BUS
 9932 3450
                    184
                                        CALL LSD
                                                        GET TI FROM MEMORY
 9934 3483
                    105
                                                        /M = 12 - 11
                                        CALL SETCT
 8936 9991
                    186
                                        MOV $1,#01H
                                                        - SETTING UP SIGN OF SUBTRACTION
```

JFO NEG1

- IF NEGATIVE PEG 1 = 1

9938 B63B

107

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HYCOS - A6 REV 18 1/19/80

LOC	08J	SEQ	SOURCE STATEMENT	
003A	63	108	DEC R1	ELSE REG 1 = 0
4	543R	189 NEG1	CALL LKUP1	; ELSE REG 1 = 0 , GET BINNRY VALUE FOR %T X 3, 78
4030	04311	110	; BINARY RESULT STORED I	N REGISTER 4 RESISTOR R1 IS IN MEMORY
		111		400 (= 66H) AND 2T VALUE
993 0	3450	112	CALL LSD	GET RI FROM MEMORY
003F	9398	113	ADD A, #88H	R1 + 424 (COULD NOT GET 400 EXPCT)
0041	29	114	XCH AJR1	EXCHANGE SUM WITH SIGN OF AT
9942	53FF	115	anl rubseth	AND TO SEE IF 0
0044	C64C	116	JZ P051	; IF 0 IT WAS POSITIVE
	_	117	MON 2 DA	ELSE NEGATIVE
004 6	-	118	MOV A, R4	GET XT Gones Complement
0047		119	CPL A INC A	; 21S COMPLEMENT
	17	120	ADD AJR1	;SUM ~ XT
	69	121 122	JMP SUM1	SUBTRACTION COMPLETE
994C	944E	123 P051:		GET 2T
	69	124	ADD A, R1	SUM + XT
	AR	125 SUM1:		R1' INTO REG 2
	2320	126	MOV AJ #219H	; R2 R/D
	3489	127	CALL GONOGO	; INTO ACCUM
0053		128	XCH A.R2	; SMAP R2 AND R17
	3463	129	CALL SBTCT	;R2 = R11
8956	8682	139	JFØ START	; IF NEGATIVE NO ERROR
		131		REPEAT WHOLE OPERATION
0058	3 23 9 7	132	MOV R, #97H	ELSE LIGHT
985i	39	1 33		AIR LAMP
0056	8 0402	134	JHP START	REPERT WHOLE OPERATION
		135		
		136	; RUDDER CIRCUITRY	
		137 138	; TAKE ANALOG OUTPUTS 0	NE 2 POTS 1970 COMMERT.
		139	SURTRACT FROM FACH OF	HER, THEN SUBTRACT DIFFERENCE
		140	FROM A GIVEN TOLERANO	
		141	TOO HIGH LIGHT RUDDER	
		142	, , , , , , , , , , , , , , , , , , , ,	
865	D 2318	143 RUDDE	R: MOV A, #18H	RUDDER POT DATA
	F 34R9	144	CALL GONOGO	, FROM RZD
996	1.88	145	MOV R2, A	; PUT_INTO_R2
996	2 2338	146	MOV A, #38H	; RUDDER PEDAL DATA
996	4 34R9	147	CALL GONOGO	; FROM A/D
	€ 3483	148		R2-R=DELTA
	8 23F4	149	MOV R, #0F4H	; 2'S COMPLEMENT OF 12 ; Subtract 12 from Delta
	A 6A	150	ADD AJR2 JNC RSRVR	; IF NO CARRY RUDDERS OK
•••	B E679	151	JHC KSKYK MOV AJ #95H	CALL RUDDER LAMP
	10 23 0 5 1F 39	152 153	OUTL P1, A	AND LITE IT
900	F 37	154	0012 12/11	711790 6.21
		155		
		156		
		157		
		158	RESERVOIR ROUTINE	
		159		T THE FOLLOWING CONSTANTS ARE USED
		160	, EACH BIT IS 53 OHMS	6799/127
		161	SLOPE FOR NORMAL DIS	PLACEMENT IS 1 85 OHMS (DEGREE F =
		162	(2.23 OHMS / DEGREE C	: ≈ 16 DEG C / BIT

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ISIS-II MCS-48/UPI-41 MACRO ASSEMBLER, V2.0
                                                         PAGE
HYCOS - R6 REY 18 1/19/80
 L00 08J
                   SEQ
                               SOURCE STATEMENT
                                35420 OHMS RT -54 C =LEVEL MINIMUM
                    163
                    164
                                ;5070 OHMS AT -54 C =LERK MINIMUM
                    165
                                FTEMPERATURE TRANSDUCER READS IN DEG C AND IS SET SO THAT
                                3-54C IS EQUAL TO 0. EQUATIONS ARE
                    166
                    167
                                (LEVEL = 5420 + 3.33 X XT - R (IF POSITIVE HE LIGHT LAMP)
                    168
                    169
                                FLERK = 5070 + 3.33 X ZT - R (IF POSITIVE WE LIGHT LAMP)
                    170
                    171 RSRVR:
                                                                 FINITIAL ADDRESS OF MEMORY
  0070 BD00
                    172
                                        MOV R5, 10H
  0072 BE10
                    173
                                        MOV R6, $18H
                                                                 : INITIAL CONDITION
  0074 3488
                    174
                                        CALL THPCK
                                                                 FOR TEMPERATURE - CHECK FOR
                    175
                                                                 -OVERTENPERATURE STORE IN R2 & A
                                        CALL BYTST
  0076 3447
                    176
                                                                 PUT IN HEMORY LOCATIONS 101 & 111
  9978 F8
                    177
                                        MOV PLRO
                                                                 FITEMP BACK TO ACCUM
  9979 5459
                    178
                                        CRLL LKUP2
                                                                 FIGET BINNRY EQUIVALENT OF TEMP
                    179
                                                                 #AND STORE IN R4
  8978 2329
                    180
                                        MOV A. #020H
                                                                 ; DISPLACEMENT VALUE
  997D 34R9
                    181
                                        CALL GONOGO
                                                                 FINTO ACCUM
                    182
  997F BD92
                                        MOV R5, #62H
                                                                 , INITIAL CONDITIONS
  9981 AA
                    183
                                        MOV R2 R
                                                                 ESTORE DISPLACEMENT IN R2
  0082 3447
                    184
                                        CALL BYTST
                                                                 : PUT DISPLACEMENT IN HEHORY
                                                                :LOCATIONS "2" & "3"
                    185
  0084 FC
                                        MOV RUR4
                    186
                                                                 GET 2 T
  0085 34B3
                    187
                                        CALL SBTCT
                                                                 DISPLACEMENT - 2T = 2R
  9987 RC
                    188
                                        MOV R4, A
                                                                 STORE 2 R IN R4
  888 BR66
                    189
                                        MOV R2, $66H
                                                                 35429 OHMS
                    190
  000A 34B3
                                        CALL SBTCT
                                                                 ;5420 - % R
  8698 8698
                    191
                                        JFØ RAT
                                                                ; IF F0 %R > 5420
  008E 2303
                    192
                                        MOV AL #03H
                                                                FELSE LIGHT RESERVOIR
  0090 39
                    193
                                        OUTL PLA
                                                                       LEVEL LAMP
  0091 BR60
                    194
                                        MOV R2, #968H
                                                                 ;5979 OHMS
  0093 FC
                    195
                                        MOV R, R4
                                                                 GET % R
  0094 3483
                    196
                                        CALL SBTCT
                                                                 ;5979 - XR
  8896 B698
                    197
                                        JF0 RAT
                                                                JIF F0 XR > 5070
  9998 2389
                    198
                                        MOV A, $688H
                                                                 JELSE LIGHT RESERVOIR
  009R 39
                    199
                                        OUTL P1, A
                                                                       LEAK LAMP
                    200
                    201
                                FRAT ROUTINE
                    202
                                THIS ROUTINE SOLVES THE EQUATION
                    203
                    294
                                 ; PPR = (R/3850) X (530/(T + 460)) X PSYS
                    205
                    206
                                ; PSYS = PRESSURE READING + TEMPERATURE CORRECTION FACTOR
                    207
                                FR = RESISTANCE IN OHMS
                    208
                                ; 3850 = RESISTANCE AT STP
                    209
                                ;530 = 70 DEGREES F + 460 TO MAKE DEGREES RANKIN
                    210
                                ;T = MEASURED TEMPERATURE IN DEGREES F
                    211
                                FIRST HE SOLVE FOR PSYS, AND STORE RESULT IN HEMORY, THEN HE
                    212
                    213
                                ; PERFORM 2 DIVISIONS, THEN 2 MULTIPLICATIONS. HE THEN SUBTRACT
                                :450 PSI FROM THE RESULT TO TEST IF OUR PRECHARGE PRESSURE IS ADEQUATE
                    214
                    215
                                FOR THE SYSTEM . IF NOT HE LIGHT THE RAT LAMP.
                    216
                    217
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	-48/UPI-41 MACR) AS REY 18 1/19/29	SEMBLER, V2.0	PRGE 5
L0C 08J	SEQ	Source Statement	
	218		
009B 3400	219 220 RAT:	CALL PRSCLC	SOLVE FOR PSYS
9990 2385	221	MOV A, #85H	PUT 400 INTO ACCUM
909F 6E	222	ADD R, R6	ADD TO GET RANKIN
9999 E684	223	JNC NOCA	: IF NO CARRY NO OVERFLON
99A2 23FF	224	MOV A MOFFIH	ELSE PUT FF INTO CARRY
0004 BAB1	225 NOCA:	MOV R2 #981H	PUT 530 R IN R2
00A6 8821	226	MOV R8, #21H	FINITIALIZE TO ADDRESS 33
99R8 5499	227	CALL DIVIDE	; PERFORM 530/(T+460)
	228		; STORE T IN 34 & 35
00AA 2328	229	HOY A, #28H	GET DISPLACEMENT FROM
00AC 34A9		CALL GONOGO	A./D CONVERTER
OORE AA	231	HOV R2, A	AND PUT IN R2
00NF 2378		MOV A. #78H	PUT 3850 INTO ACCUM
0081 5400	233	CALL DIVIDE	PERFORM R/3850
2002-02	234	~ ^ ^	STORE IN 36 & 37
0083 27 0084 AC	23 5 236	CLR A MOV R4, A	; MANT 0 IN ; R4 AND
6665 AD	237	MOV R5, A	7.85 mm2 2.85
9986 B829	·-	MOV R9, #29H	ADDRESS 32
0088 F0	239	MOV ALERS	HSBYTE OF PRESSURE
9689 AE	240	MOV R6 A	; TO 86
000A 18	241	INC RO	ADDRESS 33
9988 F0	242	MOV A BRO	LSBYTE OF PRESSURE
99BC AF	243	MOV R7, A	, TO R7
9980 18	244	TNC R0	: ADDRESS 34
008E F0	245	MOV AJ ERØ	MSBYTE OF TEMP
99BF C6C5	246	JZ NOMLT	FIF 0 NO MULTIPLY
99C1 FE	247	MOV A, R6	MSBYTE OF PRESS
88C2 AC	248	MOV R4, A	: T0 R4
00C3 FF	249	MOV AJR7	LSBYTE OF PRESSURE
99C4 RD	250	MOV R5, A	TO R5
00U5 18 00U6 F0	251 NOMLT 252	: INC R8 MOV A, er8	ADDRESS 35 ALSBYTE OF TEMP
9907 5466		CALL QUADM	MULTIPLY TEMP & PRES
00C9 18	254	INC RO	ADDRESS 36
99CA F0	255	MOV A, eRO	MSBYTE
99CB C6D6		JZ NMLT1	; IF 8 CONTINUE
99CD FE	257	MOV ALRE	: MSBYTE TO A
89CE 8464	258	JMP NMLT2	; NO MULTIPLY
0000 1 8	259 NMLT1	: INC RO	ADDRESS 37
9901 F9	269	MOV A. ero	LSBYTE OF DISPLACEMENT
0002 5466		CALL QUADA	HULT PREV RESULT
9904 53FF			
8806 96E4		JNZ END2	GREATER THAN 512
9908 FF	264	MOV AJR7	LSBYTE OF PPR
0009 AA 000A 2386	265 5 266	110V R2+A 110V R, 1100-5H	, PUT IN R2 ; PUT 480 INTO A
990C 34B3		CALL SBTCT	REMAINDER - 400
986E 95	. 267 268	OPL F8	- ALIBITINGES = 100
000E 95		JF0 ENC2	JF CARRY REMD400
99E1 2394		110v R, 984H	ADDRESS PAT LAMP
00E3 39	271	OUTL P1, A	TURN IT ON
00E4 0482		JMP STAPT	REPERT

.00 08 3	SEQ	SOURCE STATEMENT	
	273	200 24204	
100	274	ORG 0100H	
	275 276	PRESSURE CALCULATION	TO THE DOCUME PROBLEM THE MELTINES
	276 277		es the pressure reading in My-Takes 3 Ados or Subtracts a temperature
	277 278		TIAL SLOPE READING MULTIPLIES THE NEW
	279 279		ing and ados an initial offset, the HSB
	299	; IS STORED IN R5, AND 1	
	281	POSITIVE TEMPERATURE	ine esome in RS
	282	PRESSURE = (21 + (3T)	')¥9 911) ¥ MV + 27
	283	NEGATIVE TEMPERATURE	7/10. 011/ N (IF) 25
	284	PRESSURE = (21 - (31)	1)X0 017) X MV + 23
	285) (C250000 (C25 (3)	7/10. 0217 1/11/11 23
0100 2330	286 PRSCLC	: MOV RJ #38H	GET PRESSURE DATA FROM
0182 34R9	287	CALL GONOGO	R/D CONVERTER
9194 A8	288	MOV RO, A	; SAVE VALUE
9165 BAGA	289	MOV R2, WORH	, 429 PSI
9107 34B3	290	CALL SBTCT	; 429 - P
9109 B60D	291	JFO ENE4	FIF CARRY P < 429
910B 94E1	292	JMP END3	:LIGHT LAMP
91 9 0 F8	293 END4:	MOV AJRO	GET VALUE BACK
91.9E AF	294	MOV R7, A	; STORE
010F 2310	295	MOV A. #10H	GET TEMPERATURE DATA FROM
0111 34R9	296	Call. Gonogo	; A/D CONVERTER
0113 AE	29 7	MOV R6, A	; STORE
0114 AA	298	MOV R2 A	; * ALSO IN R2
0115 232B	299	MOV A, #28H	GET 70 F IN ACCUM
011 7 3483	300	CALL SBTCT	;T-70 = T'
0119 77	301	RR A	i
011A 77	382	rir A	;
011B 77	303	RR A	<i>i</i>
011C 77	394	RR A	DIVIDE BY 16
011D 530F	385	ANL A, NOFH	; 4 SHIFTS SHOULD BE 0
011F B629	386	JF0 NTMPTR	; IF NEGATIVE TEMPERATURE
0121 77	397	RR A	ELSE DIVIDE BY 32
9122 5397	388	ANL A 407H	;5 SHIFTS SHOULD BE 0
0124 0316	389	ADD A #16H	ADD 22 TO DELTA
8126 AD	310	MOV R5, A	SAVE IN R5
0127 242E	311	JHP HVHPLY	GO TO MULTIPLY
0129 BA16	312 NTMPTR		GET 22
0128 3483	313	CALL SBTCT	; 22 MINUS DELTA
012D AD 012E FF	314	MOV R5, A	SAVE IN R5
OLZE PP OLZF AA	315 HVMPLY		GET MILLI VOLTS
0130 FD	316 317	MOV R2, R	; AND PUT IN R2 ; GET DELTA
0130 PD 0131 R9	318	MOV ALR5 MOV R1. A	AND PUT IN RA
0132 34BE	319	CALL BMPY	HULTIPLY
0134 8820	32 9	MOV R9, #29H	FROORESS #32
0134 B020	32 6 32 1	MOV ERO, A	MSBYTE IN 32
0137 18	322	INC R8	ADDRESS #33
0138 F9	323	NOV A. R1	GET LSBYTE
0139 AB	324	MOY BRO, A	STORE IN 33
9139 83	325	RET	
	326	<u>-</u> -	

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MYCOS - A6 REV 18 1/19/80

F0C 081	SEQ.	SOURCE STATEMENT	
	328	; 10 MILLISECOND SUBROL	ITINE
	329	THIS SUBROUTINE USES	THE 8748 BUILT IN TIMER THE
	339	T COUNTER IS LOADED T	TO 88HCH .
	331	THIS GIVES A 10 MILLI	SECOND COUNTDOWN EACH TIME HE
	332		CREMENT A COUNT IN R2 SO THAT
	333	HE CAN GET MULTIPLES	OF 10 MILLISECONDS.
	334		
01.38 2380	335 MS10:	MOV A. #89H	
01 30 62	336	MOV T.A	FLOAD HAX COUNT IN THALL 1975
013E 55	337	STRT T	; START COUNTDOWN
013F 1643	338 CONT:	JTF DECR	FLOOP FOR 10 MILLISECONDS
0141 243F	339	JMP CONT	, * * * *
914 3 65	340 DECR:		STOP COUNTER
0144 EA3B	341	DJNZ R2 HS10	;LOOP TILL R2 = 0
0146 8 3	342	RET	
	343		
	344		
	345		
	346	BYTE STORE SUBROUTINE	
	347		THE FIRST 4 BITS INTO THE NEXT RAM
	348	; Address , then the se	COND 4 BITS INTO THE NEXT RAM ADDRESS.
	349		
0147 A8	350 BYTST:		STORE VALUE IN RO
0148 344F	351	CALL MRITE	HRITE LSD INTO MEMORY
014R F8	352	MOV A. RO	GET HORD BACK INTO ACCUMULATOR
914B 47	353	SMAP A	PUT MSD INTO LSD POSITION
014C 344F	354	CALL WRITE	; WRITE MSD INTO MEMORY
014E 83	355 356	RET	
	356 357		
	357 358	HRITE SUBROUTINE	
	359		FIRST PUT DATA ON BUS WITH CE1 500.
	369		ADDRESS WITH ONLY OD HIGH THEN ADDRESS
	361		N OFF MEMORY, R6 HRS 18H STORED R3 AN
	362	INITIAL CONDITION	TOTAL TELEVISION TOTAL STORES TO THE
014F 02	363 WRITE		OUTPUT DATA ON BUS
9159 FD	364	MOV A, R5	PUT INTO ACCUM
0151 4E	365	ORL A. R6	PUT A 1 IN FRONT OF ADDRESS
0152 3A	366	OUTL P2, A	OUTPUT TO MEMORY
0153 4350	367	ORL A. #50H	TURN ON HRITE
0155 3A	368	OUTL P2, A	RND OUTPUT TO HEMORY
0156 531F	369	ANL R #1FH	PUT 1 IN FRONT OF ADDRESS
9158 3A	370	OUTL P2, A	OUTPUT TO MEMORY
0159 80	371	MOVX AJ GRO	; PUT BUS IN TRI STATE
015A 1D	372	INC R5	GET NEXT RODRESS
0158 83	373	RET	
	374		
	375	; LSD_SUBROUTINE	
	376	THIS SUBROUTINE GOES	TO MEMORY AND FETCHES A NIBBLE AND
	377		rs the second nibble combines then
	378	FAND HE GET THE MHOLE	BYTE
3484	379	***	
015C 3464	380 LSD	CALL READ	OET LSD
915E 47	381 300	SMAP A	PUT LSD IN LSD POSITION
015F A8	382	MOV RO, A	-STORE IN RO

ISIS-II MCS-48/UPI HYCOS - 86 REV 18		EMBLER: V2.0	PAGE 8
F0C 0B1	SE9	Source Statement	
0160 3464	383	CALL READ	GET MSD
9162 48	384	ORL AJRO	PUT BYTE TOGETHER
01 63 83	385	RET	
	386		
	387	; READ SUBROUTINE	
	388 389	; read data out of ram. 1	NITIAL CONDITIONS R5=88 1, R6=38
0164 80	390 READ	MOVX AJ ERO	FDISABLE BUS
8165 27	391	CLR A	; ZERO ACCUM
0166 39	392	OUTL P1.A	CLEAR BUS
01 67 FD	393	MOV PLR5	; PUT INTO ACCUM
0168 4E	394	ORL R-R6	PUT A 3 IN FRONT OF ADDRESS
0169 3A	395	OUTL P2, A	AND OUTPUT TO RAM
016A 532F	396	anl fl #2fh	FENABLE READ
016C 4340	397	ORL PJ #40H	∍60 IN FRONT OF ADDRESS
016E 3A	398	OUTL P2, A	; * ·
016F 08	399	ins a bus	GET HORD FROM RAM
9179 98	488	INS A BUS	3 TMICE
0171 53F0	401	ANL A NOFOH	; MASK OUT LSD
01,73 AF	482	MOV R7/A	STORE IN R7
0174 FD	403	MOV AJR5	GET ADDRESS BACK
01.75 4E	494	ORL AJ R6	PUT 7 IN FRONT OF ADDRESS
0176 533F	485	anl a useh	3 IN FRONT OF ADDRESS
01.78 3A	486	OUTL P2, A	TURN OFF HENORY
0179 FF	407	MOV PLR?	PUT WORD BACK IN ACCUM
0179 1D	488	INC R5	GET NEXT RODRESS
61.78 83	489	RET	
	418	. MA TIOLU CIRROUTINE	
	411	HULTIPLY SUBROUTINE	IN OCCUM FROM TA IN DO TOUTE THE
	412 413		IN ACCUM FROM T1 IN R2 TAKES THE IES IT BY CONSTANT (SLOPE) TO GET
	414	DELTA RESISTANCE CON	
	415		HNULTIPLY BY 2 AND ADD 1
	416	TING PITTE DI C IIE	THOUTHER DY 2 THO THU 1
	417		
61 7C 34B3	418 MLTPLY:		; T1-T9=T'
917E B903	419	NOV RL #03H	NEED 3 SHIFTS
0180 97	428 MULT:	CLR C	SET CARRY = 0
9181 67	421	RRC A	DIVIDE BY 2
0182 E986	422	DJNZ R1, HULT	DIVIDE 3 TIMES
9184 R9	423	MOV RLA	STORE RESULT IN R1
0185 97	424 425	CLRC	SET CHRRY = 0
0186 F7 0187 69	425 426	RLC A ADD A, R1	; MULTIPLY BY 2 ; AND ADD 1
9188 A9	427	MOV R1/A	STORE IN R1
6189 83	428	RET) DIONE IN KI
0107 03	429	NE I	
	438	; TMPCK SUBROUTINE	
	431		FROM A/D (FOR RESERVOIR AND AIR
	432		IF IT IS ABOVE 250F (= 1210). IF
	433	IT IS TOO HIGH HE LIGH	
	434		-
918A 2388	435 TMPCK	MOV A, 1198H	CALL T1 A/D CONVERTER
918C 34R9	436	CALL GONOGO	GET T1 DATA
018E AA	437	MOV R2-R	JURNT T1 IN R2

1515-11 MCS-48/1 HVC05 - R6 REV :	JP1-41 MACRO RSSEM 18 1/19/80	BLER V2.0	PAGE 9
£00 0BJ	SEQ SO	URCE STATEMENT	
018F AB	438	MOV R3, A	; SRVE IN R3
0190 2368	439	MOV AL #68H	;68 = 1210 =250F INTO ACCUM
0192 3483	440	CALL SBTCT	; 121-T1
8194 B699	441	JF0 EXCH	; IF CARRY T1<250F
0196 2340	442	HOV A. #40H	ELSE ENABLE TEMP LAMP
9198 39	443	OUTL P1, A	LIGHT IT
0199 28	444 EXCH:	XCH ALR3	GET T1 FROM R3
019A 2A	445	XCH R. R2	FPUT IT IN R2
9198 83	446	RET	
	447		
	448		
	449 ;	RESISTOR SUBROUTINE	
	450 ;	FINDS CALCULATED VALU	IE OF RESISTANCE AND SUBTRACTS IT FROM
	451 ; 452	actual value	
919C B6A2	453 RSTR:	JF0 SBRTN	; IF F0 IS SET WE HAVE TO SUBTRACT
019E 6R	454	ADD A, R2	, else hie add
919F RA	455	MOV R2, A	; STORE IN R2
01A0 24A4	456	JMP FINI	ADDITION COMPLETE
01A2 34B3	457 SBRTN:	CALL SBTCT	STEP 1 ABOVE
01A4 2320	458 FINI:	MOV RJ #20H	GET ACTUAL R FROM A/D
01A6 34A9	459	CALL GONOGO	HAND PUT IN ACCUM
01A8 83	460	RET	
	461		
	462		
	46 3		
	464		
		GONOGO SUBROUTINE	
			ES THE SELECTED A/D CONVERTER
			US. THE DATA VALID OUTPUT OF THE A/D
		IS CHECKED AND DATA I	IS HOUSPIED IF INDE
A4.00 20	469	01T1 D4 0	CELECT A M. COMMENTEDS
01A9 39	479 GONOGO:	· · · · · · · · · · · · · · · · · · ·	
91AA 98	471 NOK:	INS ALBUS	; INPUT DATA FROM BUS
01AB 08 01AC F280	472 473	INS A. BUS	; TWICE ; CHECK BIT 7 DATA VALID BIT
81AE 24AA	473 474	JB7 OK JMP NOK	FIF NOT VALID GET NEW DATA
01B0 537F	475 OK:	ANL R. #7FH	
91B2 83	476	RET	ספרו ויטע ארוווי אני ו
0105 02	477	NL I	
		SUBTRACT SUBROUTINE	
			ACCUMULATOR FROM NUMBER IN REGISTER R2
			T IN R2. FLAG FO IS "O" FOR POSITIVE
		RESULTS AND "1" FOR	
	482		
91B3 85	483 SBTCT:	CLR F0	SET FLAG FO TO 0
01B4 37	484	CPL A	COMPLEMENT ACCUM
01B5 6A	485	ROD A, R2	AND ADD TO R2
01B6 F6BB	486	JC PLUS	; IF A CARRY RESULT IS PLUS
9198 95	487	CPL F0	SET FLAG FO TO "1"
01B 9 37	488	CPL A	; COMPLEMENT ANSHER
01BA 07	489	DEC A	SUBTRACT 1 AS HE ADD 1 NEXT STEP
01B8 17	490 PLUS	INC A	ADD 1 TO GET CORRECT ANSWER
O1BC AA	491	MOV R2, A	STORE ANSWER IN R2
018 0 83	492	RET	, return

F0C 08	J 550	SOURCE STATEMENT	
	493		
	494		
	495	BINARY MULTIPLY SUBR	
	496	· · · · · · · · · · · · · · · · · · ·	A 1-BYTE MULTIPLIER AND A 1-BYTE
	497		DUCT THEREFORE IS 2 BYTES LONG.
	498	THE ALGORITHM FOLLOW	
	499	; (1) THE REGISTERS AR	E HIROTHIGED HS FULLUMS
	500 501	; ACC = 0	ra
	582	; R1 = MULTIPLI ; R2 = MULTIPLI	
	503	; R2 = MULTIPLE ; R3 = L00P COU	
	584		REGISTER RL ARE TREATED AS A REGISTER
	5 8 5	PRIR MHEN THEY ARE S	
	596		AND R1 ARE SHIFTED RIGHT 1 PLACE - THUS THE
	507	LSB OF THE MULTIPLIE	R GOES INTO THE CARRY
	588	; (3) THE MULTIPLICAND	15 ADDED TO THE ACCUMULATOR IF THE CARRY
	589	BIT IS A '1' NO ACTI	ON IF CARRY IS A 101
	510	; (4) DECREMENT THE LO	op counter and loop (return to step 2) unti
	511	; IT REACHES ZERO.	
	512	; (5) SHIFT THE RESUL	T RIGHT 1 LAST TIME JUST BEFORE EXITING
	513	; THE ROUTINE	
	514		
	515		FOUND MSBYTE IN THE ACCUMULATOR AND
	516	; LSBYTE IN R1.	
01BE BE			
0100 27		CLR A	CLEAR ACCUMULATOR
01C1 97 01C2 34		CLR C P1: CALL DBLRT	CLEAR CARRY BIT DOUBLE SHIFT RIGHT ACC
QTCS 74	521	ri. CHEL DECKI	AND R1 INTO CARRY
9104 E6	_	JNC BMP2	; IF CARRY = 1 ADD ELSE DON'T
01C6 69	_	ADD R. R2	ADD MULTIPLICAND TO ACCUMULATOR
01C7 EE			
V 20. L 0	525	2. 50/12 /13/2/11	LOOP IF NOT ZERO
01 09 34		CALL DBLRT	yabbi ir irbi barib
6108 83		RET	
	528		
	529		
	530		
01CC 67	7 531 08	LRT: RRC A	ROTATE RIGHT THRU CAPPY
01CD 25		XCH A, R1	GET R1 IN ACCUM
01CE 67	7 533	RRC A	
01CF 25		XCH A, R1	, PUT_R1_BACK
01D0 83		RET	
	536		
0454 05	537 MR		OFF S HOLLE FROM O.F.
9101 23		MOV A, #29H	GET R VALUE FROM A/D
9103 34		CALL CONOCO	PUT IN ACCUMULATOR
01D5 BF	75C 540 541	MOV R2, #95CH	FIF R MUST BE LESS THAN
	542		-11 5K OUT OF 15 7K A/D - VALUE MUST BE LESS THAN
	543		11 5/15 7 X 127 ≈92≈050H
		total two	- 11 3/13 / X 12/ =92=60CH - 05CH ~ R VALUE
04D7 74	MR (~44		
01D7 34		CALL SBTCT CPL FA	FOR THE VILLE
0107 34 0109 95 0109 86	5 545	CPL F0 JF0 MRK2	, IF A CARPY NO EPPOF

1515-11 MCS-48/ HYCOS - A6 REV	'UPI-41 MACRO AS 18 1/19/80	SEMBLER: V2.0	PAGE 11
F0C 081	SEQ	Source Statement	
01DE 39	548	OUTL PLA	; LEVEL LAMP
01DF 0498	549 MRK2:	JMP RAT	
	550		
	551		
	\$52	DIVIDE ROUTINE	
	55 3	HE DIVIDE A 16 BIT D	IVIDEND BY AN 8 BIT DIVISOR
	554	SMSBYTE OF DIVIDEND IS	5 IN R2
	555	SUSBYTE OF DIVIDEND 19	5 IN R3
	556	OTVISOR IS IN THE AC	CUMULATOR
	557	HE CHECK FOR THE FIRE	ST '1' IN THE DIVISOR WHICH TELLS US HOW
	558	- : MANY DIVISIONS. HE A	DO THE 215 COMPLEMENT OF THE DIVISOR TO
	559	THE DIVIDEND. THE RES	ULTING CARRY IS SHIFTED INTO THE LSB
	568	POSITION OF THE LSBY	TE THAT RESULTING CARRY IS SHIFTED INTO
	561	THE LSB POSITION OF	THE MSBYTE. THE FINAL ANSWER IS STORED
	562	; IN HEMORY	
82 80	56 3	org 9298H	
8290 88 90	564 DIVIDE	: MOY R3, #0	CLEAR R3
8282 BD88	565	MOV R5, #0	CLEAR RS
8284 85	56 6	CLR F0	CLEAR FLAG FO
9295 97	567	CLR C	CLEAR CARRY
0206 890 8	568	MOV RL, MOSH	INITIAL # OF DIVIDE STEPS
0208 53FF	569	and a hoffh	>TO SEE IF ACCUM ≈ 0
020 8 0632	579	JZ X7	HANT TO RYOID DIVIDE BY B
82 9 0 F7	571 X1:	RLC A	HANT FIRST 111 SO WE KNOW
0200 19	572	INC R1	HOM HANY DIVIDE STEPS
020E 1D	573	INC R5	Fame as above
020F E60C	574	JNC X1	FIRST ONE
0211 67	575	RRC A	RETURN (1) TO ACCUM
6 212 37	576	CPL R	11'S COMPLEMENT
021 3 1 7	577	INC A	321S COMPLEMENT
0214 AC	578	MOY R4, A	; SRVE DIVISOR
8215 27	579	CLR A	
0216 97	588 X6:	CLR C	
0217 A7	581	CPL C	
9218 F 7	582	RLC A	
0219 ED16	583	DJNZ R5, X6	
021B AE	584	MOV R6, A	
921C FC	585	MOV 8. R4	
8210 6A	586 X2:	ADD A, R2	SUBTRACT DIVISOR FROM DIVIDEND
921E F622	587	JC X5	FIF FLAG SET WAS A CARRY
8228 E625	588	JNC X3	IF NO CARRY NO CHANGE
622 2 97	589 X5:	CLR C	- WANT TO SET CARRY TO 1
8223 A7	590	CPL C	ELECT CASE AND DECIMAL TALLOW
0224 AA	591	MOV R2.A	ELSE PUT NEW RESULT IN R2
0225 FB	592 X3	MOY A, R3	LSBYTE IN ACCUM
6226 F7	593	RLC A	SHIFT CARRY INTO LSB
8227 AB	594	MOV R3, A	PUT BACK
8228 85 9999 50	595	CLR F0	CLEAR FLAG FO
8229 FR	596	MOV A, R2	MSBYTE IN ACCUM
8228 F7	597 500	RLC A	SHIFT CHRRY INTO LSB
8228 E62E	598 500	JNC X4	; NO CARRY DON'T SET FO
9220 95	599	CPL F0	: IF CARRY SET F9
022E AR	689 X4	MOV R2, A	PUT BACK
922F FC	681	MOV A, R4	GEY DIVISOR BACK
0230 E910	602	DJNZ R1, X2	- CONTINUE DIVISION

ISIS-II MCS-48. HYCOS - A6 REV	/UPI-41 MACRO AS 18 1/19/80	SEMBLER, V2. 0	PRGE 12
LOC OBJ	SEQ	Source Statement	
0232 FE	693 X7:	HOV A. R6	
6233 5A	684	ANL A.R2	
6234 18	685	INC RO	GET NEXT MEMORY POSITION
0235 A0	686	MOV ero, A	STORE IN MEMORY
8236 18	697	INC RO	NEXT MEMORY LOCATION
8237 FB	688	MOY A, R3	LSBYTE TO ACCUM
9238 AB	689	MOV ere, A	AND STORE IN MEMORY
8239 83	610	RET	7700 State In Tellan
	611		
	612	; LKUP1	
	613		GET (T2 - T1) X 3.78 INTO THE BINARY
	614		H BIT IS 53 OHMS. THIS MAKES EVERY 14 DEGREES
	615		Suning a temperature shing Max of From -54
	616	; C TO + 135 C OR 189	DEGREES, 189/14 = 13.5. THIS PROGRAM HILL
	617	:LET T' = 13 FOR 2T >	182 AND WILL SUBTRACT 1 FOR EACH 14 DEGREE
	618		RED IN REG 3. THE ANSHER IS IN REG 4
	619	; (182 - 14 N) WHERE	N = NUMBER OF SUBTRACTIONS
	620		
	621		
923A AB	622 LKUP1 :	MOV R3, A	STORE 2T IN R3
0238 BC0E	623	MOV R4, MOEH	START WITH 14 IN R4
0230 606 6	624	HOV R5, #886H	START WITH 182 IN R5
023F FB	625 REPT1:	MOV AJR3	AT IN ACCUM
8248 AA	626	MOV R2, Ř	AND PUT IN R2
0241 FD	627	MOV AJRS	₹182 -14N
0242 34B3	628	CALL SBTCT	(2T - (182 - 14N)
0244 FD	629	MOV AJR5	; GET 182 -14N
0245 03F2	630	ADD A, #8F2H	; Subtract another 14
0247 AD	631	MOV R5, A	; NEW YALUE BACK IN RS
8248 FC	632	MOV ALR4	; PUT_R4_INTO_ACCUM
0249 07	633	DEC A	a contains answer
024A C64F	634	JZ NOMR1	; IF R4 = 0 END ROUTINE
024C AC	635	HOV R4, A	; ELSE PUT RESULT BRCK IN R4
0240 B63F	636	JF0 REPT1	; IF F9 %T ((182 - 14N)
0 24F 83	637 Nohr 1.:	RET	
	638		
	639		
	540		
	641	; LKUP2	
	642		LOOKUP TABLE . THIS ROUTINE WILL TAKE
	643		53 AND GIVE THE BINARY EQUIVALENT OF THE
	644		KUP1 ABOVE EACH TEMPERATURE DELTA IS 16
	645		MRX = 189 . 189/16 = 11.8. WE LET THE
	646		R 2T > 176 AND HE SUBTRACT 1 FOR EVERY
	647	,16 DEGREE LONERING	
	648	XT IS STORED IN R3.	
	649	FINAL ANSWER STORED	IN K4
	65 0		
	651 650		
anen ne	652	MAI 85 A	CTORE OF THE REAL PROPERTY.
8258 AB	653 LKUP2:		STORE XT IN REG 3
9251 BC9C	654 (55	MOV R4, BOCH	START WITH 12 IN R4
6253 BD89	655 656 PERTO:	MOV R5, 11088H MOV A, R3	; START WITH 176 IN R5
9255 FB 9256 AA	656 REPT2: 657	HOV R2/R	; 2T IN ACCUM ; AND INTO R2
02JO 181	e)(muy KZ/N	FIRE INTO RE

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ISIS-II MCS-48/UPI-41 MACRO ASSEMBLER: V2. 0
                                                          PAGE
HYC05 - R6 REV 18 1/19/88
 LOC OBJ
                   Œθ
                               SOURCE STATEMENT
  6257 FD
                    658
                                         HOV ALRS
                                                                  :176 - 16N INTO ACCUM
                                                                  ;2T - ( 176 - 16N )
                                         CALL SBTCT
  0258 3483
                    659
  925A FD
                    660
                                         MOV RURS
                                                                  GET 176 -16N
  0258 03F0
                                         ADD R. MOFOH
                                                                  ; SUBTRACT ANOTHER 16
                    661
  8250 AD
                     662
                                         MOV R5. A
                                                                  FAND STORE RESULT IN R5
  025E FC
                                                                  FR4 INTO ACCUM
                    663
                                         MOV PLR4
  825F 87
                    664
                                         DEC A
                                                                  FR HAS ANSHER
  0260 C665
                    665
                                         JZ NONR2
                                                                  FIF R4 IS 0 END ROUTINE
  8262 AC
                     666
                                                                  FELSE PUT RESULT BACK IN R4
                                         MOV R4, A
  0263 B655
                                         JF0 REPT2
                                                                  ; IF F0 2T < € 176 - 16N →
                    667
  9265 83
                    668 NOMR2:
                                         RET
                    669
                    670
                    671
                    672
                    673
                    674 ; QUAD MULTIPLY
                    675 FIRST MULTIPLY # AND R7 (LSBYTE) DROP LSBYTE OF RESULT
                    676 ; AND ADD MSBYTE OF RESULT TO R5.
                    677 ; THEN MULTIPLY # AND R6 (MSBYTE), ADD LSBYTE OF RESULT
                    678 ; TO R5 AND MSBYTE OF RESULT TO R4.
                    679
                    689
  0266 RA
                    681 QUADM:
                                         MOV R2, R
                                                         GET MULTIPLIER IN R2
  8267 FF
                    682
                                         MOV PLR7
                                                         ; LSBYTE
  0268 R9
                    683
                                         HOV RLA
                                                         ; TO R1
                                         CRLL BMPY
  0269 34BE
                    684
                                                         HULTIPLY
                                                         FADD MSBY OF CALC TO R5
  9268 60
                    685
                                         ADD AJR5
                                         MOV R5, A
  826C AD
                    686
                                                         ; STORE IN R5
  925D E679
                    687
                                         JNC Y1
                                                         FIF CARRY
  026F 1C
                    688
                                         INC R4
                                                         ; RDD 1 TO R4
  9279 FE
                    689 Y1:
                                         MOV RURG
                                                         ; MSBYTE
  0271 R9
                    698
                                         HOY RL R
                                                         ; TO R1
  0272 34BE
                    691
                                         CRLL BMPY
                                                         HULTIPLY
  8274 29
                                                         ; MSBY TO R1 LSBY TO A
                    692
                                         XCH R-R1
  8275 60
                                         ADD A/R5
                                                         ADD LSBYTES
                    693
  0276 BD00
                    694
                                         MOV R5, #9H
                                                         ; CLEAR R5
  0278 AF
                    695
                                         HOY R7, A
                                                         FRESULT TO R7
  0279 E670
                    696
                                         JNC Y2
                                                         FIF CARRY
  027B 1C
                    697
                                         INC R4
                                                         FADD 1 TO MSBY
  027C F9
                    698 Y2:
                                         MOV A, R1
                                                         , MSBYTE TO A
  6270 GC
                    699
                                         ADD ALR4
                                                         ; ADD MSBYTES
  627E BC00
                                                         CLEAR R4
                    700
                                         MOV R4, #8H
  0280 RE
                    791
                                         MOV R6, A
                                                         RESULT TO R7
  0281 83
                    702
                                         RET
                    703
                    794
                    705
                    706
                    707
                    798
                                         END
USER SYMBOLS
      01C2
                                              BYTST 0147
emp1
               RMP2
                      91C7
                               RMPV
                                     MAE
                                                             CONT
                                                                     013F
                                                                             DBLRT 01CC
                                                                                            DECR 0143
                                                                                                            DIVIDE 0200
                                                                                                            LKUP2 0250
END2
      99E4
               END3
                      00E1
                              END4
                                     9190
                                              EXCH
                                                     0199
                                                             FINI
                                                                     01R4
                                                                             GONOGO 01R9
                                                                                            LKUP1 023A
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1515-11 MC5-48/UP1-41 MACRO ASSEMBLER, V2.0 HYCOS - R6 REV 18 1/19/80							PRGE 14								
LSD	915 C	MLTPLY	917 C	MRK1	01 D1	MRK2	91DF	MS18	0138	MULT	9189	HVMPLY	012E	NEG1	9938
NMLT1	9909	NMLT2	9904	NOCR	9994	NOK	01AA	NOMLT	00C5	NOMP1	924F	NOMR2	0265	NTMPTR	0129
ÛK	01B0	PLUS	91BB	P051	884 C	PRSCLC	0100	QUADH	0266	RAT	9998	READ	9164	REPT1	023F
REPT2	6255	RMLD	9925	RSRVR	9979	RSTR	019C	RUDDER	995D	SERTN	9182	SBTCT	01B3	SONCE	601 6
START	8882	SIM	004E	THPCK	9188	TSTUT	991B	MRITE	014F	X1	020C	X2	021D	X3	0225
¥4	822F	X5	9222	X6	9216	X7	9070	W	9279	¥2	927C	-			_

RESEMBLY COMPLETE. NO ERRORS

